# chemicals Documentation 

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1 Key Features \& Capabilities ..... 3
2 Installation ..... 495
3 Latest source code ..... 497
4 Bug reports ..... 499
5 License information ..... 501
6 Citation ..... 503
7 Indices and tables ..... 505
Bibliography ..... 507
Python Module Index ..... 541
Index ..... 543

## KEY FEATURES \& CAPABILITIES

The chemicals library features an extensive compilation of pure component chemical data that can serve engineers, scientists, technicians, and anyone working with chemicals. The chemicals library facilitates the retrieval and calculation of:

- Chemical constants including formula, molecular weight, normal boiling and melting points, triple point, heat of formation, absolute entropy of formation, heat of fusion, similarity variable, dipole moment, acentric factor, etc.
- Assorted information of safety and toxicity of chemicals.
- Methods (and their respective coefficients) for the calculation of temperature and pressure dependent chemical properties including vapor pressure, heat capacity, molar volume, thermal conductivity, surface tension, dynamic viscosity, heat of vaporization, relative permittivity, etc.
- Methods to solve thermodynamic phase equilibrium, including flash routines, vapor-liquid equilibrium constant correlations, and both numerical and analytical solutions for the Rachford Rice and Li-Johns-Ahmadi equations. Rachford Rice solutions for systems of 3 or more phases are also available.

Data for over 20,000 chemicals are made available as local databanks in this library. All databanks are loaded ondemand, saving loading time and RAM. For example, if only data on the normal boiling point is required, the chemicals library will only load normal boiling point datasets. This on-demand loading feature makes the chemicals library an attractive dependence for software modeling chemical processes. In fact, The Biorefinery Simulation and TechnoEconomic Analysis Modules (BioSTEAM) is reliant on the chemicals library for the simulation of unit operations.

The chemicals library also supports integration with Numba, a powerful accelerator that works well with NumPy; Pint Quantity objects to keep track of units of measure; and NumPy vectorized functions.
If you need to know something about a chemical, give chemicals a try.

### 1.1 Chemicals tutorial

### 1.1.1 Importing

Chemicals can be imported as a standalone library, or all of its functions and classes may be imported with star imports:

```
>>> import numpy as np
>>> import chemicals # Good practice
>>> from chemicals import * # Bad practice but convenient
```

All functions are available from either the main chemicals module or the submodule; i.e. both chemicals.Antoine and chemicals.vapor_pressure. Antoine are valid ways of accessing a function.

### 1.1.2 Design philosophy

Like all libraries, this was developed to scratch my own itches.
The bulk of this library's API is considered quite stable; enhancements to functions and classes will still happen, and default methods when using a generic correlation interface may change to newer and more accurate correlations as they are published and reviewed.
All functions are designed to accept inputs in base SI units. However, any set of consistent units given to a function will return a consistent result. The user is directed to unit conversion libraries such as pint to perform unit conversions if they prefer not to work in SI units. The tutorial for using it with chemicals is at chemicals.units.

There are two ways to use numpy arrays with chemicals. The easiest way to use numpy is a vectorized module, which wraps all of the chemicals functions with np.vectorize. Instead of importing from chemicals, the user can import from chemicals.vectorized:

```
>>> from chemicals.vectorized import *
>>> Antoine(np.linspace(100, 200, 5), A=8.95894, B=510.595, C=-15.95)
array([7.65674361e+02, 1.89116754e+04, 1.41237759e+05, 5.60609191e+05,
    1.53010431e+06])
```

Inputs do not need to be numpy arrays; they can be any iterable:

```
>>> import chemicals.vectorized
>>> chemicals.vectorized.Tc(['108-88-3', '7732-18-5'])
array([591.75 , 647.096])
```

It is possible to switch back and forth between the namespaces with a subsequent import:

```
>>> from chemicals import *
```

The second way is Numba. This optional dependency provides the speed you expect from NumPy arrays - or better. In some cases, much better. The tutorial for using it is at chemicals.numba, but in general use it the same way but with a different import.

```
>>> import chemicals.numba_vectorized
```

Note that numba can also be used to speed up scalar calculations without numpy.

```
>>> import chemicals.numba
```


### 1.1.3 Working with Elements

Chemicals contains a periodic table.

```
>>> from chemicals import *
>>> periodic_table.Na
<Element Sodium (Na), number 11, MW=22.98977>
>>> periodic_table.U.MW
238.02891
>>> periodic_table['Th'].CAS
'7440-29-1'
>>> periodic_table.lead.protons
82
```

(continues on next page)

```
>>> periodic_table['7440-57-5'].symbol
'Au'
>>> len(periodic_table)
118
>>> 'gold' in periodic_table
True
>>> periodic_table.He.protons, periodic_table.He.neutrons, periodic_table.He.electrons #_
Standard number of protons, neutrons, electrons
(2, 2, 2)
>>> periodic_table.He.phase # Phase of the element in the standard state
'g'
>>> periodic_table.He.Hf # Heat of formation in standard state in J/mol - by definition (1)
0.0
>>> periodic_table.He.S0 # Absolute entropy (J/(mol%K) in standard state - non-zero)
126.2
>>> periodic_table.Kr.block, periodic_table.Kr.period, periodic_table.Kr.group
('p', 4, 18)
>>> periodic_table.Rn.InChI
'Rn'
>>> periodic_table.Rn.smiles
'[Rn]'
>>> periodic_table.Pu.number
94
>>> periodic_table.Pu.PubChem
23940
>>> periodic_table.Bi.InChI_key
' JCXGWMGPZLAOME-UHFFFAOYSA-N'
```

The periodic table is a singleton of the periodic table class PeriodicTable. Each attribute accessed is a reference to an element object Element. The elements are the basic building blocks of every chemical.

### 1.1.4 Working with Chemical Identifiers

Chemicals comes with a large library of chemical identifiers. Chemicals has various ways of searching through its database. There are a number of different support chemical identifiers as well.

CAS numbers - These are the primary identifiers in Chemicals. A CAS number uniquely identifies a chemical molecule. 7732-18-5 is the CAS number for water. Sometimes, it also identifies the phase of the chemical. 7440-44-0 is the CAS number for carbon in general, but 7782-42-5 is the CAS number for graphite and 7782-40-3 is the CAS number for diamond. Note that because these are assigned by people, mistakes are made and often multiple CAS numbers point to the same compound. Common Chemistry lists 57 "retired" CAS numbers which point to the element carbon. The CAS numbers in Chemicals come mostly from PubChem as there was no Common Chemistry project back then.

PubChem IDs - These are the identifiers for each compound in the PubChem database. Most of the metadata in Chemicals came from PubChem. 962 is the Pubchem identifier for water. Each entry in PubChem comes with a structure. Sometimes structures are found to be duplicates of each other and entries are merged; these identifiers are assigned automatically by the NIH.

Smiles - These are actual chemicals structures, rendered into easily readable text. Multiple smiles strings can represent the same compound; they are not unique. Both " $\mathrm{C}(=\mathrm{O})=\mathrm{O}$ " and " $\mathrm{O}=\mathrm{C}=\mathrm{O}$ " are valid SMILES strings for identifying CO 2 . Programs like rdkit can create a computational representation of the molecule from a SMILES string. To solve this duplication issue, a concept of a canonical SMILES string was developed which is supposed to be unique, but in
general is not reliable at all and only consistent within the same molecular modeling software. There is in general no organization which controls this format, but a there is an effort in the open source community to standardize the format called opensmiles
Chemical Formula - These are what every student is taught in chemistry class. H2O is the formula for water. Is OH 2 also a valid formula? Yes. There is a convention called the Hill convention (implemented in chemicals as atoms_to_Hill () which specified the H 2 O is how the formula should be written. Not all formulas, especially inorganic formulas or older formulas, follow this convention. Formulas are in general NOT unique. Even simple formulas which seem like there should only be one compound with that formula are often duplicated; carbonic acid and performic acid both have the formula "CH2O3". Searching Chemical's databases with a formula is a common mistake by users. While you can do it and you may get a match, there is no guarantee the match you wanted was found. The following snippet of code counts the number of compounds with the same formula as asprin; illustrating why searching by formula is a bad idea.

```
>>> from chemicals.identifiers import pubchem_db
>>> len(list(i for i in pubchem_db if i.formula == 'C9H804'))
20
```

Chemical name - Anyone can call a chemical by any name, so predictably names are a mess. A large number of names were retrieved from PubChem, and form the basis for searches by name in Chemicals. Only one chemical hit will be found for each name search. There is an effort by IUPAC to systematically generate names for each chemical structure, called OPSIN. Most chemicals in Chemicals have a correct, associated IUPAC name retrieved from PubChem. There are in the range of a million names that can be looked by in Chemicals.

InChI - Short for the IUPAC International Chemical Identifier, these are programmatically derived strings which represent a compound. A non-profit was established to maintain a software package to manage this format; it is not like SMILES where lots of software implement the format. There contain all the information required to form a structure. There is a variant which is truly unique per compound; this is what is in Chemicals. They have more features than SMILES strings. "C6H14/c1-3-5-6-4-2/h3-6H2,1-2H3" is a sample string, for n-hexane. This is the best possible type of an identifier for a chemical. These can get to be quite long for complex structures.

InChI key - A 27-character hash of the unique InChI identifier. These are also in Chemicals and generated by the same InChI software. These were intended to be unique, and easy to search for as search engines don't search for InChI strings well. Some collisions have been detected. 'VLKZOEOYAKHREP-UHFFFAOYSA-N' is the InChI key for n-hexane as an example.
The main interface for looking up a chemical from one of these identifying markers is search_chemical (). The search can be performed with any of the following input forms:

- Name, in IUPAC form or common form or a synonym registered in PubChem
- InChI name, prefixed by 'InChI=1S/' or 'InChI=1/'
- InChI key, prefixed by 'InChIKey='
- PubChem CID, prefixed by 'PubChem='
- SMILES (prefix with 'SMILES=' to ensure smiles parsing; ex. 'C' will return Carbon as it is an element whereas the SMILES interpretation for ' C ' is methane)
- CAS number (obsolete numbers may point to the current number)

If the input is an ID representing an element, the following additional inputs may be specified as

- Atomic symbol (ex 'Na')
- Atomic number (as a string)

Some sample queries illustrating the topic:

```
>>> search_chemical('water')
<ChemicalMetadata, name=water, formula=H2O, smiles=0, MW=18.0153>
>>> search_chemical('InChI=1S/C2H6O/c1-2-3/h3H, 2H2,1H3')
<ChemicalMetadata, name=ethanol, formula=C2H60, smiles=CCO, MW=46.0684>
>>> search_chemical('CCCCCCCCCC')
<ChemicalMetadata, name=DECANE, formula=C10H22, smiles=CCCCCCCCCC, MW=142.286>
>>> search_chemical('InChIKey=LFQSCWFLJHTTHZ-UHFFFAOYSA-N')
<ChemicalMetadata, name=ethanol, formula=C2H60, smiles=CCO, MW=46.0684>
>>> search_chemical('pubchem=702')
<ChemicalMetadata, name=ethanol, formula=C2H60, smiles=CCO, MW=46.0684>
>>> search_chemical('0') # only elements can be specified by symbol
<ChemicalMetadata, name=oxygen, formula=0, smiles=[0], MW=15.9994>
```

Each of those queries returns a ChemicalMetadata object. The object holds the chemical metadata. It is an almost unbearable task to assemble a chemical property database. Making a database of chemical metadata is only slightly easier. The chemical metadata database doesn't have any information whatsoever about about any chemical properties; only information about the chemical structure and those identifiers mentioned above. Each of those identifiers is an attribute of the returned object.

```
>>> water = search_chemical('water')
>>> (water.pubchemid, water.formula, water.smiles, water.InChI, water.InChI_key, water.
    CASs)
(962, 'H2O', 'O', 'H2O/h1H2', 'XLYOFNOQVPJJNP-UHFFFAOYSA-N', '7732-18-5')
>>> water.common_name, water.iupac_name, len(water.synonyms)
('water', 'oxidane', 89)
```


### 1.2 Acentric Factor (chemicals.acentric)

This module contains a lookup function, a definition function, and correlations for a chemical's acentric factor, normally given the variable $\omega$.

A similar variable called the stiel polar factor can be calculated from its definition as well.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Lookup Functions
- Definitions
- Correlations


### 1.2.1 Lookup Functions

chemicals.acentric.omega (CASRN, method=None)
Retrieve a chemical's acentric factor, omega.
Automatically select a method to use if no method is provided; returns None if the data is not available.

$$
\omega \equiv-\log _{10}\left[\lim _{T / T_{c}=0.7}\left(P^{s a t} / P_{c}\right)\right]-1.0
$$

## Parameters

# CASRN [str] CASRN [-] 

## Returns

omega [float] Acentric factor of compound

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'HEOS', 'PSRK', 'PD', or 'YAWS'. All valid values are also held in the variable omega_all_methods.

## See also:

omega_methods

## Notes

A total of four sources are available for this function. They are:

- 'PSRK', a compillation of experimental and estimated data published in the Appendix of [2], the fourth revision of the PSRK model.
- 'PD', an older compillation of data published in (Passut \& Danner, 1973) [3].
- 'YAWS', a large compillation of data from a variety of sources; no data points are sourced in the work of [4].
- 'ACENTRIC_DEFINITION', the precalculated results using the VaporPressure object of Thermo and the critical properties of chemicals.
- 'HEOS', a series of values from the NIST REFPROP Database for Highly Accurate Properties of Industrially Important Fluids (and other high-precision fundamental equations of state)


## References

[1], [2], [3], [4], [5]

## Examples

>>> omega(CASRN='64-17-5')
0.646
chemicals.acentric.omega_methods (CASRN)
Return all methods available for obtaining omega for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain omega with the given inputs.

## See also:

omega
chemicals.acentric.omega_all_methods = ('HEOS', 'PSRK', 'PD', 'YAWS', 'ACENTRIC_DEFINITION')

Tuple of method name keys. See the omega for the actual references

### 1.2.2 Definitions

chemicals.acentric.omega_definition (Psat, $P c$ )
Returns the acentric factor of a fluid according to its fundamental definition using the vapor pressure at a reduced temperature of 0.7 Tc .

$$
\omega \equiv-\log _{10}\left[\lim _{T / T_{c}=0.7}\left(P^{s a t} / P_{c}\right)\right]-1.0
$$

## Parameters

Psat [float] Vapor pressure of the fluid at a reduced temperature of 0.7 [ Pa ]
Pc [float] Critical pressure of the fluid [Pa]

## Returns

omega [float] Acentric factor of the fluid [-]

## References

[1]

## Examples

Water
>>> omega_definition(999542, 22048320.0)
0. 3435744558761711
chemicals.acentric.Stiel_polar_factor (Psat, Pc, omega)
This function handles the calculation of a chemical's Stiel Polar factor, directly through the definition of Stielpolar factor. Requires the vapor pressure Psat at a reduced temperature of 0.6 , the critical pressure $P c$, and the acentric factor omega.

$$
x=\left.\log _{10} P_{r}\right|_{T_{r}=0.6}+1.70 \omega+1.552
$$

## Parameters

Psat [float] Vapor pressure of fluid at a reduced temperature of 0.6 [Pa]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor of the fluid [-]

## Returns

factor [float] Stiel polar factor of compound, [-]

## Notes

A few points have also been published in [2], which may be used for comparison. Currently this is only used for a surface tension correlation.

## References

[1], [2]

## Examples

Calculating the factor for water:

```
>>> Stiel_polar_factor(Psat=169745, Pc=22048321.0, omega=0.344)
```

0.02322146744772713

### 1.2.3 Correlations

## chemicals.acentric.LK_omega ( $T b, T c, P c$ )

Estimates the acentric factor of a fluid using a correlation in [1].

$$
\omega=\frac{\ln P_{b r}^{s a t}-5.92714+6.09648 / T_{b r}+1.28862 \ln T_{b r}-0.169347 T_{b r}^{6}}{15.2518-15.6875 / T_{b r}-13.4721 \ln T_{b r}+0.43577 T_{b r}^{6}}
$$

## Parameters

Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]

## Returns

omega [float] Acentric factor of the fluid [-]

## Notes

The units of the above equation are atmosphere and Kelvin; values are converted internally.

## References

[1]

## Examples

Isopropylbenzene, from Reid (1987).
>>> LK_omega(425.6, 631.1, 32.1E5)
0. 32544249926397856

### 1.3 Air: Fundamental Equation of State for Air (chemicals.air)

This module contains various thermodynamic functions for air and humid air.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Dry Air Basic Solvers
- Dry Air Bubble/Dew Points
- Dry Air Constants
- Dry Air Ideal Gas Terms
- Dry Air Residual Terms
- Humid Air Virial Terms
- Henry's Law for Air in Water


### 1.3.1 Dry Air Basic Solvers

chemicals.air.lemmon2000_rho $(T, P)$
Calculate the density of air according to the Lemmon (2000) [1] given a temperature $T$ and pressure $P$.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Molar density of air, [ $\mathrm{mol} / \mathrm{m}^{\wedge} 3$ ]

## Notes

This solution is iterative due to the nature of the equation. This solver has been tested only for gas solutions.

## References

[1]

## Examples

>>> lemmon2000_rho(T=300.0, $\mathrm{P}=1 \mathrm{e} 6)$
402.046613509

2 GPa and 2000 K are suggested as upper limits of [1] although there are no hardcoded limits for temperature and pressure.

```
>>> lemmon2000_rho(T=2000.0, P=2e9)
```

32892.9327834

## chemicals.air.lemmon2000_P( $T$, rho)

Calculate the pressure of air according to the (2000) given a temperature $T$ and molar density rho.

## Parameters

T [float] Temperature, [K]
rho [float] Molar density of air, [ $\mathrm{mol} / \mathrm{m}^{\wedge} 3$ ]

## Returns

$\mathbf{P}$ [float] Pressure, [Pa]

## Notes

Helmholtz equations of state are explicit with inputs of temperature and density, so this is a direct calculation with no iteration required.

## References

[1]

## Examples

```
>>> lemmon2000_P(330.0, lemmon2000_rho(T=330.0, P=8e5))
8e5
>>> lemmon2000_P(823.0, 40)
273973.0024911
```

chemicals.air.lemmon2000_T( $P$, rho)
Calculate the temperature of air according to the Lemmon (2000) [1] given a pressure $P$ and molar density $r$ oho .

## Parameters

$\mathbf{P}$ [float] Pressure, [Pa]
rho [float] Molar density of air, [ $\mathrm{mol} / \mathrm{m}^{\wedge} 3$ ]

## Returns

$\mathbf{T}$ [float] Temperature, [K]

## Notes

This solution is iterative due to the nature of the equation. This solver has been tested only for gas solutions.

## References

[1]

## Examples

>>> lemmon2000_T(P=1e5, rho=20.0)
601.1393854499

### 1.3.2 Dry Air Bubble/Dew Points

chemicals.air.lemmon2000_air_P_dew ( $T$ )
Calculates the dew pressure of standard dry air according to Lemmon (2000).

$$
\ln \left(\frac{P_{\text {dew }}}{P_{j}}\right)=\left(\frac{T_{j}}{T}\right) \sum_{i}^{8} N_{i} \theta^{i / 2}
$$

## Parameters

T [float] Temperature, [K]

## Returns

P_dew [float] Dew pressure, [Pa]

## Notes

The stated range of this ancillary equation is $59.75 \mathrm{~K}<=\mathrm{T}<=132.6312 \mathrm{~K}$.

## Examples

```
>>> lemmon2000_air_P_dew(100.0)
567424.1338937
```

chemicals.air.lemmon2000_air_P_bubble( $T$ )
Calculates the bubble pressure of standard dry air according to Lemmon (2000).

$$
\ln \left(\frac{P_{b u b b l e}}{P_{j}}\right)=\left(\frac{T_{j}}{T}\right) \sum_{i}^{8} N_{i} \theta^{i / 2}
$$

## Parameters

$\mathbf{T}$ [float] Temperature, [K]

## Returns

P_bubble [float] Bubble pressure, [Pa]

## Notes

The stated range of this ancillary equation is $59.75 \mathrm{~K}<=\mathrm{T}<=132.6312 \mathrm{~K}$.

## Examples

```
>>> lemmon2000_air_P_bubble(100.0)
```

663128.589440

## chemicals.air.lemmon2000_air_rho_dew ( $T$ )

Calculates the dew molar density of standard dry air according to Lemmon (2000).

$$
\ln \left(\frac{\rho_{\text {dew }}}{\rho_{j}}\right)=N_{1} \theta^{0.41}+N_{2} \theta+N_{3} \theta^{2.8}+N_{4} \theta^{6.5}
$$

## Parameters

T [float] Temperature, [K]

## Returns

rho_dew [float] Dew point molar density, [ $\mathrm{mol} / \mathrm{m}^{\wedge} 3$ ]

## Notes

The stated range of this ancillary equation is $59.75 \mathrm{~K}<=\mathrm{T}<=132.6312 \mathrm{~K}$.

## Examples

>>> lemmon2000_air_rho_dew(100.0)
785.7863223794999

## chemicals.air.lemmon2000_air_rho_bubble( $T$ )

Calculates the bubble molar density of standard dry air according to Lemmon (2000).

$$
\left(\frac{\rho_{\text {bubble }}}{r h o_{j}}-1\right)=N_{1} \theta^{0.65}+N_{2} \theta^{0.85}+N_{3} \theta^{0.95}+N_{4} \theta^{1.1}+N_{5} \ln \frac{T}{T_{j}}
$$

## Parameters

$$
\mathbf{T} \text { [float] Temperature, [K] }
$$

## Returns

rho_bubble [float] bubble point molar density, $\left[\mathrm{mol} / \mathrm{m}^{\wedge} 3\right.$ ]

## Notes

The stated range of this ancillary equation is $59.75 \mathrm{~K}<=\mathrm{T}<=132.6312 \mathrm{~K}$.

## Examples

>>> lemmon2000_air_rho_bubble(100.0)
26530.979020427476

### 1.3.3 Dry Air Constants

```
chemicals.air.lemmon2000_air_T_reducing = 132.6312
```

Reducing temperature in K for the Lemmon (2000) EOS for dry air

```
chemicals.air.lemmon2000_air_rho_reducing = 10447.7
```

Reducing molar density in $\mathrm{mol} / \mathrm{m}^{\wedge} 3$ for the Lemmon (2000) EOS for dry air

```
chemicals.air.lemmon2000_air_P_reducing = 3785020.0
```

Reducing pressure in Pa for the Lemmon (2000) EOS for dry air

```
chemicals.air.lemmon2000_air_MW = 28.9586
```

Molecular weight of air in $\mathrm{g} / \mathrm{mol}$ for the Lemmon (2000) EOS for dry air

## chemicals.air.lemmon2000_air_R = 8.31451

Molar gas constant in Jlemmon2000_air_R/(mol*K) used in the the Lemmon (2000) EOS for dry air

```
chemicals.air.lemmon2000_air_T_max = 2000.0
```

Maximum temperature in K valid for the Lemmon (2000) EOS for dry air

```
chemicals.air.lemmon2000_air_P_max = 2000000000.0
```

Maximum pressure in Pa valid for the Lemmon (2000) EOS for dry air

### 1.3.4 Dry Air Ideal Gas Terms

## chemicals.air.lemmon2000_air_AQ (tau, delta)

Calculates the ideal gas Helmholtz energy of air according to Lemmon (2000).
$\phi^{\circ}=\ln \delta+\sum_{i=1}^{5} N_{i} \tau^{i-4}+N_{6} \tau^{1.5}+N_{7} \ln \tau+N_{8} \ln \left[1-\exp \left(-N_{11} \tau\right)\right]+N_{9} \ln \left[1-\exp \left(-N_{12} \tau\right)\right]+N_{10} \ln \left[2 / 3+\exp \left(N_{13} \tau\right)\right]$

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

A0 [float] Ideal gas dimensionless Helmholtz energy A0/(RT) [-]

## Notes

The coefficients are as follows:
$\mathrm{Ns}=[0.605719400 \mathrm{E}-7,-0.210274769 \mathrm{E}-4,-0.158860716 \mathrm{E}-3,-13.841928076,17.275266575,-0.195363420 \mathrm{E}-3$, $2.490888032,0.791309509,0.212236768,-0.197938904,25.36365,16.90741,37.31279]$

## Examples

>>> lemmon2000_air_A0(132.6312/200.0, 13000/10447.7)
-14.65173785639

## chemicals.air.lemmon2000_air_dAO_dtau(tau, delta)

Calculates the first temperature derivative of ideal gas Helmholtz energy of air according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

dA0_dtau [float] First derivative of $A O /(R T)$ Ideal gas dimensionless Helmholtz energy with respect to tau [-]

## Examples

>>> lemmon2000_air_dA0_dtau(132.6312/200.0, 13000/10447.7)
3.749095669249
chemicals.air.lemmon2000_air_d2AO_dtau2 (tau, delta)
Calculates the second temperature derivative of ideal gas Helmholtz energy of air according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (126.192 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d2A0_dtau2 [float] Second derivative of $A 0 /(R T)$ Ideal gas dimensionless Helmholtz energy with respect to tau [-]

## Examples

```
>>> lemmon2000_air_d2A0_dtau2(132.6312/200.0, 13000/10447.7)
-5.66675499015
```

chemicals.air.lemmon2000_air_d3AQ_dtau3(tau, delta)
Calculates the third temperature derivative of ideal gas Helmholtz energy of air according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (126.192 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d3A0_dtau3 [float] Third derivative of $A 0 /(R T)$ Ideal gas dimensionless Helmholtz energy with respect to tau [-]

## Examples

>>> lemmon2000_air_d3A0_dtau3(132.6312/200.0, 13000/10447.7)
17.10538866838

## chemicals.air.lemmon2000_air_d4AO_dtau4(tau, delta)

Calculates the fourth temperature derivative of ideal gas Helmholtz energy of air according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d4A0_dtau4 [float] Fourth derivative of $A O /(R T)$ Ideal gas dimensionless Helmholtz energy with respect to tau [-]

## Examples

```
>>> lemmon2000_air_d4AO_dtau4(126.192/200.0, 13000/10447.7)
```

-94.815532727

### 1.3.5 Dry Air Residual Terms

chemicals.air.lemmon2000_air_Ar (tau, delta)
Calculates the residual Helmholtz energy of air according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, $(132.6312 \mathrm{~K}) / \mathrm{T}[-]$
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

Ar [float] Residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt and many multiplies/adds.

## Examples

```
>>> lemmon2000_air_Ar(132.6312/200.0, 13000/10447.7)
```

-0. 34683017661
>>> lemmon2000_air_Ar(0.36842, 0.15880050154579475)
0.0047988122806
chemicals.air.lemmon2000_air_dAr_dtau(tau,delta)
Calculates the first derivative of residual Helmholtz energy of air with respect to tau according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

$\mathbf{d A r}$ _dtau [float] First derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to tau, [-]

## Notes

The cost of this function is 1 power, $3 \exp , 2$ sqrt, 1 divisions and the necessary adds/multiplies.

## Examples

>>> lemmon2000_air_dAr_dtau(132.6312/200.0, 13000/10447.7)
-1.8112257495223263
chemicals.air.lemmon2000_air_d2Ar_dtau2 (tau, delta)
Calculates the second derivative of residual Helmholtz energy of air with respect to tau according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d2Ar_dtau2 [float] Second derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to tau, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 2 divisions and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d2Ar_dtau2(132.6312/200.0, 13000/10447.7)
-0.7632109061747
```

chemicals.air.lemmon2000_air_d3Ar_dtau3(tau, delta)
Calculates the third derivative of residual Helmholtz energy of air with respect to tau according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d3Ar_dtau3 [float] Third derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to tau, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 4 divisions and the necessary adds/multiplies.

## Examples

>>> lemmon2000_air_d3Ar_dtau3(132.6312/200.0, 13000/10447.7)
0.27922007457420

## chemicals.air.lemmon2000_air_d4Ar_dtau4(tau, delta)

Calculates the fourth derivative of residual Helmholtz energy of air with respect to tau according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/( $\left.10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right)$, [-]

## Returns

d4Ar_dtau4 [float] Fourth derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to tau, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 4 divisions and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d4Ar_dtau4(132.6312/200.0, 13000/10447.7)
-8.197368061417
```

chemicals.air.lemmon2000_air_dAr_ddelta(tau,delta)
Calculates the first derivative of residual Helmholtz energy of air with respect to delta according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

dAr_ddelta [float] First derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to delta, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_dAr_ddelta(132.6312/200.0, 13000/10447.7)
```

-0.1367917666005
chemicals.air.lemmon2000_air_d2Ar_ddelta2 (tau, delta)
Calculates the second derivative of residual Helmholtz energy of air with respect to delta according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/( $\left.10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right)$, [-]

## Returns

d2Ar_ddelta2 [float] Second derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to delta, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d2Ar_ddelta2(132.6312/200.0, 13000/10447.7)
```

0. 27027259528316
chemicals.air.lemmon2000_air_d3Ar_ddelta3(tau, delta)
Calculates the third derivative of residual Helmholtz energy of air with respect to delta according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d3Ar_ddelta3 [float] Third derivative of residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ with respect to delta, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, and the necessary adds/multiplies.

## Examples

>>> lemmon2000_air_d3Ar_ddelta3(132.6312/200.0, 13000/10447.7)
0.1849386546766

## chemicals.air.lemmon2000_air_d4Ar_ddelta4(tau,delta)

Calculates the fourth derivative of residual Helmholtz energy of air with respect to delta according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d4Ar_ddelta4 [float] Fourth derivative of residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ with respect to delta, [-]

## Notes

The cost of this function is 1 power, $3 \exp , 2$ sqrt, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d4Ar_ddelta4(132.6312/200.0, 13000/10447.7)
```

0.37902213262258
chemicals.air.lemmon2000_air_d2Ar_ddeltadtau(tau, delta)
Calculates the second derivative of residual Helmholtz energy of air with respect to delta and tau according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/( $\left.10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right),[-]$

## Returns

d2Ar_ddeltadtau [float] Second derivative of residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ with respect to delta and tau, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d2Ar_ddeltadtau(132.6312/200.0, 13000/10447.7)
```

-1.359976184125

## chemicals.air.lemmon2000_air_d3Ar_ddeltadtau2 (tau, delta)

Calculates the third derivative of residual Helmholtz energy of air with respect to delta once and tau twice according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/( $10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3$ ), [-]

## Returns

d3Ar_ddeltadtau2 [float] Third derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to delta once and tau twice, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 3 divisions, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d3Ar_ddeltadtau2(132.6312/200.0, 13000/10447.7)
-0.19089212184849
```

chemicals.air.lemmon2000_air_d3Ar_ddelta2dtau(tau, delta)
Calculates the third derivative of residual Helmholtz energy of air with respect to delta twice and tau once according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, ( 132.6312 K )/T [-]
delta [float] Dimensionless density, rho/( $10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3$ ), [-]

## Returns

d3Ar_ddelta2dtau [float] Third derivative of residual dimensionless Helmholtz energy Ar/(RT) with respect to delta twice and once twice, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 3 divisions, and the necessary adds/multiplies.

## Examples

>>> lemmon2000_air_d3Ar_ddelta2dtau(132.6312/200.0, 13000/10447.7)
0.01441788198940

## chemicals.air.lemmon2000_air_d4Ar_ddelta2dtau2 (tau, delta)

Calculates the fourth derivative of residual Helmholtz energy of air with respect to delta twice and tau twice according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d4Ar_ddelta2dtau2 [float] Fourth derivative of residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ with respect to delta twice and tau twice, [-]

## Notes

The cost of this function is 1 power, $3 \exp , 2$ sqrt, 2 divisions, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d4Ar_ddelta2dtau2(132.6312/200.0, 13000/10447.7)
0.1196873112730
```


## chemicals.air.lemmon2000_air_d4Ar_ddeltadtau3(tau, delta)

Calculates the fourth derivative of residual Helmholtz energy of air with respect to delta once and tau thrice according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/(10447.7 mol/m^3), [-]

## Returns

d4Ar_ddeltadtau3 [float] Fourth derivative of residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ with respect to delta once and tau thrice, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 1 division, and the necessary adds/multiplies.

## Examples

>>> lemmon2000_air_d4Ar_ddeltadtau3(132.6312/200.0, 13000/10447.7)
2.077739387492

## chemicals.air.lemmon2000_air_d4Ar_ddelta3dtau(tau, delta)

Calculates the fourth derivative of residual Helmholtz energy of air with respect to delta thrice and tau once according to Lemmon (2000).

## Parameters

tau [float] Dimensionless temperature, (132.6312 K)/T [-]
delta [float] Dimensionless density, rho/( $10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3$ ), [-]

## Returns

d4Ar_ddelta3dtau [float] Fourth derivative of residual dimensionless Helmholtz energy $\mathrm{Ar} /(\mathrm{RT})$ with respect to delta thrice and tau once, [-]

## Notes

The cost of this function is 1 power, 3 exp, 2 sqrt, 1 division, and the necessary adds/multiplies.

## Examples

```
>>> lemmon2000_air_d4Ar_ddelta3dtau(132.6312/200.0, 13000/10447.7)
-0.26039336747
```


### 1.3.6 Humid Air Virial Terms

## chemicals.air.TEOS10_BAW_derivatives $(T)$

Calculates the second molar virial cross coefficient between air and water according to [1].

$$
B_{a w}(T)=\frac{1}{\bar{\rho}^{*}} \sum_{i=1}^{3} c_{i}(\theta)^{d_{i}}
$$

Where $\theta=T / T^{*}$ and $T^{*}=100 \mathrm{~K}$ and $\bar{\rho}=10^{6} \mathrm{~mol} / \mathrm{m}^{\wedge} 3$.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]

## Returns

Baw [float] Air-water second molar virial cross coefficient [m^3/mol]
dBaw_dT [float] First temperature derivative of air-water second molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 3 /(\mathrm{mol} * \mathrm{~K})\right]$
d2Baw_dT2 [float] Second temperature derivative of air-water second molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 3 /\left(\mathrm{mol}^{*} \mathrm{~K}^{\wedge} 2\right)\right]$
d3Baw_dT3 [float] Third temperature derivative of air-water second molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 3 /\left(\mathrm{mol}^{*} \mathrm{~K}^{\wedge} 3\right)\right]$

## Notes

The coefficients are as follows:
cis $=[0.665687 \mathrm{E} 2,-0.238834 \mathrm{E} 3,-0.176755 \mathrm{E} 3]$
dis $=[-0.237,-1.048,-3.183]$

## References

[1]

## Examples

```
>>> TEOS10_BAW_derivatives(300.0)
(-2.956727474282386e-05, 2.8009736043809844e-07, -2.425992413058737e-09, 3.
\rightarrow 0 7 3 6 9 7 4 3 0 2 7 8 7 5 5 7 e - 1 1 )
```

chemicals.air.TEOS10_CAAW_derivatives( $T$ )
Calculates the third molar virial cross coefficient between air and air-water according to [1].

$$
C_{a a w}(T)=\frac{1}{\left(\bar{\rho}^{*}\right)^{2}} \sum_{i=1}^{5} c_{i}(\theta)^{1-i}
$$

Where $\theta=T / T^{*}$ and $T^{*}=100 \mathrm{~K}$ and $\bar{\rho}=10^{6} \mathrm{~mol} / \mathrm{m}^{\wedge} 3$.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]

## Returns

Caaw [float] Air air-water second molar virial cross coefficient [ $\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2$ ]
dCaaw_dT [float] First temperature derivative of air air-water third molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 6 /\left(\mathrm{mol}^{\wedge} 2^{*} \mathrm{~K}\right)\right]$
d2Caaw_dT2 [float] Second temperature derivative of air air-water third molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 6 /\left(\mathrm{mol}^{\wedge} 2 * \mathrm{~K}^{\wedge} 2\right)\right]$
d3Caaw_dT3 [float] Third temperature derivative of air air-water third molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 6 /\left(\mathrm{mol}^{\wedge} 2 * \mathrm{~K}^{\wedge} 3\right)\right]$

## Notes

The coefficients are as follows:
$\mathrm{cis}=[0.482737 \mathrm{E}-9,1.05678 \mathrm{E}-7,-6.56394 \mathrm{E}-5,0.294442 \mathrm{E}-1,-3.19317]$

## References

[1]

## Examples

```
>>> TEOS10_CAAW_derivatives(300.0)
(8.019777407407409e-10, -1.9610345679012353e-12, 1.700556378600824e-14, -1.
\rightarrow 0 1 2 9 8 2 7 1 6 0 4 9 3 8 3 2 e - 1 6 )
```


## chemicals.air.TEOS10_CAWW_derivatives(T)

Calculates the third molar virial cross coefficient between air and water-water according to [1].

$$
C_{a w w}(T)=\frac{1}{\left(\bar{\rho}^{*}\right)^{2}} \exp \left[\sum_{i=1}^{4} d_{i}(\theta)^{1-i}\right]
$$

Where $\theta=T / T^{*}$ and $T^{*}=100 \mathrm{~K}$ and $\bar{\rho}=10^{6} \mathrm{~mol} / \mathrm{m}^{\wedge} 3$.

## Parameters

T [float] Temperature, [K]

## Returns

Caww [float] Air water-water second molar virial cross coefficient [ $\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2$ ]
dCaww_dT [float] First temperature derivative of air water-water third molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 6 /\left(\mathrm{mol}^{\wedge} 2^{*} \mathrm{~K}\right)\right]$
d2Caww_dT2 [float] Second temperature derivative of air water-water third molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 6 /\left(\mathrm{mol}^{\wedge} 2^{*} \mathrm{~K}^{\wedge} 2\right)\right]$
d3Caww_dT3 [float] Third temperature derivative of air water-water third molar virial cross coefficient $\left[\mathrm{m}^{\wedge} 6 /\left(\mathrm{mol}^{\wedge} 2 * \mathrm{~K}^{\wedge} 3\right)\right]$

## Notes

The coefficients are as follows:
dis $=[-0.10728876 \mathrm{E} 2,0.347802 \mathrm{E} 2,-0.383383 \mathrm{E} 2,0.334060 \mathrm{E} 2]$

## References

[1]

## Examples

```
>>> TEOS10_CAWW_derivatives(300.0)
(-1.1555278368039349e-07, 2.6136327775413448e-09, -7.513345818045024e-11, 2.
๑601834967770415e-12)
```


### 1.3.7 Henry's Law for Air in Water

## chemicals.air.iapws04_Henry_air( $T$ )

Calculate the Henry's law constant of air in water according to the IAPWS-04 standard.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]

## Returns

H [float] Henry's law constant, [1/Pa]

## Notes

The mole fractions of air in this model are $0.7812 \mathrm{~N} 2,0.2095 \mathrm{O} 2$ and 0.0093 Ar .

## References

[1]

## Examples

```
>>> iapws04_Henry_air(320.0)
1.0991553689889531e-10
```

chemicals.air.iapws04_dHenry_air_dT( $T$ )
Calculate the temperature derivative of Henry's law constant of air in water according to the IAPWS-04 standard. As the actual Henry's law constant must be calculated as well, it is also returned.

## Parameters

T [float] Temperature, [K]

## Returns

dH_dT [float] First temperature derivative of Henry's law constant, [1/(Pa*K)]
H [float] Henry's law constant, [1/Pa]

## Notes

The mole fractions of air in this model are $0.7812 \mathrm{~N} 2,0.2095 \mathrm{O} 2$ and 0.0093 Ar .

## References

[1]

## Examples

>>> iapws04_dHenry_air_dT(320.0)
(-8.680064421141611e-13, $1.0991553689889561 \mathrm{e}-10)$

### 1.4 Combustion Calculations (chemicals.combustion)

This module contains a series of functions for modeling combustion reactions.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Combustion Stoichiometry
- Heat of Combustion
- Heat of Combustion and Stiochiometry
- Basic Combustion Spec Solvers
- Engine Combustion
- Lookup Functions


### 1.4.1 Combustion Stoichiometry

chemicals.combustion. combustion_stoichiometry(atoms, MW=None, missing_handling='elemental')
Return a dictionary of stoichiometric coefficients of chemical combustion, given a dictionary of a molecule's constituent atoms and their counts.

This function is based on the combustion of hydrocarbons; the products for some inorganics can be hard to predict, and no special handling is included here for them. This reaction is the standard one at standard pressure with an excess of oxygen; it does not account for partial combustion or nitrous oxides.

## Parameters

atoms [dict[str, int]] Dictionary of atoms and their counts, [-]
MW [float, optional] Molecular weight of chemical, used only if missing_handling is 'Ash', [ $\mathrm{g} / \mathrm{mol}$ ]
missing_handling [str, optional] How to handle compounds which do not appear in the stoichiometric reaction below. If 'elemental', return those atoms in the monatomic state; if 'ash', converts all missing attoms to 'Ash' in the output at a $M W$ of $1 \mathrm{~g} / \mathrm{mol},[-]$

## Returns

stoichiometry [dict[str, float]] Stoichiometric coefficients of combustion. May inlcude the following keys for complete combustion: 'H2O', 'CO2', 'SO2', ' Br 2 ', ' $\mathrm{I2}$ ', ' HCl ', ' HF ' 'P4O10'; if missing_handling is 'elemental' can include the other elements; if missing_handling is 'ash', Ash will be present in the output if the compounds whose reactions are not included here. ' O 2 ' is always present, with negative values indicating oxygen is required. [-]

## Notes

The stoichiometry is given by:

$$
\begin{gathered}
C_{c} H_{h} O_{o} N_{n} S_{s} B r_{b} I_{i} C l_{x} F_{f} P_{p}+k O_{2}->c C O_{2}+\frac{b}{2} B r_{2}+\frac{i}{2} I+x H C l+f H F+s S O_{2}+\frac{n}{2} N_{2}+\frac{p}{4} P_{4} O_{10}+\frac{h+x+f}{2} H_{2} \\
k=c+s+\frac{h}{4}+\frac{5 P}{4}-\frac{x+f}{4}-\frac{o}{2}
\end{gathered}
$$

Also included in the results is the moles of O 2 required per mole of the mixture of the molecule.
HF and HCl are gaseous products in their standard state. P 4 O 10 is a solid in its standard state. Bromine is a liquid as is iodine. Water depends on the chosen definition of heating value. The other products are gases.
Atoms not in ['C', 'H', 'N', 'O', 'S', 'Br', 'I', ' Cl ', ' F ', ' P '] are returned as pure species; i.e. sodium hydroxide produces water and pure Na .

## Examples

Methane gas burning:

```
>>> combustion_stoichiometry({'C': 1, 'H':4})
{'CO2': 1, 'O2': -2.0, 'H2O': 2.0}
```

chemicals.combustion.combustion_products_mixture(atoms_list, zs, reactivities=None, CASs=None, missing_handling='elemental', combustion_stoichiometries=None)
Calculates the combustion products of a mixture of molecules and their, mole fractions; requires a list of dictionaries of each molecule's constituent atoms and their counts. Products for non-hydrocarbons may not be correct, but are still calculated.

## Parameters

atoms_list [list[dict]] List of dictionaries of atoms and their counts, [-]
zs [list[float]] Mole fractions of each molecule in the mixture, [-]
reactivities [list[bool]] Indicators as to whether to combust each molecule, [-]
CASs [list[str]] CAS numbers of all compounds; non-reacted products will appear in the products indexed by their CAS number, [-]
missing_handling [str, optional] How to handle compounds which do not appear in the stoichiometric reaction below. If 'elemental', return those atoms in the monatomic state; if 'Ash', converts all missing attoms to 'Ash' in the output at a $M W$ of $1 \mathrm{~g} / \mathrm{mol}$, [-]
combustion_stoichiometries [list[dict[str, float]]] List of return values from combustion_stoichiometry, can be provided if precomputed [-]

## Returns

combustion_producucts [dict] Dictionary of combustion products and their counts, [-]

## Notes

Also included in the results is the moles of O 2 required per mole of the mixture to be burnt.
Note that if O 2 is in the feed, this will be subtracted from the required O 2 amount.
HF and HCl are gaseous products in their standard state. P 4 O 10 is a solid in its standard state. Bromine is a liquid as is iodine. Water depends on the chosen definition of heating value. The other products are gases.
Note that if instead of mole fractions, mole flows are given - the results are in terms of mole flows as well!

## Examples

Mixture of methane and ethane.

```
>>> combustion_products_mixture([{'H': 4, 'C': 1}, {'H': 6, 'C': 2}, {'Ar': 1}, {'C
๑': 15, 'H': 32}],
... [.9, .05, .04, .01], reactivities=[True, True, True, False],
...CASs=['74-82-8', '74-84-0', '7440-37-1', '629-62-9'])
{'CO2': 1.0, 'O2': -1.975, 'H2O': 1.95000000000000002, 'Ar': 0.04, '629-62-9': 0.01}
```


### 1.4.2 Heat of Combustion

chemicals.combustion.HHV_stoichiometry(stoichiometry, Hf, Hf_chemicals=None)
Return the higher heating value [ HHV ; in $\mathrm{J} / \mathrm{mol}$ ] based on the theoretical combustion stoichiometry and the heat of formation of the chemical.

## Parameters

stoichiometry [dict[str, float]] Stoichiometric coefficients of combustion. May inlcude the following keys: 'H2O', ‘CO2', 'SO2', 'Br2', 'I2', 'HCl', 'HF' and 'P4O10'.

Hf [float] Heat of formation [ $\mathrm{J} / \mathrm{mol}$ ].
Hf_chemicals [dict[str, float]] Heat of formation of chemicals present in stoichiometry, [J/mol]

## Returns

HHV [float] Higher heating value [J/mol].

## Notes

The combustion reaction is based on the following equation:

$$
\begin{gathered}
C_{c} H_{h} O_{o} N_{n} S_{s} B r_{b} I_{i} C l_{x} F_{f} P_{p}+k O_{2}->c C O_{2}+\frac{b}{2} B r_{2}+\frac{i}{2} I+x H C l+f H F+s S O_{2}+\frac{n}{2} N_{2}+\frac{p}{4} P_{4} O_{10}+\frac{h+x+f}{2} H_{2} \\
k=c+s+\frac{h}{4}+\frac{5 P}{4}-\frac{x+f}{4}-\frac{o}{2}
\end{gathered}
$$

The HHV is calculated as the heat of reaction.

## Examples

Burning methane gas:

```
>>> HHV_stoichiometry({'O2': -2.0, 'CO2': 1, 'H2O': 2.0}, -74520.0)
```

-890604.0
chemicals.combustion.HHV_modified_Dulong(mass_fractions)
Return higher heating value [HHV; in J/g] based on the modified Dulong's equation [1].

## Parameters

mass_fractions [dict[str, float]] Dictionary of atomic mass fractions [-].

## Returns

HHV [float] Higher heating value [ $\mathrm{J} / \mathrm{mol}$ ].

## Notes

The heat of combustion in $\mathrm{J} / \mathrm{mol}$ is given by Dulong's equation [1]:

$$
H c(J / m o l)=M W \cdot(338 C+1428(H-O / 8)+95 S)
$$

This equation is only good for <10 wt. \% Oxygen content. Variables C, H, O, and S are atom weight fractions.

## References

[1]

Examples

Dry bituminous coal:

```
>> HHV_modified_Dulong({'C': 0.716, 'H': 0.054, 'S': 0.016, 'N': 0.016, 'O': 0.093,
```

$\rightarrow$ 'Ash': 0.105\})
-304.0395
chemicals.combustion.LHV_from_HHV $\left(H H V, N \_H 2 O\right)$
Return the lower heating value [ LHV ; in $\mathrm{J} / \mathrm{mol}$ ] of a chemical given the higher heating value [ HHV ; in $\mathrm{J} / \mathrm{mol}$ ] and the number of water molecules formed per molecule burned.

## Parameters

HHV [float] Higher heating value [ $\mathrm{J} / \mathrm{mol}$ ].
$\mathbf{N} \_\mathbf{H 2 O}$ [int] Number of water molecules produced [-].

## Returns

LHV [float] Lower heating value [ $\mathrm{J} / \mathrm{mol}$ ].

## Notes

The LHV is calculated as follows:

$$
\begin{gathered}
L H V=H H V+H_{v a p} \cdot H_{2} O \\
H_{v a p}=44011.496 \frac{\mathrm{~J}}{\mathrm{molH}_{2} \mathrm{O}} \\
\mathrm{H}_{2} \mathrm{O}=\frac{\mathrm{molH}_{2} \mathrm{O}}{m o l}
\end{gathered}
$$

## Examples

Methanol lower heat of combustion:

```
>>> LHV_from_HHV(-726024.0, 2)
-638001.008
```


### 1.4.3 Heat of Combustion and Stiochiometry

chemicals.combustion.combustion_data (formula=None, stoichiometry=None, $H f=N o n e, M W=N o n e$, method=None, missing_handling='ash')
Return a CombustionData object (a named tuple) that contains the stoichiometry coefficients of the reactants and products, the lower and higher heating values [LHV, HHV; in J/mol], the heat of formation [Hf; in J/mol], and the molecular weight [MW; in $\mathrm{g} / \mathrm{mol}$ ].

## Parameters

formula [str, or dict[str, float], optional] Chemical formula as a string or a dictionary of atoms and their counts.
stoichiometry [dict[str, float], optional] Stoichiometry of combustion reaction.
Hf [float, optional] Heat of formation of given chemical [J/mol]. Required if method is "Stoichiometry".

MW [float, optional] Molecular weight of chemical [g/mol].
method ["Stoichiometry" or "Dulong", optional] Method to estimate LHV and HHV.
missing_handling [str, optional] How to handle compounds which do not appear in the stoichiometric reaction below. If 'elemental', return those atoms in the monatomic state; if 'Ash', converts all missing attoms to 'Ash' in the output at a $M W$ of $1 \mathrm{~g} / \mathrm{mol},[-]$

## Returns

combustion_data [CombustionData] A combustion data object with the stoichiometric coefficients of combustion, higher heating value, heat of formation, and molecular weight as attributes named stoichiomery, HHV, Hf, and MW, respectively.

## Notes

The combustion reaction is based on the following equation:

$$
\begin{gathered}
C_{c} H_{h} O_{o} N_{n} S_{s} B r_{b} I_{i} C l_{x} F_{f} P_{p}+k O_{2}->c C O_{2}+\frac{b}{2} B r_{2}+\frac{i}{2} I+x H C l+f H F+s S O_{2}+\frac{n}{2} N_{2}+\frac{p}{4} P_{4} O_{10}+\frac{h+x+f}{2} H_{2} \\
k=c+s+\frac{h}{4}+\frac{5 P}{4}-\frac{x+f}{4}-\frac{o}{2}
\end{gathered}
$$

If the method is "Stoichiometry", the HHV is found using through an energy balance on the reaction (i.e. heat of reaction). If the method is "Dulong", Dulong's equation is used [1]:

$$
H c(J / \mathrm{mol})=M W \cdot(338 C+1428(H-O / 8)+95 S)
$$

The LHV is calculated as follows:

$$
\begin{gathered}
L H V=H H V+H_{\text {vap }} \cdot H_{2} \mathrm{O} \\
H_{v a p}=44011.496 \frac{\mathrm{~J}}{\mathrm{molH}_{2} \mathrm{O}} \\
\mathrm{H}_{2} \mathrm{O}=\frac{\mathrm{molH}_{2} \mathrm{O}}{\mathrm{~mol}}
\end{gathered}
$$

## References

[1]

## Examples

Liquid methanol burning:

```
>>> combustion_data({'H': 4, 'C': 1, '0': 1}, Hf=-239100)
CombustionData(stoichiometry={'CO2': 1, 'O2': -1.5, 'H2O': 2.0}, HHV=-726024.0, Hf=-
\hookrightarrow239100, MW=32.04186)
```

class chemicals. combustion. CombustionData(stoichiometry, HHV,Hf,MW)
Return a CombustionData object (a named tuple) that contains the stoichiometry coefficients of the reactants and products, the lower and higher heating values [LHV, HHV; in J/mol], the heat of formation [Hf; in J/mol], and the molecular weight [ MW ; in $\mathrm{g} / \mathrm{mol}$ ].

## Parameters

stoichiometry [dict[str, float]] Stoichiometric coefficients of the reactants and products.
HHV [float] Higher heating value [ $\mathrm{J} / \mathrm{mol}$ ].
Hf [float] Heat of formation [ $\mathrm{J} / \mathrm{mol}$ ].
MW [float] Molecular weight $[\mathrm{g} / \mathrm{mol}$ ].

## Attributes

LHV Lower heating value [LHV; in J/mol]

### 1.4.4 Basic Combustion Spec Solvers

chemicals.combustion.fuel_air_spec_solver(zs_air, zs_fuel, CASs, atomss, $n$ _fuel=None, $n \_a i r=N o n e$, n_out=None, O2_excess=None, frac_out_O2=None, frac_out_O2_dry=None, ratio=None, Vm_air=None, Vm_fuel=None, MW_air=None, $M W$ _fuel=None, ratio_basis='mass', reactivities=None, combustion_stoichiometries=None)
Solves the system of equations describing a flow of air mixing with a flow of combustibles and burning completely. All calculated variables are returned as a dictionary.

Supports solving with any 2 of the extensive variables, or one extensive and one intensive variable:
Extensive variables:

- n_air
- n_fuel
- n_out

Intensive variables:

- O2_excess
- frac_out_O2
- frac_out_O2_dry
- ratio

The variables $V m \_$air, Vm_fuel, $M W_{\_}$air, and $M W_{-}$fuel are only required when an air-fuel ratio is given. Howver, the ratios cannot be calculated for the other solve options without them.

## Parameters

zs_air [list[float]] Mole fractions of the air; most not contain any combustibles, [-]
zs_fuel [list[float]] Mole fractions of the fuel; can contain inerts and/or oxygen as well, [-]
CASs [list[str]] CAS numbers of all compounds, [-]
atomss [list[dict[float]]] List of dictionaries of elements and their counts for all molecules in the mixtures, [-]
n_fuel [float, optional] Flow rate of fuel, [ $\mathrm{mol} / \mathrm{s}$ ]
n_air [float, optional] Flow rate of air, [ $\mathrm{mol} / \mathrm{s}$ ]
n_out [float, optional] Flow rate of combustion products, remaining oxygen, and inerts, [ $\mathrm{mol} / \mathrm{s}$ ]
O2_excess [float, optional] The excess oxygen coming out; (O2 in)/(O2 required) - 1, [-]
frac_out_O2 [float, optional] The mole fraction of oxygen out, [-]
frac_out_O2_dry [float, optional] The mole fraction of oxygen out on a dry basis, [-]
ratio [float, optional] Air-fuel ratio, in the specified basis, [-]
Vm_air [float, optional] Molar volume of air, [m^3/mol]
Vm_fuel [float, optional] Molar volume of fuel, [m^3/mol]
MW_air [float, optional] Molecular weight of air, [ $\mathrm{g} / \mathrm{mol}$ ]
MW_fuel [float, optional] Molecular weight of fuel, $[\mathrm{g} / \mathrm{mol}$ ]
ratio_basis [str, optional] One of 'mass', 'mole', or 'volume', [-]
reactivities [list[bool], optional] Optional list which can be used to mark otherwise combustible compounds as incombustible and which will leave unreacted, [-]
combustion_stoichiometries [list[dict[str, float]]] List of return values from combustion_stoichiometry, can be provided if precomputed [-]

## Returns

results [dict]

- n_fuel : Flow rate of fuel, [ $\mathrm{mol} / \mathrm{s}$ ]
- $n \_$air : Flow rate of air, [ $\mathrm{mol} / \mathrm{s}$ ]
- n_out : Flow rate of combustion products, remaining oxygen, and inerts, [ $\mathrm{mol} / \mathrm{s}$ ]
- O2_excess : The excess oxygen coming out; (O2 in)/(O2 required) - 1, [-]
- frac_out_O2 : The mole fraction of oxygen out, [-]
- frac_out_O2_dry : The mole fraction of oxygen out on a dry basis, [-]
- mole_ratio : Air-fuel mole ratio, [-]
- mass_ratio : Air-fuel mass ratio, [-]
- volume_ratio : Air-fuel volume ratio, [-]
- ns_out : Mole flow rates out, [ $\mathrm{mol} / \mathrm{s}$ ]
- zs_out : Mole fractions out, [-]


## Notes

Combustion products themselves cannot be set as unreactive.
The function works so long as the flow rates, molar volumes, and molecular weights are in a consistent basis.
The function may also be used to obtain the other ratios, even if both flow rates are known.
Be careful to use standard volumes if the ratio known is at standard conditions!

## Examples

```
>>> zs_air = [0.79, 0.205, 0, 0, 0, 0.0045, 0.0005]
>>> zs_fuel = [0.025, 0.025, 0.85, 0.07, 0.029, 0.0005, 0.0005]
>>> CASs = ['7727-37-9', '7782-44-7', '74-82-8', '74-84-0', '74-98-6', '7732-18-5',
    ->'124-38-9']
>>> atomss = [{'N': 2}, {'O': 2}, {'H': 4, 'C': 1}, {'H': 6, 'C': 2}, {'H': 8, 'C':ь
\hookrightarrow3}, {'H': 2, 'O': 1}, {'C': 1, 'O': 2}]
>>> ans = fuel_air_spec_solver(zs_air=zs_air, zs_fuel=zs_fuel, CASs=CASs,,
->atomss=atomss, n_fuel=5.0, 02_excess=0.3, Vm_air=0.02493, Vm_fuel=0.02488, MW_
air=28.79341351, MW_fuel=18.55158039)
>>> [round(i, 5) for i in ans['ns_out']]
[51.99524, 3.135, 0.0, 0.0, 0.0, 10.42796, 5.42033]
>>> [round(i, 5) for i in ans['zs_out']]
[0.73255, 0.04417, 0.0, 0.0, 0.0, 0.14692, 0.07637]
>>> ans['frac_out_02'], ans['frac_out_02_dry']
(0.04416828172034148, 0.051774902132807)
>>> ans['mole_ratio'], ans['mass_ratio'], ans['volume_ratio']
```

(13.131707317073175, 20.381372957130615, 13.15809740412517)
>>> ans['n_air']
65.65853658536588
chemicals.combustion. combustion_spec_solver (zs_air, zs_fuel, zs_third, CASs, atomss, $n \_t h i r d$, n_fuel=None, $n$ _air=None, $n \_$out $=$None, O2_excess=None, frac_out_O2=None, frac_out_O2_dry=None, ratio=None, Vm_air=None, Vm_fuel=None, Vm_third=None, $M W \_$air $=$None, $M W_{-}$fuel=None, $M W$ _third=None, ratio_basis='mass', reactivities $=$ None, combustion_stoichiometries=None)
Solves the system of equations describing a flow of air mixing with two flow of combustibles, one fixed and one potentially variable, and burning completely. All calculated variables are returned as a dictionary.

The variables Vm_air, Vm_fuel, Vm_third, $M W \_$air, $M W_{-}$fuel and $M W \_$third are only required when an air-fuel ratio is given. Howver, the ratios cannot be calculated for the other solve options without them.

## Parameters

zs_air [list[float]] Mole fractions of the air; most not contain any combustibles, [-]
zs_fuel [list[float]] Mole fractions of the fuel; can contain inerts and/or oxygen as well, [-]
zs_third [list[float]]
Mole fractions of the fixed fuel flow; can contain inerts and/or oxygen as well, [-]
CASs [list[str]] CAS numbers of all compounds, [-]
atomss [list[dict[float]]] List of dictionaries of elements and their counts for all molecules in the mixtures, [-]
n_third [float, optional] Flow rate of third stream, (fixed) fuel flow rate, [ $\mathrm{mol} / \mathrm{s}$ ]
n_fuel [float, optional] Flow rate of fuel, [ $\mathrm{mol} / \mathrm{s}$ ]
n_air [float, optional] Flow rate of air, [ $\mathrm{mol} / \mathrm{s}$ ]
n_out [float, optional] Flow rate of combustion products, remaining oxygen, and inerts, [ $\mathrm{mol} / \mathrm{s}$ ]
O2_excess [float, optional] The excess oxygen coming out; (O2 in)/(O2 required) - 1, [-]
frac_out_O2 [float, optional] The mole fraction of oxygen out, [-]
frac_out_O2_dry [float, optional] The mole fraction of oxygen out on a dry basis, [-]
ratio [float, optional] Air-fuel ratio, in the specified basis, [-]
Vm_air [float, optional] Molar volume of air, [m^3/mol]
Vm_fuel [float, optional] Molar volume of fuel, [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]
Vm_third [float, optional] Molar volume of second fuel stream, [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]
MW_air [float, optional] Molecular weight of air, [ $\mathrm{g} / \mathrm{mol}$ ]
MW_fuel [float, optional] Molecular weight of fuel, $[\mathrm{g} / \mathrm{mol}$ ]
MW_third [float, optional] Molecular weight of second fuel stream, $[\mathrm{g} / \mathrm{mol}]$
ratio_basis [str, optional] One of 'mass', 'mole', or 'volume', [-]
reactivities [list[bool], optional] Optional list which can be used to mark otherwise combustible compounds as incombustible and which will leave unreacted, [-]
combustion_stoichiometries [list[dict[str, float]]] List of return values from combustion_stoichiometry, can be provided if precomputed [-]

## Returns

results [dict]

- $\mathrm{n} \_$fuel : Flow rate of fuel, $[\mathrm{mol} / \mathrm{s}]$
- n_air : Flow rate of air, [ $\mathrm{mol} / \mathrm{s}$ ]
- $n \_$out : Flow rate of combustion products, remaining oxygen, and inerts, [ $\mathrm{mol} / \mathrm{s}$ ]
- O2_excess : The excess oxygen coming out; ( O 2 in )/(O2 required) - 1, [-]
- frac_out_O2 : The mole fraction of oxygen out, [-]
- frac_out_O2_dry : The mole fraction of oxygen out on a dry basis, [-]
- mole_ratio : Air-fuel mole ratio, [-]
- mass_ratio : Air-fuel mass ratio, [-]
- volume_ratio : Air-fuel volume ratio, [-]
- ns_out : Mole flow rates out, [ $\mathrm{mol} / \mathrm{s}$ ]
- zs_out : Mole fractions out, [-]


## Notes

Combustion products themselves cannot be set as unreactive.
The function works so long as the flow rates, molar volumes, and molecular weights are in a consistent basis.
Handling the case of the air feed containing combustibles is not implemented.

## Examples

```
>>> zs_air = [0.79, 0.205, 0, 0, 0, 0.0045, 0.0005]
>>> zs_fuel = [0.025, 0.025, 0.85, 0.07, 0.029, 0.0005, 0.0005]
>>> zs_third = [0.1, 0.005, 0.5, 0.39, 0, 0.005, 0]
>>> CASs = ['7727-37-9', '7782-44-7', '74-82-8', '74-84-0', '74-98-6', '7732-18-5',
\hookrightarrow'124-38-9']
>>> atomss = [{'N': 2}, {'O': 2}, {'H': 4, 'C': 1}, {'H': 6, 'C': 2}, {'H': 8, 'C':ь
    3}, {'H': 2, 'O': 1}, {'C': 1, 'O': 2}]
>>> combustion_stoichiometries = [combustion_stoichiometry(atoms) for atoms in
\rightarrow \text { atomss]}
>>> ans = combustion_spec_solver(zs_air=zs_air, zs_fuel=zs_fuel, zs_third=zs_third,
CASs=CASs, atomss=atomss, n_third=1.0, n_fuel=5.0, 02_excess=0.3, Vm_air=0.02493,_
\hookrightarrowm__fuel=0.02488, Vm_third=.024, MW_air=28.79341351, MW_fuel=18.55158039, MW_
third=22.0)
>>> ans['n_air']
80.6317073170732
```

chemicals.combustion.air_fuel_ratio_solver(ratio, Vm_air, Vm_fuel, MW_air, MW_fuel, $n \_a i r=N o n e$, n_fuel=None, basis='mass')
Calculates molar flow rate of air or fuel from the other, using a specified air-fuel ratio. Supports 'mole', 'mass', and 'volume'.
bases for the ratio variable. The ratio must be of the same units - i.e. $\mathrm{kg} / \mathrm{kg}$ instead $\mathrm{of} \mathrm{lb} / \mathrm{kg}$.
The mole, mass, and volume air-fuel ratios are calculated in the process and returned as well.

## Parameters

ratio [float] Air-fuel ratio, in the specified basis, [-]
Vm_air [float] Molar volume of air, [m^3/mol]
Vm_fuel [float] Molar volume of fuel, [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]
MW_air [float] Molecular weight of air, [ $\mathrm{g} / \mathrm{mol}$ ]
MW_fuel [float] Molecular weight of fuel, [ $\mathrm{g} / \mathrm{mol}$ ]
n_air [float, optional] Molar flow rate of air, [ $\mathrm{mol} / \mathrm{s}$ ]
n_fuel [float, optional] Molar flow rate of fuel, $[\mathrm{mol} / \mathrm{s}$ ]
basis [str, optional] One of 'mass', 'mole', or 'volume', [-]

## Returns

n_air [float] Molar flow rate of air, [ $\mathrm{mol} / \mathrm{s}$ ]
n_fuel [float] Molar flow rate of fuel, [ $\mathrm{mol} / \mathrm{s}$ ]
mole_ratio [float] Air-fuel mole ratio, [-]
mass_ratio [float] Air-fuel mass ratio, [-]
volume_ratio [float] Air-fuel volume ratio, [-]

## Notes

The function works so long as the flow rates, molar volumes, and molecular weights are in a consistent basis.
The function may also be used to obtain the other ratios, even if both flow rates are known.
Be careful to use standard volumes if the ratio known is at standard conditions!
This function has no provision for mixed units like mass/mole or volume/mass.

## Examples

```
>>> Vm_air = 0.024936627188566596
>>> Vm_fuel = 0.024880983160354486
>>> MW_air = 28.850334
>>> MW_fuel = 17.86651
>> n_fuel = 5.0
>> n_air = 25.0
>>> air_fuel_ratio_solver(ratio=5.0, Vm_air=Vm_air, Vm_fuel=Vm_fuel,
... MW_air=MW_air, MW_fuel=MW_fuel, n_air=n_air,
.:. n_fuel=n_fuel, basis='mole')
(25.0, 5.0, 5.0, 8.073858296891782, 5.011182039683378)
```


### 1.4.5 Engine Combustion

chemicals.combustion.Perez_Boehman_RON_from_ignition_delay(ignition_delay)
Esimates the research octane number (RON) from a known ignition delay, as shown in [1].

$$
\mathrm{RON}=120.77-\frac{425.48}{\tau_{I D}}
$$

In the above equation, ignition delay is in ms.

## Parameters

ignition_delay [float] The ignition delay, [ s ]

## Returns

RON [float] Research Octane Number [-]

## Notes

The correlation was developed using 20 components, for a range of approximately 3.6 ms to 67 ms .

## References

[1]

Examples
>>> Perez_Boehman_RON_from_ignition_delay(1/150)
56.948
chemicals.combustion.Perez_Boehman_MON_from_ignition_delay(ignition_delay)
Esimates the motor octane number (MON) from a known ignition delay, as shown in [1].

$$
\mathrm{MON}=109.93-\frac{374.73}{\tau_{I D}}
$$

In the above equation, ignition delay is in ms .

## Parameters

ignition_delay [float] The ignition delay, [s]

## Returns

MON [float] Motor Octane Number [-]

## Notes

The correlation was developed using 20 components, for a range of approximately 3.6 ms to 67 ms .

## References

[1]

## Examples

>>> Perez_Boehman_MON_from_ignition_delay(1/150)
53.7205
chemicals.combustion.octane_sensitivity (RON, MON)
This function calculates the octane sensitivity of a fuel [1].

$$
\mathrm{OS}=\mathrm{RON}-\mathrm{MON}
$$

## Parameters

RON [float] Research octane number, [-]
MON [float] Motor octane number, [-]

## Returns

OS [float] Octane sensitivity, [-]

## References

[1]

## Examples

>>> octane_sensitivity(RON=90, MON=74)
16
chemicals.combustion. AKI ( $\mathrm{RON}, \mathrm{MON}$ )
This function calculates the anti knock index (AKI) of a fuel, also known as ( $\mathrm{R}+\mathrm{M}$ )/2 and by DON [1].

$$
\mathrm{AKI}=0.5 \mathrm{RON}+0.5 \mathrm{MON}
$$

## Parameters

RON [float] Research octane number, [-]
MON [float] Motor octane number, [-]

## Returns

AKI [float] Average of RON and MON, [-]

## Notes

This is the number displayed at the gas pumps in North America; in Europe and Asia the RON is displayed.

## References

[1]

## Examples

>>> AKI (RON=90, MON=74)
82.0
chemicals.combustion.IDT_to_DCN(IDT)
This function converts the ignition delay time [1] into a derived cetane number.
If the ignition delay time is between 3.1 and 6.5 ms :

$$
\mathrm{DCN}=4.46+\frac{186.6}{\mathrm{IDT}}
$$

Otherwise:

$$
\mathrm{DCN}=\left(83.99(\mathrm{IDT}-1.512)^{-0.658}\right)+3.547
$$

## Parameters

IDT [float] Ignition delay time, [s]

## Returns

DCN [float] Derived cetane number, [-]

## Notes

This conversion is described in D6890-168.

## References

[1], [2]

Examples
>>> IDT_to_DCN(4e-3)
51.11

### 1.4.6 Lookup Functions

chemicals.combustion.RON(CASRN, method=None)
This function handles the retrieval of a chemical's research octane number (RON). Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 1400 chemicals.

## Parameters

CASRN [str] CASRN [-]

## Returns

RON [float] Research octane number, [-]

## Other Parameters

method [string, optional] A string for the method name to use, as defined by constants in RON_methods

## Notes

The available sources are as follows:

- 'FLORIAN_LIMING', the experimental values compiled in [1].
- 'FLORIAN_LIMING_ANN', a set of predicted values using a QSPR-ANN model developed in the author's earlier publication [3], from 260 comonents.
- 'COMBUSTDB', a compilation of values from various sources [2].
- 'COMBUSTDB_PREDICTIONS', a set of predicted values developed by the author of CombustDB (Travis Kessler) using the tool [4].


## References

[1], [2], [3], [4]

## Examples

```
>>> RON(CASRN='64-17-5')
```

108.6
chemicals.combustion.RON_methods (CASRN)
Return all methods available to obtain the research octane number (RON) for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain the RON with the given inputs.

## See also:

RON

```
chemicals.combustion.RON_all_methods = ('FLORIAN_LIMING', 'COMBUSTDB',
```

'FLORIAN_LIMING_ANN', 'COMBUSTDB_PREDICTIONS')

Tuple of method name keys. See the RON for the actual references
chemicals.combustion.MON (CASRN, method=None)
This function handles the retrieval of a chemical's motor octane number (MON). Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 1400 chemicals.

## Parameters

CASRN [str] CASRN [-]

## Returns

MON [float] Research octane number, [-]

## Other Parameters

method [string, optional] A string for the method name to use, as defined by constants in MON_methods

## Notes

The available sources are as follows:

- 'FLORIAN_LIMING', the experimental values compiled in [1].
- 'FLORIAN_LIMING_ANN', a set of predicted values using a QSPR-ANN model developed in the author's earlier publication [3], from 260 comonents.
- 'COMBUSTDB', a compilation of values from various sources [2].
- ‘COMBUSTDB_PREDICTIONS', a set of predicted values developed by the author of CombustDB (Travis Kessler) using the tool [4].


## References

[1], [2], [3], [4]

## Examples

>>> MON(CASRN='64-17-5')
89.7
chemicals.combustion.MON_methods(CASRN)
Return all methods available to obtain the motor octane number (MON) for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain the MON with the given inputs.

## See also:

MON
chemicals.combustion.MON_all_methods = ('FLORIAN_LIMING', 'COMBUSTDB',
'FLORIAN_LIMING_ANN', 'COMBUSTDB_PREDICTIONS')
Tuple of method name keys. See the MON for the actual references
chemicals.combustion.ignition_delay (CASRN, method=None)
This function handles the retrieval of a chemical's ignition delay time (IDT). Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 60 chemicals.

## Parameters

CASRN [str] CASRN [-]

## Returns

ignition_delay [float] Ignition delay time, [s]

## Other Parameters

method [string, optional] A string for the method name to use, as defined by constants in ignition_delay_all_methods

## Notes

The available sources are as follows:

- 'DAHMEN_MARQUARDT', the experimental values compiled in [1]; all timings come from the IQT tester device

Note that different measurement devices can give different results.

## References

[1]

## Examples

```
>>> ignition_delay(CASRN='110-54-3')
0.0043
```

chemicals.combustion.ignition_delay_methods(CASRN)
Return all methods available to obtain the ignition delay time (IDT) for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain the IDT with the given inputs.

## See also:

ignition_delay

```
chemicals.combustion.ignition_delay_all_methods = ('DAHMEN_MARQUARDT',)
```

Tuple of method name keys. See the ignition_delay for the actual references

### 1.5 Critical Properties (chemicals.critical)

This module contains lookup functions for critical temperature, critical pressure, critical volume, and critical compressibility factors. It also includes a few relationships between the critical properties, and a variety of critical mixture property estimation routines.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Critical Temperature
- Critical Pressure
- Critical Volume
- Critical Compressibility Factor
- Critical Property Relationships
- Critical Temperature of Mixtures
- Critical Volume of Mixtures


### 1.5.1 Critical Temperature

## chemicals.critical.Tc(CASRN, method=None)

This function handles the retrieval of a chemical's critical temperature. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 26000 chemicals.

## Parameters

## CASRN [str] CASRN [-]

## Returns

Tc [float] Critical temperature, [K]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'IUPAC', 'MATTHEWS', ‘CRC', 'PD', ‘WEBBOOK', ‘PSRK', ‘PINAMARTINES', 'YAWS', 'WILSON_JASPERSON', 'JOBACK', 'HEOS'. All valid values are also held in the list Tc_all_methods.

See also:
Tc_methods

## Notes

The available sources are as follows:

- 'IUPAC', a series of critically evaluated experimental datum for organic compounds in [1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], and [12].
- 'MATTHEWS', a series of critically evaluated data for inorganic compounds in [13].
- 'CRC', a compillation of critically evaluated data by the TRC as published in [14].
- 'PSRK', a compillation of experimental and estimated data published in [15].
- 'PD', an older compillation of data published in [16]
- 'YAWS', a large compillation of data from a variety of sources; no data points are sourced in the work of [17].
- 'WEBBOOK', a NIST resource [18] containing mostly experimental and averaged values
- 'JOBACK', an estimation method for organic substances in [19]
- 'WILSON_JASPERSON', an estimation method in [21]
- 'PINAMARTINES', a series of values in the supporting material of [20]
- 'HEOS’, a series of values from the NIST REFPROP Database for Highly Accurate Properties of Industrially Important Fluids (and other high-precision fundamental equations of state)


## References

[1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], [12], [13], [14], [15], [16], [17], [18], [19], [20], [21], [22]

## Examples

```
>>> Tc(CASRN='64-17-5')
```

514.71

## chemicals.critical.Tc_methods(CASRN)

Return all methods available to obtain the critical temperature for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain Tc with the given inputs.

## See also:

## TC

```
chemicals.critical.Tc_all_methods = ('HEOS', 'IUPAC', 'MATTHEWS', 'CRC', 'PD', 'WEBBOOK',
'PSRK', 'PINAMARTINES', 'YAWS', 'WILSON_JASPERSON', 'JOBACK')
Tuple of method name keys. See the \(T c\) for the actual references
```

chemicals.critical.Tc_all_method_types = \{'CRC': 'PROCESSED_EXPERIMENTAL', 'HEOS':
'EXPERIMENTAL_REVIEW', 'IUPAC': 'EXPERIMENTAL_REVIEW', 'JOBACK': 'PREDICTED_GC',
'MATTHEWS': 'EXPERIMENTAL_COMPILATION', 'PD': 'EXPERIMENTAL_COMPILATION_SECONDARY',
'PINAMARTINES': 'PROCESSED_EXPERIMENTAL_PREDICTED_SECONDARY', 'PSRK':
'PROCESSED_EXPERIMENTAL_PREDICTED', 'WEBBOOK': 'PROCESSED_EXPERIMENTAL',
'WILSON_JASPERSON': 'PREDICTED_GC', 'YAWS': 'PROCESSED_EXPERIMENTAL_PREDICTED'\}

### 1.5.2 Critical Pressure

## chemicals.critical.Pc(CASRN, method=None)

This function handles the retrieval of a chemical's critical pressure. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 26000 chemicals.

## Parameters

## CASRN [str] CASRN [-]

## Returns

Pc [float] Critical pressure, $[\mathrm{Pa}$ ]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'IUPAC', 'MATTHEWS', 'CRC', 'PD', 'WEBBOOK', ‘PSRK', ‘PINAMARTINES', 'YAWS', 'WILSON_JASPERSON', 'JOBACK', 'HEOS'. All valid values are also held in the list Pc_all_methods.

See also:
Pc_methods

## Notes

The available sources are as follows:

- 'IUPAC', a series of critically evaluated experimental datum for organic compounds in [1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], and [12].
- 'MATTHEWS', a series of critically evaluated data for inorganic compounds in [13].
- 'CRC', a compillation of critically evaluated data by the TRC as published in [14].
- 'PSRK', a compillation of experimental and estimated data published in [15].
- 'PD', an older compillation of data published in [16]
- 'YAWS', a large compillation of data from a variety of sources; no data points are sourced in the work of [17].
- 'WEBBOOK', a NIST resource [18] containing mostly experimental and averaged values
- 'JOBACK', an estimation method for organic substances in [19]
- 'PINAMARTINES', a series of values in the supporting material of [20]
- 'WILSON_JASPERSON', an estimation method in [21]
- 'HEOS', a series of values from the NIST REFPROP Database for Highly Accurate Properties of Industrially Important Fluids (and other high-precision fundamental equations of state)


## References

[1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], [12], [13], [14], [15], [16], [17], [18], [19], [20], [21], [22]

## Examples

>>> Pc(CASRN='64-17-5')
6268000.0

## chemicals.critical.Pc_methods(CASRN)

Return all methods available to obtain the critical pressure for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain Pc with the given inputs.

## See also:

Pc
chemicals.critical.Pc_all_methods = ('HEOS', 'IUPAC', 'MATTHEWS', 'CRC', 'PD', 'WEBBOOK', 'PSRK', 'PINAMARTINES', 'YAWS', 'WILSON_JASPERSON', 'JOBACK')

Tuple of method name keys. See the $P c$ for the actual references

### 1.5.3 Critical Volume

chemicals.critical.Vc(CASRN, method=None)
This function handles the retrieval of a chemical's critical volume. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Preferred sources are 'IUPAC' for organic chemicals, and 'MATTHEWS' for inorganic chemicals. Function has data for approximately 25000 chemicals.

## Parameters

CASRN [str] CASRN [-]

## Returns

Vc [float] Critical volume, [m^3/mol]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'IUPAC', 'MATTHEWS', ‘CRC', 'WEBBOOK', 'PSRK', 'PINAMARTINES', 'YAWS', 'FEDORS', 'JOBACK', 'HEOS'. All valid values are also held in the list Vc_all_methods.
See also:
Vc_methods

## Notes

The available sources are as follows:

- 'IUPAC', a series of critically evaluated experimental datum for organic compounds in [1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], and [12].
- 'MATTHEWS', a series of critically evaluated data for inorganic compounds in [13].
- 'CRC', a compillation of critically evaluated data by the TRC as published in [14].
- 'PSRK', a compillation of experimental and estimated data published in [15].
- 'YAWS', a large compillation of data from a variety of sources; no data points are sourced in the work of [16].
- 'WEBBOOK', a NIST resource [17] containing mostly experimental and averaged values
- 'JOBACK', an estimation method for organic substances in [18]
- 'FEDORS', an estimation methid in [20]
- 'PINAMARTINES', a series of values in the supporting material of [19]
- 'HEOS', a series of values from the NIST REFPROP Database for Highly Accurate Properties of Industrially Important Fluids (and other high-precision fundamental equations of state)


## References

[1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], [12], [13], [14], [15], [16], [17], [18], [19], [20], [21]

## Examples

```
>>> Vc(CASRN='64-17-5')
0.000168634064081
```

chemicals.critical.Vc_methods (CASRN)
Return all methods available to obtain the critical volume for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain Vc with the given inputs.

## See also:

Vc

```
chemicals.critical.Vc_all_methods = ('HEOS', 'IUPAC', 'MATTHEWS', 'CRC', 'WEBBOOK',
'PSRK', 'PINAMARTINES', 'YAWS', 'FEDORS', 'JOBACK')
```

Tuple of method name keys. See the $V c$ for the actual references
chemicals.critical.Mersmann_Kind_predictor_(atoms, coeff $=3.645$, power $=0.5$, covalent_radii=\{'Br': 1.14, 'C': 0.77, 'Cl': 0.99, 'F': 0.71, 'H': 0.37, 'I': 1.33, 'N': 0.71, 'O': 0.6, 'S': 1.04, 'Si': 1.17〕)
Predicts the critical molar volume of a chemical based only on its atomic composition according to [1] and [2]. This is a crude approach, but provides very reasonable estimates in practice. Optionally, the coeff used and the
power in the fraction as well as the atomic contributions can be adjusted; this method is general and atomic contributions can be regressed to predict other properties with this routine.

$$
\begin{array}{r}
\frac{\left(\frac{V_{c}}{n_{a} N_{A}}\right)^{1 / 3}}{d_{a}}=\frac{3.645}{\left(\frac{r_{a}}{r_{H}}\right)^{1 / 2}} \\
r_{a}=d_{a} / 2 \\
d_{a}=2 \frac{\sum_{i}\left(n_{i} r_{i}\right)}{n_{a}}
\end{array}
$$

In the above equations, $n_{i}$ is the number of atoms of species $i$ in the molecule, $r_{i}$ is the covalent atomic radius of the atom, and $n_{a}$ is the total number of atoms in the molecule.

## Parameters

atoms [dict] Dictionary of atoms and their counts, [-]
coeff [float, optional] Coefficient used in the relationship, [m^2]
power [float, optional] Power applied to the relative atomic radius, [-]
covalent_radii [dict or indexable, optional] Object which can be indexed to atomic contrinbutions (by symbol), [-]

## Returns

Vc [float] Predicted critical volume of the chemical, [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]

## Notes

Using the chemicals.elements.periodic_table covalent radii (from RDKit), the coefficient and power should be 4.261206523632586 and 0.5597281770786228 respectively for best results.

## References

[1], [2]

## Examples

Prediction of critical volume of decane:

```
>>> Mersmann_Kind_predictor({'C': 10, 'H': 22})
0.0005851858957767497
```

This is compared against the experimental value, 0.000624 (a $6.2 \%$ relative error)
Using custom fitted coefficients we can do a bit better:

```
>>> from chemicals.critical import rcovs_regressed
>>> Mersmann_Kind_predictor({'C': 10, 'H': 22}, coeff=4.261206523632586,
... power=0.5597281770786228, covalent_radii=rcovs_regressed)
0.0005956870915974391
```

The relative error is only $4.5 \%$ now. This is compared to an experimental uncertainty of $5.6 \%$.
Evaluating 1321 critical volumes in the database, the average relative error is $5.0 \%$; standard deviation $6.8 \%$; and worst value of $79 \%$ relative error for phosphorus.

### 1.5.4 Critical Compressibility Factor

chemicals.critical.Zc (CASRN, method=None)
This function handles the retrieval of a chemical's critical compressibility. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Preferred sources are 'IUPAC' for organic chemicals, and 'MATTHEWS' for inorganic chemicals. Function has data for approximately 25000 chemicals.

## Parameters

CASRN [str] CASRN [-]
Returns
Zc [float] Critical compressibility, [-]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'IUPAC', 'MATTHEWS', 'CRC', 'PSRK', 'YAWS', 'HEOS'. All valid values are also held in Zc_all_methods.

## See also:

Zc_methods

## Notes

The available sources are as follows:

- 'IUPAC', a series of critically evaluated experimental datum for organic compounds in [1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], and [12].
- 'MATTHEWS', a series of critically evaluated data for inorganic compounds in [13].
- 'CRC', a compillation of critically evaluated data by the TRC as published in [14].
- 'PSRK', a compillation of experimental and estimated data published in [15].
- 'YAWS', a large compillation of data from a variety of sources; no data points are sourced in the work of [16].
- 'WEBBOOK', a NIST resource [17] containing mostly experimental and averaged values
- 'JOBACK', an estimation method for organic substances in [18]
- 'PINAMARTINES', a series of values in the supporting material of [19]
- 'HEOS', a series of values from the NIST REFPROP Database for Highly Accurate Properties of Industrially Important Fluids (and other high-precision fundamental equations of state)


## References

[1], [2], [3], [4], [5], [6], [7], [8], [9], [10], [11], [12], [13], [14], [15], [16], [17], [18], [19], [20]

## Examples

```
>>> Zc(CASRN='64-17-5')
```

0.247

## chemicals.critical.Zc_methods(CASRN)

Return all methods available to obtain the critical compressibility for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain Zc with the given inputs.

## See also:

Zc

```
chemicals.critical.Zc_all_methods = ('HEOS', 'IUPAC', 'MATTHEWS', 'CRC', 'WEBBOOK',
```

'PSRK', 'PINAMARTINES', 'YAWS', 'JOBACK')

Tuple of method name keys. See the $Z c$ for the actual references

### 1.5.5 Critical Property Relationships

chemicals.critical.critical_surface $(T c=$ None, $P c=N o n e, V c=N o n e$, method $=$ None $)$
Function for calculating a critical property of a substance from its other two critical properties. Calls functions Ihmels, Meissner, and Grigoras, each of which use a general 'Critical surface' type of equation. Limited accuracy is expected due to very limited theoretical backing.

## Parameters

Tc [float] Critical temperature of fluid (optional) [K].
Pc [float] Critical pressure of fluid (optional) [Pa].
Vc [float] Critical volume of fluid (optional) [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ].
method [string] Request calculation uses the requested method.

## Returns

Tc, Pc or Vc [float] Critical property of fluid $[\mathrm{K}],[\mathrm{Pa}]$, or $\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]$.

## See also:

critical_surface_methods_methods

## Examples

Decamethyltetrasiloxane [141-62-8]
>>> critical_surface(Tc=599.4, Pc=1.19E6, method='IHMELS')
0.0010927333333333334
chemicals.critical.critical_surface_methods(Tc=None, $P c=N o n e, V c=N o n e)$
Return all methods available to obtain the third critial property for the desired chemical.

## Parameters

Tc [float] Critical temperature of fluid (optional) [K].
Pc [float] Critical pressure of fluid (optional) [Pa].
Vc [float] Critical volume of fluid (optional) [ $\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]$.

## Returns

methods [list[str]] Methods which can be used to obtain the third critical property with the given inputs.

## See also:

critical_surface
chemicals.critical.critical_surface_all_methods = ('IHMELS', 'MEISSNER', 'GRIGORAS')
Built-in immutable sequence.
If no argument is given, the constructor returns an empty tuple. If iterable is specified the tuple is initialized from iterable's items.

If the argument is a tuple, the return value is the same object.

## chemicals.critical.third_property (CASRN=None, $T=$ False, $P=$ False, $V=$ False)

Function for calculating a critical property of a substance from its other two critical properties, but retrieving the actual other critical values for convenient calculation. Calls functions Ihmels, Meissner, and Grigoras, each of which use a general 'Critical surface' type of equation. Limited accuracy is expected due to very limited theoretical backing.

## Parameters

CASRN [str] The CAS number of the desired chemical
T [bool] Estimate critical temperature
$\mathbf{P}$ [bool] Estimate critical pressure
V [bool] Estimate critical volume

## Returns

Tc, Pc or Vc [float] Critical property of fluid [K], [Pa], or [m^3/mol]

## Examples

Decamethyltetrasiloxane [141-62-8]

```
>>> third_property('141-62-8', V=True)
```

0.001135732

Succinic acid [110-15-6]
>>> third_property('110-15-6', P=True)
6095016.233766234

## chemicals.critical.Ihmels( $T c=$ None, $P c=$ None, $V c=$ None $)$

Most recent, and most recommended method of estimating critical properties from each other. Two of the three properties are required. This model uses the "critical surface", a general plot of Tc vs Pc vs Vc. The model used 421 organic compounds to derive equation. The general equation is in [1]:

$$
P_{c}=-0.025+2.215 \frac{T_{c}}{V_{c}}
$$

## Parameters

Tc [float] Critical temperature of fluid (optional) [K]
Pc [float] Critical pressure of fluid (optional) [Pa]
Vc [float] Critical volume of fluid (optional) [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]

## Returns

Tc, Pc or Vc [float] Critical property of fluid [K], [Pa], or [m^3/mol]

## Notes

The prediction of Tc from Pc and Vc is not tested, as this is not necessary anywhere, but it is implemented. Internal units are MPa, $\mathrm{cm}^{\wedge} 3 / \mathrm{mol}$, and K . A slight error occurs when $\mathrm{Pa}, \mathrm{cm}^{\wedge} 3 / \mathrm{mol}$ and K are used instead, on the order of $<0.2 \%$. Their equation was also compared with 56 inorganic and elements. Devations of $20 \%$ for $<200 \mathrm{~K}$ or $>1000 \mathrm{~K}$ points.

## References

[1]

## Examples

Succinic acid [110-15-6]

```
>>> Ihmels(Tc=851.0, Vc=0.000308)
```

6095016.233766234
chemicals.critical.Meissner ( $T c=$ None, $P c=$ None, $V c=$ None $)$
Old (1942) relationship for estimating critical properties from each other. Two of the three properties are required. This model uses the "critical surface", a general plot of Tc vs Pc vs Vc. The model used 42 organic and inorganic compounds to derive the equation. The general equation is in [1]:

$$
P_{c}=\frac{2.08 T_{c}}{V_{c}-8}
$$

## Parameters

Tc [float, optional] Critical temperature of fluid [K]
Pc [float, optional] Critical pressure of fluid [Pa]
Vc [float, optional] Critical volume of fluid [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]

## Returns

Tc, Pc or Vc [float] Critical property of fluid [K], [Pa], or [m^3/mol]

## Notes

The prediction of Tc from Pc and Vc is not tested, as this is not necessary anywhere, but it is implemented. Internal units are $\mathrm{atm}, \mathrm{cm}^{\wedge} 3 / \mathrm{mol}$, and K . A slight error occurs when $\mathrm{Pa}, \mathrm{cm}^{\wedge} 3 / \mathrm{mol}$ and K are used instead, on the order of $<0.2 \%$. This equation is less accurate than that of Ihmels, but surprisingly close. The author also proposed means of estimated properties independently.

## References

[1]

## Examples

Succinic acid [110-15-6]
>>> Meissner (Tc=851.0, Vc=0.000308)
5978445.199999999
chemicals.critical. Grigoras ( $T c=$ None, $P c=$ None, $V c=$ None)
Relatively recent (1990) relationship for estimating critical properties from each other. Two of the three properties are required. This model uses the "critical surface", a general plot of Tc vs Pc vs Vc. The model used 137 organic and inorganic compounds to derive the equation. The general equation is in [1]:

$$
P_{c}=2.9+20.2 \frac{T_{c}}{V_{c}}
$$

## Parameters

Tc [float, optional] Critical temperature of fluid [K]
Pc [float, optional] Critical pressure of fluid [Pa]
Vc [float, optional] Critical volume of fluid [m^3/mol]

## Returns

Tc, Pc or Vc [float] Critical property of fluid [K], [Pa], or [m^3/mol]

## Notes

The prediction of Tc from Pc and Vc is not tested, as this is not necessary anywhere, but it is implemented. Internal units are bar, $\mathrm{cm}^{\wedge} 3 / \mathrm{mol}$, and K . A slight error occurs when $\mathrm{Pa}, \mathrm{cm}^{\wedge} 3 / \mathrm{mol}$ and K are used instead, on the order of $<0.2 \%$. This equation is less accurate than that of Ihmels, but surprisingly close. The author also investigated an early QSPR model.

## References

## [1]

## Examples

Succinic acid [110-15-6]

```
>>> Grigoras(Tc=851.0, Vc=0.000308)
```

5871233.766233766
chemicals.critical.Hekayati_Raeissi ( $M W, V_{-}$sat $=$None, $T c=$ None, $P c=N o n e, V c=$ None $)$
Estimation model for missing critical constants of a fluid according to [1]. Based on the molecular weight and saturation molar volume of a fluid, and requires one of $T c$ or $P c$. Optionally, $V c$ can be provided to increase the accuracy of the prediction of $T_{c}$ or $P c$ a little.

## Parameters

MW [float] Molecular weight of fluid, $[\mathrm{g} / \mathrm{mol}]$
V_sat [float, optional] Molar volume of liquid at the saturation pressure of the fluid at 298.15
K. Used if $V c$ is not provided. [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]

Tc [float, optional] Critical temperature of fluid (optional) [K]
Pc [float, optional] Critical pressure of fluid (optional) [Pa]
Ve [float, optional] Critical volume of fluid (optional) [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]

## Returns

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
Vc [float] Critical volume of fluid [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]

## Notes

Internal units are $\mathrm{kPa}, \mathrm{m}^{\wedge} 3 / \mathrm{kmol}$, and K .

## References

[1]

## Examples

Toluene
>>> Hekayati_Raeissi(MW=92.13842, V_sat=0.00010686, Pc=4108000.0)
(599.7965819136947, 4108000.0, 0.000314909150453723)
chemicals.critical.Tb_Tc_relationship( $T b=$ None, $T c=$ None, fit='Perry8E')
This function relates the normal boiling point and the critical point of a compound. It is inspired by the relationship shown in [1] on page 2-468 for inorganic compounds.

$$
T_{c}=1.64 T_{b}
$$

## Parameters

Tb [float, optional] Normal boiling temperature of fluid [K]
Tc [float, optional] Critical temperature of fluid [K]
fit [str, optional] One of 'Perry8E’, ‘Chemicals2021FitInorganic', 'Chemicals2021FitElements', 'Chemicals2021FitBinary', 'Chemicals2021FitTernary', Chemicals2021FitOrganic', ‘Chemicals2021FitBr', ‘Chemicals2021FitC', ‘Chemicals2021FitCl', ‘Chemicals2021FitF', 'Chemicals2021FitI', 'Chemicals2021FitN', 'Chemicals2021FitO', ' 'Chemicals2021FitSi'.

## Returns

Tc or Tb [float] The temperature variable not provided [K]

## Notes

Chemicals2021FitBinary applies for inorganic compounds with two types of atoms; Chemicals2021FitTernary for three; and the various models Chemicals2021FitO, Chemicals2021FitC, etc apply for inorganic compounds with those elements in them.

The quality of this relationship is low, but if no further information is available it can be used to obtain an approximate value.

## References

[1]

## Examples

Tetrabromosilane has a known boiling point of 427.15 K and a critical temperature of 663.0 K .

```
>>> Tb_Tc_relationship(Tb=427.15, fit='Perry8E')
700.526
>>> Tb_Tc_relationship(Tb=427.15, fit='Chemicals2021FitBr')
668.0626
>>> Tb_Tc_relationship(Tb=427.15, fit='Chemicals2021FitSi')
```

651.8309
>>> Tb_Tc_relationship(Tb=427.15, fit='Chemicals2021FitBinary')
669.7712
>>> Tb_Tc_relationship(Tb=427.15, fit='Chemicals2021FitInorganic')
686.0029

The performance of the fits is fairly representative. However, because this method should only be used on compounds that don't have experimental critical points measured, many of the worst outlier chemicals have already been measured and the performance may be better than expected.
It is recommended to use the methods Chemicals2021FitElements, Chemicals2021FitBinary, and Chemicals2021FitTernary.

### 1.5.6 Critical Temperature of Mixtures

chemicals.critical.Li ( $z s, T c s, V c s$ )
Calculates critical temperature of a mixture according to mixing rules in [1]. Better than simple mixing rules.

$$
\begin{aligned}
& T_{c m}=\sum_{i=1}^{n} \Phi_{i} T_{c i} \\
& \Phi=\frac{x_{i} V_{c i}}{\sum_{j=1}^{n} x_{j} V_{c j}}
\end{aligned}
$$

## Parameters

zs [array-like] Mole fractions of all components
Tcs [array-like] Critical temperatures of all components, [K]
Ves [array-like] Critical volumes of all components, [m^3/mol]

## Returns

Tcm [float] Critical temperatures of the mixture, [K]

## Notes

Reviewed in many papers on critical mixture temperature.
Second example is from Najafi (2015), for ethylene, Benzene, ethylbenzene. This is similar to but not identical to the result from the article. The experimental point is 486.9 K .

2rd example is from Najafi (2015), for: butane/pentane/hexane 0.6449/0.2359/0.1192 mixture, exp: 450.22 K. Its result is identical to that calculated in the article.

## References

[1]

## Examples

Nitrogen-Argon 50/50 mixture
>>> Li([0.5, 0.5], [126.2, 150.8], [8.95e-05, 7.49e-05])
137.40766423357667
butane/pentane/hexane 0.6449/0.2359/0.1192 mixture, exp: 450.22 K .
>> Li([0.6449, 0.2359, 0.1192], [425.12, 469.7, 507.6],
... [0.000255, 0.000313, 0.000371])
449.68261498555444

## chemicals.critical.Chueh_Prausnitz_Tc (zs, Tcs, Vcs, taus)

Calculates critical temperature of a mixture according to mixing rules in [1].

$$
\begin{array}{r}
T_{c m}=\sum_{i}^{n} \theta_{i} T c_{i}+\sum_{i}^{n} \sum_{j}^{n}\left(\theta_{i} \theta_{j} \tau_{i j}\right) T_{r e f} \\
\theta=\frac{x_{i} V_{c i}^{2 / 3}}{\sum_{j=1}^{n} x_{j} V_{c j}^{2 / 3}}
\end{array}
$$

For a binary mxiture, this simplifies to:

$$
T_{c m}=\theta_{1} T_{c 1}+\theta_{2} T_{c 2}+2 \theta_{1} \theta_{2} \tau_{12}
$$

## Parameters

zs [array-like] Mole fractions of all components
Tcs [array-like] Critical temperatures of all components, [K]
Vcs [array-like] Critical volumes of all components, [m^3/mol]
taus [array-like of shape $z s$ by $z s$ ] Interaction parameters, [-]

## Returns

Tcm [float] Critical temperatures of the mixture, $[\mathrm{K}]$

## Notes

All parameters, even if zero, must be given to this function.

## References

[1], [2]

## Examples

butane/pentane/hexane 0.6449/0.2359/0.1192 mixture, exp: 450.22 K .
>>> Chueh_Prausnitz_Tc([0.6449, 0.2359, 0.1192], [425.12, 469.7, 507.6],
$\cdots$ [0.000255, 0.000313, 0.000371], [[0, 1.92681, 6.80358],
... [1.92681, 0, 1.89312], [ 6.80358, 1.89312, 0]])
450.122576472349
chemicals.critical.Grieves_Thodos (zs, Tcs, Aijs)
Calculates critical temperature of a mixture according to mixing rules in [1].

$$
T_{c m}=\sum_{i} \frac{T_{c i}}{1+\left(1 / x_{i}\right) \sum_{j} A_{i j} x_{j}}
$$

For a binary mxiture, this simplifies to:

$$
T_{c m}=\frac{T_{c 1}}{1+\left(x_{2} / x_{1}\right) A_{12}}+\frac{T_{c 2}}{1+\left(x_{1} / x_{2}\right) A_{21}}
$$

## Parameters

zs [array-like] Mole fractions of all components
Tcs [array-like] Critical temperatures of all components, [K]
Aijs [array-like of shape $z s$ by $z s$ ] Interaction parameters

## Returns

Tcm [float] Critical temperatures of the mixture, [K]

## Notes

All parameters, even if zero, must be given to this function. Giving 0s gives really bad results however.

## References

[1], [2]

## Examples

butane/pentane/hexane 0.6449/0.2359/0.1192 mixture, exp: 450.22 K .
>> Grieves_Thodos([0.6449, 0.2359, 0.1192], [425.12, 469.7, 507.6], [[0, 1.2503, 1. $\rightarrow 516]$, [0.799807, 0, 1.23843], [0.659633, 0.807474, 0]])
450.1839618758971
chemicals.critical.modified_Wilson_Tc (zs, Tcs, Aijs)
Calculates critical temperature of a mixture according to mixing rules in [1]. Equation

$$
T_{c m}=\sum_{i} x_{i} T_{c i}+C \sum_{i} x_{i} \ln \left(x_{i}+\sum_{j} x_{j} A_{i j}\right) T_{r e f}
$$

For a binary mxiture, this simplifies to:

$$
T_{c m}=x_{1} T_{c 1}+x_{2} T_{c 2}+C\left[x_{1} \ln \left(x_{1}+x_{2} A_{12}\right)+x_{2} \ln \left(x_{2}+x_{1} A_{21}\right)\right]
$$

## Parameters

zs [float] Mole fractions of all components
Tes [float] Critical temperatures of all components, [K]
Aijs [matrix] Interaction parameters

## Returns

Tcm [float] Critical temperatures of the mixture, $[\mathrm{K}]$

## Notes

The equation and original article has been reviewed. [1] has 75 binary systems, and additional multicomponent mixture parameters. All parameters, even if zero, must be given to this function.

2rd example is from [2], for: butane/pentane/hexane 0.6449/0.2359/0.1192 mixture, exp: 450.22 K . Its result is identical to that calculated in the article.

## References

[1], [2]

## Examples

```
>>> modified_Wilson_Tc([0.6449, 0.2359, 0.1192], [425.12, 469.7, 507.6],
#. [[0, 1.174450, 1.274390], [0.835914, 0, 1.21038],
... [0.746878, 0.80677, 0]])
450.03059668230316
```


### 1.5.7 Critical Volume of Mixtures

chemicals.critical.Chueh_Prausnitz_Vc (zs, Vcs, nus)
Calculates critical volume of a mixture according to mixing rules in [1] with an interaction parameter.

$$
V_{c m}=\sum_{i}^{n} \theta_{i} V_{c i}+\sum_{i}^{n} \sum_{j}^{n}\left(\theta_{i} \theta_{j} \nu_{i j}\right) V_{r e f} \theta=\frac{x_{i} V_{c i}^{2 / 3}}{\sum_{j=1}^{n} x_{j} V_{c j}^{2 / 3}}
$$

## Parameters

zs [float] Mole fractions of all components
Ves [float] Critical volumes of all components, [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]
nus [matrix] Interaction parameters, [ $\left.\mathrm{cm}^{\wedge} 3 / \mathrm{mol}\right]$

## Returns

Vcm [float] Critical volume of the mixture, $\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]$

## Notes

All parameters, even if zero, must be given to this function. nu parameters are in $\mathrm{cm}^{\wedge} 3 / \mathrm{mol}$, but are converted to $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ inside the function

## References

[1], [2]

## Examples

1-butanol/benzene $0.4271 / 0.5729$ mixture, $\mathrm{Vcm}=268.096 \mathrm{~mL} / \mathrm{mol}$.
>>> Chueh_Prausnitz_Vc([0.4271, 0.5729], [0.000273, 0.000256], [[0, 5.61847], [5. $\rightarrow 61847,0]$ ])
0.00026620503424517445
chemicals.critical.modified_Wilson_Vc $(z s, V c s, A i j s)$
Calculates critical volume of a mixture according to mixing rules in [1] with parameters. Equation

$$
V_{c m}=\sum_{i} x_{i} V_{c i}+C \sum_{i} x_{i} \ln \left(x_{i}+\sum_{j} x_{j} A_{i j}\right) V_{r e f}
$$

For a binary mxiture, this simplifies to:

$$
V_{c m}=x_{1} V_{c 1}+x_{2} V_{c 2}+C\left[x_{1} \ln \left(x_{1}+x_{2} A_{12}\right)+x_{2} \ln \left(x_{2}+x_{1} A_{21}\right)\right]
$$

## Parameters

zs [float] Mole fractions of all components
Ves [float] Critical volumes of all components, [ $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ ]
Aijs [matrix] Interaction parameters, [ $\left.\mathrm{cm}^{\wedge} 3 / \mathrm{mol}\right]$

## Returns

Vcm [float] Critical volume of the mixture, $\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]$

## Notes

The equation and original article has been reviewed. All parameters, even if zero, must be given to this function. $\mathrm{C}=-2500$

All parameters, even if zero, must be given to this function. nu parameters are in $\mathrm{cm}^{\wedge} 3 / \mathrm{mol}$, but are converted to $\mathrm{m}^{\wedge} 3 / \mathrm{mol}$ inside the function

## References

[1], [2]

## Examples

1-butanol/benzene $0.4271 / 0.5729$ mixture, $\mathrm{Vcm}=268.096 \mathrm{~mL} / \mathrm{mol}$.

```
>>> modified_Wilson_Vc([0.4271, 0.5729], [0.000273, 0.000256],
... [[0, 0.6671250], [1.3939900, 0]])
0.0002664335032706881
```


### 1.6 Dipole Moment (chemicals.dipole)

This module contains lookup functions for the property dipole moment.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Lookup Functions


### 1.6.1 Lookup Functions

chemicals.dipole.dipole_moment(CASRN, method=None)
This function handles the retrieval of a chemical's dipole moment. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Preferred source is 'CCCBDB'. Considerable variation in reported data has found.

## Parameters

CASRN [str] CASRN [-]

## Returns

dipole [float] Dipole moment, [debye]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'CCCBDB', 'MULLER', or 'POLING', 'PSI4_2022A'. All valid values are also held in the list dipole_all_methods.

## See also:

dipole_moment_methods

## Notes

A total of three sources are available for this function. They are:

- 'CCCBDB', a series of critically evaluated data for compounds in [1], intended for use in predictive modeling.
- 'MULLER', a collection of data in a group-contribution scheme in [2].
- 'POLING', in the appendix in [3].
- 'PSI4_2022A', values computed using the Psi4 version 1.3.2 quantum chemistry software, with initialized positions from rdkit's EmbedMolecule method, the basis set 6-31G** and the method mp2 [4].

This function returns dipole moment in units of Debye. This is actually a non-SI unit; to convert to SI, multiply by $3.33564095198 \mathrm{e}-30$ and its units will be in ampere*second ${ }^{\wedge} 2$ or equivalently and more commonly given, coulomb*second. The constant is the result of $1 \mathrm{E}-21 / \mathrm{c}$, where c is the speed of light.

## References

[1], [2], [3], [4]

## Examples

>>> dipole_moment(CASRN='64-17-5')
1.44

## chemicals.dipole.dipole_moment_methods(CASRN)

Return all methods available to obtain the dipole moment for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain the dipole moment with the given inputs.
See also:
dipole_moment

```
chemicals.dipole.dipole_moment_all_methods = ('CCCBDB', 'MULLER', 'POLING', 'PSI4_2022A')
```

Tuple of method name keys. See the dipole for the actual references

### 1.7 DIPPR Fit Equations (chemicals.dippr)

This module contains implementations of various numered property equations used by the DIPPR, the Design Institude for Physical Property Research.

No actual data is included in this module; it is just functional implementations of the formulas and some of their derivatives/integrals.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Equations
- Jacobians (for fitting)


### 1.7.1 Equations

chemicals.dippr. $\mathrm{EQ} 100(T, A=0, B=0, C=0, D=0, E=0, F=0, G=0$, order $=0$ )
DIPPR Equation \# 100. Used in calculating the molar heat capacities of liquids and solids, liquid thermal conductivity, and solid density. All parameters default to zero. As this is a straightforward polynomial, no restrictions on parameters apply. Note that high-order polynomials like this may need large numbers of decimal places to avoid unnecessary error.

$$
Y=A+B T+C T^{2}+D T^{3}+E T^{4}+F T^{5}+G T^{6}
$$

## Parameters

T [float] Temperature, [K]
A-G [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1, the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order $=\mathbf{= 1}$, property/K; if order $=\mathbf{=} \mathbf{- 1}$, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T, integral with respect to T, and integral over T with respect to T are computed as follows. All derivatives and integrals are easily computed with SymPy.

$$
\begin{gathered}
\frac{d Y}{d T}=B+2 C T+3 D T^{2}+4 E T^{3}+5 F T^{4}+6 G T^{5} \\
\int Y d T=A T+\frac{B T^{2}}{2}+\frac{C T^{3}}{3}+\frac{D T^{4}}{4}+\frac{E T^{5}}{5}+\frac{F T^{6}}{6}+\frac{G T^{7}}{7} \\
\int \frac{Y}{T} d T=A \ln (T)+B T+\frac{C T^{2}}{2}+\frac{D T^{3}}{3}+\frac{E T^{4}}{4}+\frac{F T^{5}}{5}+\frac{G T^{6}}{6}
\end{gathered}
$$

## References

[1]

## Examples

Water liquid heat capacity; DIPPR coefficients normally listed in $\mathrm{J} / \mathrm{kmol} / \mathrm{K}$.

```
>> EQ100(300, 276370., -2090.1, 8.125, -0.014116, 0.0000093701)
```

75355.81000000003
chemicals.dippr.EQ101( $T, A, B, C=0.0, D=0.0, E=0.0$, order $=0$ )
DIPPR Equation \# 101. Used in calculating vapor pressure, sublimation pressure, and liquid viscosity. All 5 parameters are required. E is often an integer. As the model is exponential, a sufficiently high temperature will cause an OverflowError. A negative temperature (or just low, if fit poorly) may cause a math domain error.

$$
Y=\exp \left(A+\frac{B}{T}+C \cdot \ln T+D \cdot T^{E}\right)
$$

## Parameters

T [float] Temperature, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for $n$, the $n$th derivative of the property is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float] Property [constant-specific]

## Notes

This function is not integrable for either dT or $\mathrm{Y} / \mathrm{T} \mathrm{dT}$.

$$
\begin{gathered}
\frac{d Y}{d T}=\left(-\frac{B}{T^{2}}+\frac{C}{T}+\frac{D E T^{E}}{T}\right) e^{A+\frac{B}{T}+C \log (T)+D T^{E}} \\
\frac{d^{2} Y}{d T^{2}}=\frac{\left(\frac{2 B}{T}-C+D E^{2} T^{E}-D E T^{E}+\left(-\frac{B}{T}+C+D E T^{E}\right)^{2}\right) e^{A+\frac{B}{T}+C \log (T)+D T^{E}}}{T^{2}} \\
\frac{d^{3} Y}{d T^{3}}=\frac{\left(-\frac{6 B}{T}+2 C+D E^{3} T^{E}-3 D E^{2} T^{E}+2 D E T^{E}+\left(-\frac{B}{T}+C+D E T^{E}\right)^{3}+3\left(-\frac{B}{T}+C+D E T^{E}\right)\left(\frac{2 B}{T}-C+D E^{2}\right.\right.}{T^{3}}
\end{gathered}
$$

## References

[1]

## Examples

Water vapor pressure; DIPPR coefficients normally listed in Pa.

```
>>> EQ101(300, 73.649, -7258.2, -7.3037, 4.1653E-6, 2)
```

3537.44834545549

## chemicals.dippr.EQ102 ( $T, A, B, C=0.0, D=0.0$, order $=0$ )

DIPPR Equation \# 102. Used in calculating vapor viscosity, vapor thermal conductivity, and sometimes solid heat capacity. High values of B raise an OverflowError. All 4 parameters are required. C and D are often 0.

$$
Y=\frac{A \cdot T^{B}}{1+\frac{C}{T}+\frac{D}{T^{2}}}
$$

## Parameters

T [float] Temperature, [K]
A-D [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order $==\mathbf{1}$, property/K; if order $==\mathbf{- 1}$, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T , integral with respect to T , and integral over T with respect to T are computed as follows. The first derivative is easily computed; the two integrals required Rubi to perform the integration.

$$
\begin{gathered}
\frac{d Y}{d T}=\frac{A B T^{B}}{T\left(\frac{C}{T}+\frac{D}{T^{2}}+1\right)}+\frac{A T^{B}\left(\frac{C}{T^{2}}+\frac{2 D}{T^{3}}\right)}{\left(\frac{C}{T}+\frac{D}{T^{2}}+1\right)^{2}} \\
\int Y d T=-\frac{2 A T^{B+3} \operatorname{hyp} 2 \mathrm{f} 1\left(1, B+3, B+4,-\frac{2 T}{C-\sqrt{C^{2}-4 D}}\right)}{(B+3)\left(C+\sqrt{C^{2}-4 D}\right) \sqrt{C^{2}-4 D}}+\frac{2 A T^{B+3} \operatorname{hyp} 2 \mathrm{f} 1\left(1, B+3, B+4,-\frac{2 T}{C+\sqrt{C^{2}-4 D}}\right)}{(B+3)\left(C-\sqrt{C^{2}-4 D}\right) \sqrt{C^{2}-4 D}} \\
\int \frac{Y}{T} d T=-\frac{2 A T^{B+2} \operatorname{hyp} 2 \mathrm{f} 1\left(1, B+2, B+3,-\frac{2 T}{C+\sqrt{C^{2}-4 D}}\right)}{(B+2)\left(C+\sqrt{C^{2}-4 D}\right) \sqrt{C^{2}-4 D}}+\frac{2 A T^{B+2} \operatorname{hyp} 2 \mathrm{f} 1\left(1, B+2, B+3,-\frac{2 T}{C-\sqrt{C^{2}-4 D}}\right)}{(B+2)\left(C-\sqrt{C^{2}-4 D}\right) \sqrt{C^{2}-4 D}}
\end{gathered}
$$

## References

[1]

## Examples

Water vapor viscosity; DIPPR coefficients normally listed in Pa*s.

```
>>> EQ102(300, 1.7096E-8, 1.1146, 0, 0)
```

9.860384711890639e-06
chemicals.dippr.EQ104 ( $T, A, B, C=0.0, D=0.0, E=0.0$, order $=0$ )
DIPPR Equation \#104. Often used in calculating second virial coefficients of gases. All 5 parameters are required. C, D, and E are normally large values.

$$
Y=A+\frac{B}{T}+\frac{C}{T^{3}}+\frac{D}{T^{8}}+\frac{E}{T^{9}}
$$

## Parameters

T [float] Temperature, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order $=\mathbf{= 1}$, property/K; if order $=\mathbf{= 1}$, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T , integral with respect to T , and integral over T with respect to T are computed as follows. All expressions can be obtained with SymPy readily.

$$
\begin{gathered}
\frac{d Y}{d T}=-\frac{B}{T^{2}}-\frac{3 C}{T^{4}}-\frac{8 D}{T^{9}}-\frac{9 E}{T^{10}} \\
\int Y d T=A T+B \ln (T)-\frac{1}{56 T^{8}}\left(28 C T^{6}+8 D T+7 E\right) \\
\int \frac{Y}{T} d T=A \ln (T)-\frac{1}{72 T^{9}}\left(72 B T^{8}+24 C T^{6}+9 D T+8 E\right)
\end{gathered}
$$

## References

[1]

## Examples

Water second virial coefficient; DIPPR coefficients normally dimensionless.

```
>>> EQ104(300, 0.02222, -26.38, -16750000, -3.894E19, 3.133E21)
```

-1.1204179007265156
chemicals.dippr.EQ105 ( $T, A, B, C, D$, order $=0$ )
DIPPR Equation \#105. Often used in calculating liquid molar density. All 4 parameters are required. C is sometimes the fluid's critical temperature.

$$
Y=\frac{A}{B^{1+\left(1-\frac{T}{C}\right)^{D}}}
$$

## Parameters

## T [float] Temperature, [K]

A-D [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , 2 , and 3, that derivative of the property is returned; No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

Y [float] Property [constant-specific]

## Notes

This expression can be integrated in terms of the incomplete gamma function for dT, however nans are the only output from that function. For Y/T dT no integral could be found.

$$
\begin{gathered}
\frac{d Y}{d T}=\frac{A B^{-\left(1-\frac{T}{C}\right)^{D}-1} D\left(1-\frac{T}{C}\right)^{D} \log (B)}{C\left(1-\frac{T}{C}\right)} \\
\frac{d^{2} Y}{d T^{2}}=\frac{A B^{-\left(1-\frac{T}{C}\right)^{D}-1} D\left(1-\frac{T}{C}\right)^{D}\left(D\left(1-\frac{T}{C}\right)^{D} \log (B)-D+1\right) \log (B)}{C^{2}\left(1-\frac{T}{C}\right)^{2}} \\
\frac{d^{3} Y}{d T^{3}}=\frac{A B^{-\left(1-\frac{T}{C}\right)^{D}-1} D\left(1-\frac{T}{C}\right)^{D}\left(D^{2}\left(1-\frac{T}{C}\right)^{2 D} \log (B)^{2}-3 D^{2}\left(1-\frac{T}{C}\right)^{D} \log (B)+D^{2}+3 D\left(1-\frac{T}{C}\right)^{D} \log (B)-3 D\right.}{C^{3}\left(1-\frac{T}{C}\right)^{3}}
\end{gathered}
$$

## References

[1]

## Examples

Hexane molar density; DIPPR coefficients normally in $\mathrm{kmol} / \mathrm{m}^{\wedge} 3$.
>>> EQ105(300., 0.70824, 0.26411, 507.6, 0.27537)
7.593170096339237
chemicals.dippr.EQ106 ( $T, T c, A, B, C=0.0, D=0.0, E=0.0$, order $=0$ )
DIPPR Equation \#106. Often used in calculating liquid surface tension, and heat of vaporization. Only parameters A and B parameters are required; many fits include no further parameters. Critical temperature is also required.

$$
\begin{gathered}
Y=A\left(1-T_{r}\right)^{B+C T_{r}+D T_{r}^{2}+E T_{r}^{3}} \\
T r=\frac{T}{T c}
\end{gathered}
$$

## Parameters

T [float] Temperature, [K]
Tc [float] Critical temperature, [K]
A-D [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , 2 , and 3 , that derivative of the property is returned; No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

Y [float] Property [constant-specific]

## Notes

This form is used by Yaws with only the parameters $A$ and $B$.
The integral could not be found, but the integral over T actually could, again in terms of hypergeometric functions.

$$
\begin{aligned}
& \frac{d Y}{d T}=A\left(-\frac{T}{T_{c}}+1\right)^{B+\frac{C T}{T_{c}}+\frac{D T^{2}}{T_{c}^{2}}+\frac{e T^{3}}{T_{c}^{3}}}\left(\left(\frac{C}{T_{c}}+\frac{2 D T}{T_{c}^{2}}+\frac{3 e T^{2}}{T_{c}^{3}}\right) \log \left(-\frac{T}{T_{c}}+1\right)-\frac{B+\frac{C T}{T_{c}}+\frac{D T^{2}}{T_{c}^{2}}+\frac{e T^{3}}{T_{c}^{3}}}{T_{c}\left(-\frac{T}{T_{c}}+1\right)}\right) \\
& \frac{d^{2} Y}{d T^{2}}=\frac{A\left(-\frac{T}{T_{c}}+1\right)^{B+\frac{C T}{T_{c}}+\frac{D T^{2}}{T_{c}^{2}}+\frac{e T^{3}}{T_{c}^{3}}}\left(2\left(D+\frac{3 e T}{T_{c}}\right) \log \left(-\frac{T}{T_{c}}+1\right)+\left(\left(C+\frac{2 D T}{T_{c}}+\frac{3 e T^{2}}{T_{c}^{2}}\right) \log \left(-\frac{T}{T_{c}}+1\right)+\frac{B+\frac{C T}{T_{c}}+\frac{D T^{2}}{T_{c}^{2}}}{\frac{T}{T_{c}}-1}\right.\right.}{T_{c}^{2}} \\
& \frac{d^{3} Y}{d T^{3}}=\frac{A\left(-\frac{T}{T_{c}}+1\right)^{B+\frac{C T}{T_{c}}+\frac{D T^{2}}{T_{c}^{2}}+\frac{e T^{3}}{T_{c}^{3}}}\left(\frac{6\left(D+\frac{3 e T}{T_{c}}\right)}{T_{c}-1}+\left(\left(C+\frac{2 D T}{T_{c}}+\frac{3 e T^{2}}{T_{c}^{2}}\right) \log \left(-\frac{T}{T_{c}}+1\right)+\frac{B+\frac{C T}{T_{c}}+\frac{D T^{2}}{T_{c}^{2}}+\frac{e T^{3}}{T_{c}^{3}}}{\frac{T}{T_{c}}-1}\right)^{3}+3((C\right.}{}
\end{aligned}
$$

## References

[1]

## Examples

Water surface tension; DIPPR coefficients normally in $\mathrm{Pa}^{*}$ s.
>>> EQ106(300, 647.096, 0.17766, 2.567, -3.3377, 1.9699)
0.07231499373541
chemicals.dippr.EQ107 ( $T, A=0, B=0, C=0, D=0, E=0$, order $=0$ )
DIPPR Equation \#107. Often used in calculating ideal-gas heat capacity. All 5 parameters are required. Also called the Aly-Lee equation.

$$
Y=A+B\left[\frac{C / T}{\sinh (C / T)}\right]^{2}+D\left[\frac{E / T}{\cosh (E / T)}\right]^{2}
$$

## Parameters

$\mathbf{T}$ [float] Temperature, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order $=\mathbf{= 1}$, property/K; if order $==\mathbf{- 1}$, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T , integral with respect to T , and integral over T with respect to T are computed as follows. The derivative is obtained via SymPy; the integrals from Wolfram Alpha.

$$
\begin{gathered}
\frac{d Y}{d T}=\frac{2 B C^{3} \cosh \left(\frac{C}{T}\right)}{T^{4} \sinh ^{3}\left(\frac{C}{T}\right)}-\frac{2 B C^{2}}{T^{3} \sinh ^{2}\left(\frac{C}{T}\right)}+\frac{2 D E^{3} \sinh \left(\frac{E}{T}\right)}{T^{4} \cosh ^{3}\left(\frac{E}{T}\right)}-\frac{2 D E^{2}}{T^{3} \cosh ^{2}\left(\frac{E}{T}\right)} \\
\int Y d T=A T+\frac{B C}{\tanh \left(\frac{C}{T}\right)}-D E \tanh \left(\frac{E}{T}\right) \\
\int \frac{Y}{T} d T=A \ln (T)+\frac{B C}{T \tanh \left(\frac{C}{T}\right)}-B \ln \left(\sinh \left(\frac{C}{T}\right)\right)-\frac{D E}{T} \tanh \left(\frac{E}{T}\right)+D \ln \left(\cosh \left(\frac{E}{T}\right)\right)
\end{gathered}
$$

## References

[1], [2]

## Examples

Water ideal gas molar heat capacity; DIPPR coefficients normally in $\mathrm{J} / \mathrm{kmol} / \mathrm{K}$

```
>>> EQ107(300., 33363., 26790., 2610.5, 8896., 1169.)
```

33585.90452768923

## chemicals.dippr.EQ114 ( $T, T c, A, B, C, D$, order=0)

DIPPR Equation \#114. Rarely used, normally as an alternate liquid heat capacity expression. All 4 parameters are required, as well as critical temperature.

$$
\begin{gathered}
Y=\frac{A^{2}}{\tau}+B-2 A C \tau-A D \tau^{2}-\frac{1}{3} C^{2} \tau^{3}-\frac{1}{2} C D \tau^{4}-\frac{1}{5} D^{2} \tau^{5} \\
\tau=1-\frac{T}{T c}
\end{gathered}
$$

## Parameters

T [float] Temperature, [K]
Tc [float] Critical temperature, [K]
A-D [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order $=\mathbf{= 1}$, property/K; if order $=\mathbf{= - 1}$, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T , integral with respect to T , and integral over T with respect to T are computed as follows. All expressions can be obtained with SymPy readily.
$\frac{d Y}{d T}=\frac{A^{2}}{T_{c}\left(-\frac{T}{T_{c}}+1\right)^{2}}+\frac{2 A}{T_{c}} C+\frac{2 A}{T_{c}} D\left(-\frac{T}{T_{c}}+1\right)+\frac{C^{2}}{T_{c}}\left(-\frac{T}{T_{c}}+1\right)^{2}+\frac{2 C}{T_{c}} D\left(-\frac{T}{T_{c}}+1\right)^{3}+\frac{D^{2}}{T_{c}}\left(-\frac{T}{T_{c}}+1\right)^{4}$
$\int Y d T=-A^{2} T_{c} \ln \left(T-T_{c}\right)+\frac{D^{2} T^{6}}{30 T_{c}^{5}}-\frac{T^{5}}{10 T_{c}^{4}}\left(C D+2 D^{2}\right)+\frac{T^{4}}{12 T_{c}^{3}}\left(C^{2}+6 C D+6 D^{2}\right)-\frac{T^{3}}{3 T_{c}^{2}}\left(A D+C^{2}+3 C D+2 D\right.$
$\int \frac{Y}{T} d T=-A^{2} \ln \left(T+\frac{-60 A^{2} T_{c}+60 A C T_{c}+30 A D T_{c}-30 B T_{c}+10 C^{2} T_{c}+15 C D T_{c}+6 D^{2} T_{c}}{60 A^{2}-60 A C-30 A D+30 B-10 C^{2}-15 C D-6 D^{2}}\right)+\frac{D^{2} T^{5}}{25 T_{c}^{5}}-\frac{T^{4}}{8 T_{c}^{4}}(C D$
Strictly speaking, the integral over T has an imaginary component, but only the real component is relevant and the complex part discarded.

## References

[1]

## Examples

Hydrogen liquid heat capacity; DIPPR coefficients normally in J/kmol/K.

```
>>> EQ114(20, 33.19, 66.653, 6765.9, -123.63, 478.27)
```

19423.948911676463
chemicals.dippr.EQ115 ( $T, A, B, C=0, D=0, E=0$, order $=0$ )
DIPPR Equation \#115. No major uses; has been used as an alternate liquid viscosity expression, and as a model for vapor pressure. Only parameters A and B are required.

$$
Y=\exp \left(A+\frac{B}{T}+C \ln T+D T^{2}+\frac{E}{T^{2}}\right)
$$

## Parameters

$\mathbf{T}$ [float] Temperature, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , 2 , and 3, that derivative of the property is returned; No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

Y [float] Property [constant-specific]

## Notes

No coefficients found for this expression. This function is not integrable for either dT or Y/T dT.

$$
\begin{gathered}
\frac{d Y}{d T}=\left(-\frac{B}{T^{2}}+\frac{C}{T}+2 D T-\frac{2 E}{T^{3}}\right) e^{A+\frac{B}{T}+C \log (T)+D T^{2}+\frac{E}{T^{2}}} \\
\frac{d^{2} Y}{d T^{2}}=\left(\frac{2 B}{T^{3}}-\frac{C}{T^{2}}+2 D+\frac{6 E}{T^{4}}+\left(\frac{B}{T^{2}}-\frac{C}{T}-2 D T+\frac{2 E}{T^{3}}\right)^{2}\right) e^{A+\frac{B}{T}+C \log (T)+D T^{2}+\frac{E}{T^{2}}} \\
\frac{d^{3} Y}{d T^{3}}=-\left(3\left(\frac{2 B}{T^{3}}-\frac{C}{T^{2}}+2 D+\frac{6 E}{T^{4}}\right)\left(\frac{B}{T^{2}}-\frac{C}{T}-2 D T+\frac{2 E}{T^{3}}\right)+\left(\frac{B}{T^{2}}-\frac{C}{T}-2 D T+\frac{2 E}{T^{3}}\right)^{3}+\frac{2\left(\frac{3 B}{T}-C+\frac{12 E}{T^{2}}\right)}{T^{3}}\right) e
\end{gathered}
$$

## References

[1]
chemicals.dippr.EQ116 ( $T, T c, A, B, C, D, E$, order $=0$ )
DIPPR Equation \#116. Used to describe the molar density of water fairly precisely; no other uses listed. All 5 parameters are needed, as well as the critical temperature.

$$
\begin{gathered}
Y=A+B \tau^{0.35}+C \tau^{2 / 3}+D \tau+E \tau^{4 / 3} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
$$

## Parameters

T [float] Temperature, [K]
Tc [float] Critical temperature, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1 , the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order $=\mathbf{= 1}$, property/K; if order $=\mathbf{= 1}$, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T and integral with respect to T are computed as follows. The integral divided by T with respect to T has an extremely complicated (but still elementary) integral which can be read from the source. It was computed with Rubi; the other expressions can readily be obtained with SymPy.

$$
\begin{gathered}
\frac{d Y}{d T}=-\frac{7 B}{20 T_{c}\left(-\frac{T}{T_{c}}+1\right)^{\frac{13}{20}}}-\frac{2 C}{3 T_{c} \sqrt[3]{-\frac{T}{T_{c}}+1}}-\frac{D}{T_{c}}-\frac{4 E}{3 T_{c}} \sqrt[3]{-\frac{T}{T_{c}}+1} \\
\int Y d T=A T-\frac{20 B}{27} T_{c}\left(-\frac{T}{T_{c}}+1\right)^{\frac{27}{20}}-\frac{3 C}{5} T_{c}\left(-\frac{T}{T_{c}}+1\right)^{\frac{5}{3}}+D\left(-\frac{T^{2}}{2 T_{c}}+T\right)-\frac{3 E}{7} T_{c}\left(-\frac{T}{T_{c}}+1\right)^{\frac{7}{3}}
\end{gathered}
$$

## References

[1]

## Examples

Water liquid molar density; DIPPR coefficients normally in $\mathrm{kmol} / \mathrm{m}^{\wedge} 3$.

```
>>> EQ116(300., 647.096, 17.863, 58.606, -95.396, 213.89, -141.26)
55.17615446406527
```

chemicals.dippr.EQ127 (T, A, B, C, D, E, F, G, order=0)
DIPPR Equation \#127. Rarely used, and then only in calculating ideal-gas heat capacity. All 7 parameters are required.

$$
Y=A+B\left[\frac{\left(\frac{C}{T}\right)^{2} \exp \left(\frac{C}{T}\right)}{\left(\exp \frac{C}{T}-1\right)^{2}}\right]+D\left[\frac{\left(\frac{E}{T}\right)^{2} \exp \left(\frac{E}{T}\right)}{\left(\exp \frac{E}{T}-1\right)^{2}}\right]+F\left[\frac{\left(\frac{G}{T}\right)^{2} \exp \left(\frac{G}{T}\right)}{\left(\exp \frac{G}{T}-1\right)^{2}}\right]
$$

## Parameters

T [float] Temperature, [K]
A-G [float] Parameter for the equation; chemical and property specific [-]
order [int, optional] Order of the calculation. 0 for the calculation of the result itself; for 1, the first derivative of the property is returned, for -1 , the indefinite integral of the property with respect to temperature is returned; and for -1 j , the indefinite integral of the property divided by temperature with respect to temperature is returned. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

## Returns

$\mathbf{Y}$ [float]
Property [constant-specific; if order == 1, property/K; if order ==-1, property*K; if order $==-1 \mathrm{j}$, unchanged from default]

## Notes

The derivative with respect to T , integral with respect to T , and integral over T with respect to T are computed as follows. All expressions can be obtained with SymPy readily.

$$
\begin{aligned}
& \frac{d Y}{d T}=-\frac{B C^{3} e^{\frac{C}{T}}}{T^{4}\left(e^{\frac{C}{T}}-1\right)^{2}}+\frac{2 B C^{3} e^{\frac{2 C}{T}}}{T^{4}\left(e^{\frac{C}{T}}-1\right)^{3}}-\frac{2 B C^{2} e^{\frac{C}{T}}}{T^{3}\left(e^{\frac{C}{T}}-1\right)^{2}}-\frac{D E^{3} e^{\frac{E}{T}}}{T^{4}\left(e^{\frac{E}{T}}-1\right)^{2}}+\frac{2 D E^{3} e^{\frac{2 E}{T}}}{T^{4}\left(e^{\frac{E}{T}}-1\right)^{3}}-\frac{2 D E^{2} e^{\frac{E}{T}}}{T^{3}\left(e^{\frac{E}{T}}-1\right)^{2}}-\frac{F G^{\frac{3}{2}}}{T^{4}\left(e^{\frac{C}{T}}\right.} \\
& \int Y d T=A T+\frac{B C^{2}}{C e^{\frac{C}{T}}-C}+\frac{D E^{2}}{E e^{\frac{E}{T}}-E}+\frac{F G^{2}}{G e^{\frac{C}{T}}-G} \\
& \int \frac{Y}{T} d T=A \ln (T)+B C^{2}\left(\frac{1}{C T e^{\frac{C}{T}}-C T}+\frac{1}{C T}-\frac{1}{C^{2}} \ln \left(e^{\frac{C}{T}}-1\right)\right)+D E^{2}\left(\frac{1}{E T e^{\frac{E}{T}}-E T}+\frac{1}{E T}-\frac{1}{E^{2}} \ln \left(e^{\frac{E}{T}}-1\right)\right)
\end{aligned}
$$

## References

[1]

## Examples

Ideal gas heat capacity of methanol; DIPPR coefficients normally in $\mathrm{J} / \mathrm{kmol} / \mathrm{K}$

```
>>> EQ127(20., 3.3258E4, 3.6199E4, 1.2057E3, 1.5373E7, 3.2122E3, -1.5318E7, 3.
->2122E3)
33258.0
```


### 1.7.2 Jacobians (for fitting)

chemicals.dippr.EQ101_fitting_jacobian (Ts, $A, B, C, D, E)$
Compute and return the Jacobian of the property predicted by DIPPR Equation \# 101 with respect to all the coefficients. This is used in fitting parameters for chemicals.

## Parameters

Ts [list[float]] Temperatures of the experimental data points, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]

## Returns

jac [list[list[float, 5], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.dippr.EQ102_fitting_jacobian( $T s, A, B, C, D$ )
Compute and return the Jacobian of the property predicted by DIPPR Equation \# 102 with respect to all the coefficients. This is used in fitting parameters for chemicals.

## Parameters

Ts [list[float]] Temperatures of the experimental data points, [K]
A-D [float] Parameter for the equation; chemical and property specific [-]

## Returns

jac [list[list[float, 4], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.dippr.EQ105_fitting_jacobian ( $T s, A, B, C, D$ )
Compute and return the Jacobian of the property predicted by DIPPR Equation \# 105 with respect to all the coefficients. This is used in fitting parameters for chemicals.

## Parameters

Ts [list[float]] Temperatures of the experimental data points, [K]
A-D [float] Parameter for the equation; chemical and property specific [-]

## Returns

jac [list[list[float, 4], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.dippr.EQ106_fitting_jacobian $(T s, T c, A, B, C, D, E)$
Compute and return the Jacobian of the property predicted by DIPPR Equation \# 106 with respect to all the coefficients. This is used in fitting parameters for chemicals.

## Parameters

Ts [list[float]] Temperatures of the experimental data points, [K]
Tc [float] Critical temperature, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]

## Returns

jac [list[list[float, 5], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.dippr.EQ107_fitting_jacobian (Ts, $A, B, C, D, E$ )
Compute and return the Jacobian of the property predicted by DIPPR Equation \# 107 with respect to all the coefficients. This is used in fitting parameters for chemicals.

## Parameters

Ts [list[float]] Temperatures of the experimental data points, [K]
A-E [float] Parameter for the equation; chemical and property specific [-]

## Returns

jac [list[list[float, 5], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]

### 1.8 Periodic Table (chemicals.elements)

This module contains a complete periodic table, routines for working with chemical formulas, computing molecular weight, computing mass fractions and atom fractions, and assorted other tasks.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Periodic Table and Elements
- Working with Formulas
- Working with Parsed Formulas


### 1.8.1 Periodic Table and Elements

chemicals.elements.periodic_table = <chemicals.elements.PeriodicTable object>
Single instance of the PeriodicTable class. Use this, not the PeriodicTable class directly.
A brief overview of using the periodic table and its elements:

```
>>> periodic_table.Na
<Element Sodium (Na), number 11, MW=22.98977>
>>> periodic_table.U.MW
238.02891
>>> periodic_table['Th'].CAS
'7440-29-1'
>>> periodic_table.lead.protons
82
>>> periodic_table['7440-57-5'].symbol
'Au'
>>> len(periodic_table)
118
>>> 'gold' in periodic_table
True
>>> periodic_table.He.protons, periodic_table.He.neutrons, periodic_table.He.
electrons # Standard number of protons, neutrons, electrons
(2, 2, 2)
>>> periodic_table.He.phase # Phase of the element in the standard state
'g'
>>> periodic_table.He.Hf # Heat of formation in standard state in J/mol - byь
    ๑definition (0
0.0
>>> periodic_table.He.SO # Absolute entropy (J/(mol*K) in standard state - non-zero)
126.2
>>> periodic_table.Kr.block, periodic_table.Kr.period, periodic_table.Kr.group
('p', 4, 18)
>>> periodic_table.Rn.InChI
'Rn'
>>> periodic_table.Rn.smiles
'[Rn]'
>>> periodic_table.Pu.number
94
```

```
>>> periodic_table.Pu.PubChem
23940
>>> periodic_table.Bi.InChI_key
'JCXGWMGPZLAOME-UHFFFAOYSA-N'
```

class chemicals.elements.Element (number, symbol, name, MW, CAS, AReneg, rcov, rvdw, maxbonds, elneg, ionization, elaffinity, period, group, PubChem, phase, Hf, S0, InChI_key=None)
Class for storing data on chemical elements. Supports most common properties. If a property is not available, it is set to None.

The elements are created automatically and should be accessed via the periodic_table interface.

## Attributes

number [int] Atomic number, [-]
name [str] name, [-]
symbol [str] Elemental symbol, [-]
MW [float] Molecular weight, [ $\mathrm{g} / \mathrm{mol}$ ]
CAS [str] CAS number, [-]
period [str] Period in the periodic table, [-]
group [str] Group in the periodic table, [-]
block [str] Which block of the periodic table the element is in.
AReneg [float] Allred and Rochow electronegativity, [-]
rcov [float] Covalent radius, [Angstrom]
rvdw [float] Van der Waals radius, [Angstrom]
maxbonds [float] Maximum valence of a bond with this element, [-]
elneg [float] Pauling electronegativity, [-]
ionization [float] Ionization potential, $[\mathrm{eV}$ ]
ionization [float] elaffinity affinity, [eV]
protons [int] The number of protons of the element.
electrons [int] The number of electrons of the element.
InChI [str] The InChI identifier of the element.
InChI_key [str] 25-character hash of the compound's InChI, [-]
smiles [str] The SMILES identification string of the element.
PubChem [int] PubChem Compound identifier (CID) of the chemical, [-]
phase [str] Standard state at 1 atm and $298.15 \mathrm{~K},[-]$
Hf [float] Enthalpy of formation of the element in its standard state ( 0 by definition), [ $\mathrm{J} / \mathrm{mol}$ ]
$\mathbf{S 0}$ [float] Standard absolute entropy of the element in its standard state (1 bar, 298.15 K), [J/mol/K]

## class chemicals.elements.PeriodicTable(elements)

Periodic Table object for use in dealing with elements.
As there is only one periodic table of elements, this is automatically initialized into the object periodic_table; there is no need to construct a new instance of this class.

## Parameters

elements [list[Element]] List of Element objects, [-]

## See also:

periodic_table
Element

## Notes

Can be checked to sese if an element in in this, can be iterated over, and as a current length of 118 elements.

## References

[1]

### 1.8.2 Working with Formulas

chemicals.elements.simple_formula_parser(formula)
Basic formula parser, primarily for obtaining element counts from formulas as formated in PubChem. Handles formulas with integer or decimal counts (with period separator), but no brackets, no hydrates, no charges, no isotopes, and no group multipliers.

Strips charges from the end of a formula first. Accepts repeated chemical units. Performs no sanity checking that elements are actually elements. As it uses regular expressions for matching, errors are mostly just ignored.

## Parameters

formula [str] Formula string, very simply formats only.

## Returns

atoms [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

## Notes

Inspiration taken from the thermopyl project, at https://github.com/choderalab/thermopyl.

## Examples

>>> simple_formula_parser('CO2')
\{'C': 1, '0': 2\}
chemicals.elements.nested_formula_parser(formula, check=True)
Improved formula parser which handles braces and their multipliers, as well as rational element counts.
Strips charges from the end of a formula first. Accepts repeated chemical units. Performs no sanity checking that elements are actually elements. As it uses regular expressions for matching, errors are mostly just ignored.

## Parameters

formula [str] Formula string, very simply formats only.
check [bool] If check is True, a simple check will be performed to determine if a formula is not a formula and an exception will be raised if it is not, [-]

## Returns

atoms [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

## Notes

Inspired by the approach taken by CrazyMerlyn on a reddit DailyProgrammer challenge, at https://www.reddit. com/r/dailyprogrammer/comments/6eerfk/20170531_challenge_317_intermediate_counting/

## Examples

>>> nested_formula_parser('Pd(NH3)4.0001+2')
\{'Pd': 1, 'N': 4.0001, 'H': 12.0003$\}$

## chemicals.elements.charge_from_formula (formula)

Basic formula parser to determine the charge from a formula - given that the charge is already specified as one element of the formula.

Performs no sanity checking that elements are actually elements.

## Parameters

formula [str] Formula string, very simply formats only, ending in one of ' +x ', ' -x ', $\mathrm{n}^{\text {*' }}+$ ', or $\mathrm{n}^{*}$ '-' or any of them surrounded by brackets but always at the end of a formula.

## Returns

charge [int] Charge of the molecule, [faraday]

## Examples

```
>>> charge_from_formula('Br3-')
-1
>>> charge_from_formula('Br3(-)')
-1
```

chemicals.elements.serialize_formula(formula)
Basic formula serializer to construct a consistently-formatted formula. This is necessary for handling usersupplied formulas, which are not always well formatted.
Performs no sanity checking that elements are actually elements.

## Parameters

formula [str] Formula string as parseable by the method nested_formula_parser, [-]

## Returns

formula [str] A consistently formatted formula to describe a molecular formula, [-]

## Examples

```
>>> serialize_formula('Pd(NH3)4+3')
'H12N4Pd+3'
```


## chemicals.elements.atoms_to_Hill(atoms)

Determine the Hill formula of a compound, given a dictionary of its atoms and their counts, in the format \{symbol: count $\}$.

## Parameters

atoms [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

## Returns

Hill_formula [str] Hill formula, [-]

## Notes

The Hill system is as follows:
If the chemical has ' $C$ ' in it, this is listed first, and then if it has ' $H$ ' in it as well as ' $C$ ', then that goes next. All elements are sorted alphabetically afterwards, including ' H ' if ' C ' is not present. All elements are followed by their count, unless it is 1 .

## References

[1]

Examples
>>> atoms_to_Hill(\{'H': 5, 'C': 2, 'Br': 1\})
'C2H5Br'

### 1.8.3 Working with Parsed Formulas

## chemicals.elements.molecular_weight (atoms)

Calculates molecular weight of a molecule given a dictionary of its atoms and their counts, in the format \{symbol: count $\}$.

$$
M W=\sum_{i} n_{i} M W_{i}
$$

## Parameters

atoms [dict] Dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

## Returns

MW [float] Calculated molecular weight [g/mol]

## Notes

Elemental data is from rdkit, with CAS numbers added. An exception is raised if an incorrect element symbol is given. Elements up to 118 are supported, as are deutreium and tritium.

## References

[1]

## Examples

>>> molecular_weight(\{'H': 12, 'C': 20, '0': 5\}) \# DNA 332.30628
chemicals.elements.similarity_variable(atoms, $M W=$ None)
Calculates the similarity variable of an compound, as defined in [1]. Currently only applied for certain heat capacity estimation routines.

$$
\alpha=\frac{N}{M W}=\frac{\sum_{i} n_{i}}{\sum_{i} n_{i} M W_{i}}
$$

## Parameters

atoms [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

MW [float, optional] Molecular weight, [ $\mathrm{g} / \mathrm{mol}$ ]

## Returns

similarity_variable [float] Similarity variable as defined in [1], [mol/g]

## Notes

Molecular weight is optional, but speeds up the calculation slightly. It is calculated using the function molecular_weight if not specified.

## References

[1]

Examples
>>> similarity_variable(\{'H': 32, 'C': 15\})
0. 2212654140784498

## chemicals.elements.index_hydrogen_deficiency(atoms)

Calculate the index of hydrogen deficiency of a compound, given a dictionary of its atoms and their counts, in the format $\{$ symbol: count $\}$.

## Parameters

atoms [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

## Returns

HDI [float] Hydrogen deficiency index, [-]

## Notes

The calculation is according to:

$$
\mathrm{IDH}=0.5(2 C+2+N-H-X+0 O)
$$

where $X$ is the number of halogen atoms. The number of oxygen atoms does not impact this calculation.

## References

[1]

## Examples

Agelastatin A:
>>> index_hydrogen_deficiency(\{'C': 12, 'H': 13, 'Br': 1, 'N': 4, 'O': 3\})
8.0

## chemicals.elements.atom_fractions(atoms)

Calculates the atomic fractions of each element in a compound, given a dictionary of its atoms and their counts, in the format $\{$ symbol: count $\}$.

$$
a_{i}=\frac{n_{i}}{\sum_{i} n_{i}}
$$

## Parameters

atoms [dict] dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

## Returns

afracs [dict] dictionary of atomic fractions of individual atoms, indexed by symbol with proper capitalization, [-]

## Notes

No actual data on the elements is used, so incorrect or custom compounds would not raise an error.

## References

[1]

## Examples

>>> atom_fractions(\{'H': 12, 'C': 20, '0': 5\})
\{'H': 0.32432432432432434, 'C': 0.5405405405405406, 'O': 0.13513513513513514\}
chemicals.elements.mass_fractions(atoms, $M W=$ None)
Calculates the mass fractions of each element in a compound, given a dictionary of its atoms and their counts, in the format $\{$ symbol: count $\}$.

$$
w_{i}=\frac{n_{i} M W_{i}}{\sum_{i} n_{i} M W_{i}}
$$

## Parameters

atoms [dict] Dictionary of counts of individual atoms, indexed by symbol with proper capitalization, [-]

MW [float, optional] Molecular weight, [ $\mathrm{g} / \mathrm{mol}$ ]

## Returns

mfracs [dict] Dictionary of mass fractions of individual atoms, indexed by symbol with proper capitalization, [-]

## Notes

Molecular weight is optional, but speeds up the calculation slightly. It is calculated using the function molecular_weight if not specified.
Elemental data is from rdkit, with CAS numbers added. An exception is raised if an incorrect element symbol is given. Elements up to 118 are supported.

## References

## [1]

## Examples

```
>>> mass_fractions({'H': 12, 'C': 20, 'O': 5})
{'H': 0.03639798802478244, 'C': 0.7228692758981262, 'O': 0.24073273607709128}
```

chemicals.elements.mixture_atomic_composition(atomss, zs)
Simple function to calculate the atomic average composition of a mixture, using the mole fractions of each species and their own atomic compositions.

## Parameters

atomss [list[dict[(str, int)]]] List of dictionaries of atomic compositions, [-]
zs [list[float]] Mole fractions of each component, [-]

## Returns

atoms [dict[(str, int)]] Atomic composition

## Examples

```
>>> mixture_atomic_composition([{'0': 2}, {'N': 1, '0': 2}, {'C': 1, 'H': 4}], [0.
495, 0.025, .025])
{'0': 1.95, 'N': 0.025, 'C': 0.025, 'H': 0.1}
```


## chemicals.elements.mixture_atomic_composition_ordered(atomss, zs)

Simple function to calculate the atomic average composition of a mixture, using the mole fractions of each species and their own atomic compositions. Returns the result as a sorted list with atomic numbers from low to high.

## Parameters

atomss [list[dict[(str, int)]]] List of dictionaries of atomic compositions, [-]
zs [list[float]] Mole fractions of each component; this can also be a molar flow rate and then the abundances will be flows, [-]

## Returns

abundances [list[float]] Number of atoms of each element per mole of the feed, [-]
atom_keys [list[str]] Atomic elements, sorted from lowest atomic number to highest

## Notes

Useful to ensure a matrix order is consistent in multiple steps.

## Examples

>>> mixture_atomic_composition_ordered([\{'0': 2\}, \{'N': 1, 'O': 2\}, \{'C': 1, 'H': 4\} $\rightarrow],[0.95,0.025, .025])$
([0.1, 0.025, 0.025, 1.95], ['H', 'C', 'N', 'O'])
chemicals.elements.atom_matrix (atomss, atom_IDs=None)
Simple function to create a matrix of elements in each compound, where each row has the same elements.

## Parameters

atomss [list[dict[(str, int)]]] List of dictionaries of atomic compositions, [-]
atom_IDs [list[str], optional] Optionally, a subset (or simply ordered differently) of elements to consider, [-]

## Returns

matrix [list[list[float]]] The number of each element in each compound as a matrix, indexed as [compound][element], [-]

## Examples

```
>>> atom_matrix([{'C': 1, 'H': 4}, {'C': 2, 'H': 6}, {'N': 2}, {'0': 2}, {'H': 2, '0
    \leftrightarrow': 1}, {'C': 1, '0': 2}])
[[4, 1, 0.0, 0.0], [6, 2, 0.0, 0.0], [0.0, 0.0, 2, 0.0], [0.0, 0.0, 0.0, 2], [2, 0.
\bullet,0.0, 1], [0.0, 1, 0.0, 2]]
```


### 1.9 Environmental Properties (chemicals.environment)

This module contains lookup functions for three important environmental properties - Global Warming Potential, Ozone Depletion Potential, and octanol-water partition coefficient.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Global Warming Potential
- Ozone Depletion Potential
- Octanol-Water Partition Coefficient


### 1.9.1 Global Warming Potential

## chemicals.environment. GWP (CASRN, method=None)

This function handles the retrieval of a chemical's Global Warming Potential, relative to CO2. Lookup is based on CASRNs.

There are three sources of data:

- IPCC Fifth Assessment Report (AR5) from 2014 [2]
- IPCC Fourth Assessment Report (AR4) from 2007 [1]
- IPCC Second Assesment Report or (SAR) from 1995 [1]

This function returns the GWP for the 20yr outlook from the AR5 by default.

## Parameters

CASRN [str] CASRN [-]

## Returns

GWP [float] Global warming potential, [(impact/mass chemical)/(impact/mass CO2)]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are ('IPCC (2014) 100yr', 'IPCC (2014) 20yr', ‘IPCC (2007) 100yr', 'IPCC (2007) 20yr', 'IPCC (2007) 500yr', 'IPCC (1995) 100yr'). All valid values are also held in the variable GWP_all_methods.

## See also:

GWP_methods

## Notes

"Fossil methane" is included in the IPCC reports to take into account different isotopic composition, but as that has the same CAS number it is not included in this function.

Six of the entries in [2] are actually duplicates; the entries with data similar to more recent data [3] were prefered.

## References

[1], [2], [3]

## Examples

Methane, 20-yr outlook AR5

```
>>> GWP(CASRN='74-82-8')
84.0
```

Methane, specifying the default method explicitly (this is recommended the default data source may be updated in the future)

```
>>> GWP(CASRN='74-82-8', method='IPCC (2014) 100yr')
```

28.0

Methane, 20-year values from 1995 and 2007
>>> (GWP(CASRN='74-82-8', method='IPCC (1995) 100yr'), GWP(CASRN='74-82-8', method= $\rightarrow$ 'IPCC (2007) 100yr'))
(21.0, 25.0)
chemicals.environment.GWP_methods (CASRN)
Return all methods available to obtain GWP for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain GWP with the given inputs.
See also:

GWP
chemicals.environment.GWP_all_methods = ('IPCC (2014) 100yr', 'IPCC (2014) 20yr', 'IPCC (2007) $100 \mathrm{yr} ', ~ ' I P C C ~(2007) ~ 20 y r ', ~ ' I P C C ~(2007) ~ 500 y r ', ~ ' I P C C ~(1995) ~ 100 y r ') ~$

Tuple of method name keys. See the GWP for the actual references

### 1.9.2 Ozone Depletion Potential

chemicals.environment. ODP (CASRN, method=None)
This function handles the retrieval of a chemical's Ozone Depletion Potential, relative to CFC-11 (trichlorofluoromethane). Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.
Returns the ODP of a chemical according to [2] when a method is not specified. If a range is provided in [2], the highest value is returned.

## Parameters

CASRN [str] CASRN [-]

## Returns

ODP [float or str] Ozone Depletion potential, [(impact/mass chemical)/(impact/mass CFC-11)]; if method selected has string in it, this will be returned as a string regardless of if a range is given or a number

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'ODP2 Max', 'ODP2 Min', 'ODP2 string', 'ODP2 logarithmic average', and methods for older values are 'ODP1 Max', 'ODP1 Min', 'ODP1 string', and 'ODP1 logarithmic average'. All valid values are also held in the list ODP_methods.

## Notes

Values are tabulated only for a small number of halogenated hydrocarbons, responsible for the largest impact. The original values of ODP as defined in the Montreal Protocol are also available, as methods with the ODP1 prefix.

All values are somewhat emperical, as actual reaction rates of chemicals with ozone depend on temperature which depends on latitude, longitude, time of day, weather, and the concentrations of other pollutants.

All data is from [1]. Several mixtures listed in [1] are not included here as they are not pure species. Methods for values in [2] are 'ODP2 Max', 'ODP2 Min', 'ODP2 string', 'ODP2 logarithmic average', and methods for older values are 'ODP1 Max', 'ODP1 Min', 'ODP1 string', and ‘ODP1 logarithmic average'.

## References

[1], [2]

## Examples

Dichlorotetrafluoroethane, according to [2].

```
>>> ODP(CASRN='76-14-2')
0.58
```

chemicals.environment. ODP_methods ( $C A S R N$ )
Return all methods available to obtain ODP for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain ODP with the given inputs.

## See also:

ODP

```
chemicals.environment.ODP_all_methods = ('ODP2 Max', 'ODP1 Max', 'ODP2 logarithmic
average', 'ODP1 logarithmic average', 'ODP2 Min', 'ODP1 Min', 'ODP2 string', 'ODP1
string')
Tuple of method name keys. See the \(O D P\) for the actual references
```


### 1.9.3 Octanol-Water Partition Coefficient

## chemicals.environment. $\log \mathrm{P}(C A S R N$, method=None $)$

This function handles the retrieval of a chemical's octanol-water partition coefficient. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

## Parameters

CASRN [str] CASRN [-]

## Returns

$\log \mathbf{P}$ [float] Octanol-water partition coefficient, [-]

## Other Parameters

method [string, optional] The method name to use. Accepted methods are 'SYRRES', 'CRC', and 'WIKIDATA'. All valid values are also held in the list logP_methods.

## Notes

Although matimatically this could be expressed with a logarithm in any base, reported values are published using a base 10 logarithm.

$$
\log _{10} P_{\text {oct } / \text { wat }}=\log _{10}\left(\frac{[\text { solute }]_{\text {octanol }}^{\text {un-ionized }}}{[\text { solute }]_{\text {water }}^{\text {un-ionized }}}\right)
$$

## References

[1], [2]

## Examples

```
>>> logP('67-56-1')
-0.74
>>> logP('100-66-3', 'WIKIDATA')
2.11
```


## chemicals.environment.logP_methods(CASRN)

Return all methods available to obtain $\log \mathrm{P}$ for the desired chemical.

## Parameters

CASRN [str] CASRN, [-]

## Returns

methods [list[str]] Methods which can be used to obtain $\log \mathrm{P}$ with the given inputs.
See also:
$\log P$
chemicals.environment.logP_all_methods = ('SYRRES', 'CRC', 'WIKIDATA')
Tuple of method name keys. See the $\log P$ for the actual references

### 1.10 Exceptions Generated by Chemicals (chemicals.exceptions)

This module contains various exception classes that may be raised by chemicals.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
class chemicals.exceptions.UnderspecifiedError
Generic error to raise when not enough values are given.

## Attributes

## args

## Methods

| with_traceback | Exception.with_traceback(tb) <br> self.__traceback__ to tb and return self. | set |
| :--- | :--- | :--- |

class chemicals.exceptions.OverspeficiedError
Generic error to raise when too many values are given.

## Attributes

args

Methods

| with_traceback | Exception.with_traceback(tb)-- <br> self.__traceback__ to tb and return self. |
| :--- | :--- |

class chemicals.exceptions.TrivialSolutionError(message, comp_difference $=$ None, iterations=None, err=None)
Error raised SS converges to trivial solution.

## Attributes

> args

Methods

| with_traceback | Exception.with_traceback(tb)-- <br> self._traceback__to tb and return self. |
| :--- | :--- | :--- |

class chemicals.exceptions.PhaseCountReducedError (message, $z s=N o n e, K s=N o n e$ )
Error raised SS inner flash loop says all Ks are under 1 or above 1.

## Attributes

args

Methods

with_traceback | Exception.with_traceback(tb) |
| :--- | :--- | :--- |
| self. traceback_ to tb and return self. |

class chemicals.exceptions.PhaseExistenceImpossible(message, $z s=$ None, $T=$ None, $P=$ None)
Error raised SS inner flash loop says all Ks are under 1 or above 1.

## Attributes

args

Methods

### 1.11 Ideal VLE and Flash Initialization (chemicals.flash_basic)

This module contains the ideal flash solver; two flash initialization routines; a vapor-liquid equilibrium constant correlation; a liquid-water equilibrium constant correlation, and a definition function to show the commonly used calculation frameworks.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Ideal Flash Function
- Flash Initialization
- Equilibrium Constants


### 1.11.1 Ideal Flash Function

chemicals.flash_basic.flash_ideal(zs, funcs, Tcs=None, $T=N o n e, ~ P=N o n e, V F=N o n e)$

PVT flash model using ideal, composition-independent equation. Solves the various cases of compositionindependent models.

Capable of solving with two of $T, P$, and $V F$ for the other one; that results in three solve modes, but for $V F=1$ and $V F=0$, there are additional solvers; for a total of seven solvers implemented.

The function takes a list of callables that take $T$ in Kelvin as an argument, and return vapor pressure. The callables can include the effect of non-ideal pure component fugacity coefficients. For the $(T, P)$ and $(P, V F)$ cases, the Poynting correction factor can be easily included as well but not the ( $T, V F$ ) case as the callable only takes $T$ as an argument. Normally the Poynting correction factor is used with activity coefficient models with composition dependence.

Both flash_wilson and flash_Tb_Tc_Pc are specialized cases of this function and have the same functionality but with the model built right in.

Even when using more complicated models, this is useful for obtaining initial
This model uses flash_inner_loop to solve the Rachford-Rice problem.

## Parameters

zs [list[float]] Mole fractions of the phase being flashed, [-]
funcs [list[Callable]] Functions to calculate ideal or real vapor pressures, take temperature in Kelvin and return pressure in $\mathrm{Pa},[-]$

Tes [list[float], optional] Critical temperatures of all species; uses as upper bounds and only for the case that $T$ is not specified; if they are needed and not given, it is assumed a method solve_prop exists in each of funcs which will accept $P$ in Pa and return temperature in $K$, [K]

T [float, optional] Temperature, [K]
$\mathbf{P}$ [float, optional] Pressure, [Pa]

VF [float, optional] Molar vapor fraction, [-]

## Returns

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]
VF [float] Molar vapor fraction, [-]
xs [list[float]] Mole fractions of liquid phase, [-]
ys [list[float]] Mole fractions of vapor phase, [-]

## Notes

For the cases where $V F$ is 1 or 0 and T is known, an explicit solution is used. For the same cases where $P$ and $V F$ are known, there is no explicit solution available.

There is an internal Tmax parameter, set to 50000 K ; which, in the event of convergence of the Secant method, is used as a bounded for a bounded solver. It is used in the PVF solvers.

## Examples

Basic case with four compounds, usingthe Antoine equation as a model and solving for vapor pressure:

```
>>> from chemicals import Antoine, Ambrose_Walton
>>> Tcs = [369.83, 425.12, 469.7, 507.6]
>>> Antoine_As = [8.92828, 8.93266, 8.97786, 9.00139]
>>> Antoine_Bs = [803.997, 935.773, 1064.84, 1170.88]
>>> Antoine_Cs = [-26.11, -34.361, -41.136, -48.833]
>>> Psat_funcs = []
>> for i in range(4):
... def Psat_func(T, A=Antoine_As[i], B=Antoine_Bs[i], C=Antoine_Cs[i]):
... return Antoine(T, A, B, C)
... Psat_funcs.append(Psat_func)
>>> zs = [.4, .3, .2, .1]
>>> T, P, VF, xs, ys = flash_ideal(T=330.55, P=1e6, zs=zs, funcs=Psat_funcs,, ь
    Tcs=Tcs)
>>> round(VF, 10)
1.00817e-05
```

Similar case, using the Ambrose-Walton corresponding states method to estimate vapor pressures:

```
>>> Tcs = [369.83, 425.12, 469.7, 507.6]
>>> Pcs = [4248000.0, 3796000.0, 3370000.0, 3025000.0]
>>> omegas = [0.152, 0.193, 0.251, 0.2975]
>>> Psat_funcs = []
>>> for i in range(4):
... def Psat_func(T, Tc=Tcs[i], Pc=Pcs[i], omega=omegas[i]):
#. return Ambrose_Walton(T, Tc, Pc, omega)
... Psat_funcs.append(Psat_func)
>>> _, P, VF, xs, ys = flash_ideal(T=329.151, VF=0, zs=zs, funcs=Psat_funcs,ь
    \rightarrow T c s = T c s )
>>> round(P, 3)
1000013.343
```

Case with fugacities in the liquid phase, vapor phase, activity coefficients in the liquid phase, and Poynting correction factors.

```
>>> Tcs = [647.14, 514.0]
>>> Antoine_As = [10.1156, 10.3368]
>>> Antoine_Bs = [1687.54, 1648.22]
>>> Antoine_Cs = [-42.98, -42.232]
>>> gammas = [1.1, .75]
>>> fugacities_gas = [.995, 0.98]
>>> fugacities_liq = [.9999, .9998]
>>> Poyntings = [1.000001, .999999]
>>> zs = [.5, .5]
>>> funcs = []
>>> for i in range(2):
... def K_over_P(T, A=Antoine_As[i], B=Antoine_Bs[i], C=Antoine_Cs[i],七
๑f=fugacities_liq[i],
fg=fugacities_gas[i], gamma=gammas[i], poy=Poyntings[i]):
... funcs.append(K_over_P)
>>> _, _, VF, xs, ys = flash_ideal(zs, funcs, Tcs=Tcs, P=1e5, T=364.0)
>>> VF, xs, ys
(0.5108639717, [0.55734934039, 0.44265065960], [0.44508982795, 0.554910172040])
```

Note that while this works for PT composition independent flashes - an outer iterating loop is needed for composition dependence!

### 1.11.2 Flash Initialization

## chemicals.flash_basic.flash_wilson(zs, Tcs, Pcs, omegas, $T=$ None, $P=N o n e, V F=N o n e$ )

PVT flash model using Wilson's equation - useful for obtaining initial guesses for more rigorous models, or it can be used as its own model. Capable of solving with two of $T, P$, and $V F$ for the other one; that results in three solve modes, but for $V F=1$ and $V F=0$, there are additional solvers; for a total of seven solvers implemented.

This model uses flash_inner_loop to solve the Rachford-Rice problem.

$$
K_{i}=\frac{P_{c}}{P} \exp \left(5.37(1+\omega)\left[1-\frac{T_{c}}{T}\right]\right)
$$

## Parameters

zs [list[float]] Mole fractions of the phase being flashed, [-]
Tcs [list[float]] Critical temperatures of all species, [K]
Pcs [list[float]] Critical pressures of all species, [Pa]
omegas [list[float]] Acentric factors of all species, [-]
T [float, optional] Temperature, [K]
$\mathbf{P}$ [float, optional] Pressure, [Pa]
VF [float, optional] Molar vapor fraction, [-]

## Returns

$\mathbf{T}$ [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

```
VF [float] Molar vapor fraction, [-]
xs [list[float]] Mole fractions of liquid phase, [-]
ys [list[float]] Mole fractions of vapor phase, [-]
```


## Notes

For the cases where $V F$ is 1 or 0 and T is known, an explicit solution is used. For the same cases where $P$ and $V F$ are known, there is no explicit solution available.

There is an internal Tmax parameter, set to 50000 K ; which, in the event of convergence of the Secant method, is used as a bounded for a bounded solver. It is used in the PVF solvers. This typically allows pressures up to 2 GPa to be converged to. However, for narrow-boiling mixtures, the PVF failure may occur at much lower pressures.

## Examples

```
>>> Tcs = [305.322, 540.13]
>>> Pcs = [4872200.0, 2736000.0]
>>> omegas = [0.099, 0.349]
>> zs = [0.4, 0.6]
>>> flash_wilson(zs=zs, Tcs=Tcs, Pcs=Pcs, omegas=omegas, T=300, P=1e5)
(300, 100000.0, 0.422194532936, [0.02093881508003, 0.979061184919], [0.918774185622,
0.0812258143])
```

chemicals.flash_basic.flash_Tb_Tc_Pc (zs, Tbs, Tcs, Pcs, $T=N o n e, ~ P=N o n e, V F=N o n e) ~$
PVT flash model using a model published in [1], which provides a PT surface using only each compound's boiling temperature and critical temperature and pressure. This is useful for obtaining initial guesses for more rigorous models, or it can be used as its own model. Capable of solving with two of $T, P$, and $V F$ for the other one; that results in three solve modes, but for $V F=1$ and $V F=0$, there are additional solvers; for a total of seven solvers implemented.
This model uses flash_inner_loop to solve the Rachford-Rice problem.

$$
K_{i}=\frac{P_{c, i}^{\left(\frac{1}{T}-\frac{1}{T_{b, i}}\right) /\left(\frac{1}{T_{c, i}}-\frac{1}{T_{b, i}}\right)}}{P}
$$

## Parameters

zs [list[float]] Mole fractions of the phase being flashed, [-]
Tbs [list[float]] Boiling temperatures of all species, [K]
Tcs [list[float]] Critical temperatures of all species, [K]
Pcs [list[float]] Critical pressures of all species, [Pa]
T [float, optional] Temperature, [K]
$\mathbf{P}$ [float, optional] Pressure, [Pa]
VF [float, optional] Molar vapor fraction, [-]

## Returns

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]
VF [float] Molar vapor fraction, [-]
xs [list[float]] Mole fractions of liquid phase, [-]
ys [list[float]] Mole fractions of vapor phase, [-]

## Notes

For the cases where $V F$ is 1 or 0 and T is known, an explicit solution is used. For the same cases where $P$ and $V F$ are known, there is no explicit solution available.
There is an internal Tmax parameter, set to 50000 K ; which, in the event of convergence of the Secant method, is used as a bounded for a bounded solver. It is used in the PVF solvers. This typically allows pressures up to 2 MPa to be converged to. Failures may still occur for other conditions.

This model is based on [1], which aims to estimate dew and bubble points using the same K value formulation as used here. While this implementation uses a numerical solver to provide an exact bubble/dew point estimate, [1] suggests a sequential substitution and flowchart based solver with loose tolerances. That model was also implemented, but found to be slower and less reliable than this implementation.

## References

[1]

## Examples

```
>> Tcs = [305.322, 540.13]
>>> Pcs = [4872200.0, 2736000.0]
>>> Tbs = [184.55, 371.53]
>>> zs = [0.4, 0.6]
>>> flash_Tb_Tc_Pc(zs=zs, Tcs=Tcs, Pcs=Pcs, Tbs=Tbs, T=300, P=1e5)
(300, 100000.0, 0.3807040748145, [0.0311578430365, 0.968842156963], [0.
\leftrightarrows9999999998827, 1.1729141887e-10])
```


### 1.11.3 Equilibrium Constants

chemicals.flash_basic.K_value( $P=$ None, $P s a t=N o n e, p h i \_l=N o n e, p h i \_g=N o n e$, gamma=None, Poynting=1.0)
Calculates the equilibrium K-value assuming Raoult's law, or an equation of state model, or an activity coefficient model, or a combined equation of state-activity model.

The calculation procedure will use the most advanced approach with the provided inputs:

- If $P$, Psat, phi_l, phi_g, and gamma are provided, use the combined approach.
- If $P$, Psat, and gamma are provided, use the modified Raoult's law.
- If $p h i_{-} l$ and $p h i_{-} g$ are provided, use the EOS only method.
- If $P$ and Psat are provided, use Raoult's law.

Definitions:

$$
K_{i}=\frac{y_{i}}{x_{i}}
$$

Raoult's law:

$$
K_{i}=\frac{P_{i}^{s a t}}{P}
$$

Activity coefficient, no EOS (modified Raoult's law):

$$
K_{i}=\frac{\gamma_{i} P_{i}^{s a t}}{P}
$$

Equation of state only:

$$
K_{i}=\frac{\phi_{i}^{l}}{\phi_{i}^{v}}=\frac{f_{i}^{l} y_{i}}{f_{i}^{v} x_{i}}
$$

Combined approach (liquid reference fugacity coefficient is normally calculated the saturation pressure for it as a pure species; vapor fugacity coefficient calculated normally):

$$
K_{i}=\frac{\gamma_{i} P_{i}^{s a t} \phi_{i}^{l, \text { ref }}}{\phi_{i}^{v} P}
$$

Combined approach, with Poynting Correction Factor (liquid molar volume in the integral is for $i$ as a pure species only):

$$
K_{i}=\frac{\gamma_{i} P_{i}^{\text {sat }} \phi_{i}^{l, \text { ref }} \exp \left[\frac{\int_{P_{i}^{s a t}}^{P} V_{i}^{l} d P}{R T}\right]}{\phi_{i}^{v} P}
$$

## Parameters

$\mathbf{P}$ [float] System pressure, optional
Psat [float] Vapor pressure of species i, [Pa]
phi_l [float] Fugacity coefficient of species i in the liquid phase, either at the system conditions (EOS-only case) or at the saturation pressure of species i as a pure species (reference condition for the combined approach), optional [-]
phi_g [float] Fugacity coefficient of species i in the vapor phase at the system conditions, optional [-]
gamma [float] Activity coefficient of species i in the liquid phase, optional [-]
Poynting [float] Poynting correction factor, optional [-]

## Returns

K [float] Equilibrium K value of component i, calculated with an approach depending on the provided inputs [-]

## Notes

The Poynting correction factor is normally simplified as follows, due to a liquid's low pressure dependency:

$$
K_{i}=\frac{\gamma_{i} P_{i}^{s a t} \phi_{i}^{l, r e f} \exp \left[\frac{V_{l}\left(P-P_{i}^{s a t}\right)}{R T}\right]}{\phi_{i}^{v} P}
$$

## References

[1], [2]

## Examples

Raoult's law:

```
>>> K_value(101325, 3000.)
```

0.029607698001480384

Modified Raoult's law:

```
>>> K_value(P=101325, Psat=3000, gamma=0.9)
0.026646928201332347
```

EOS-only approach:

```
>>> K_value(phi_l=1.6356, phi_g=0.88427)
```

1.8496613025433408

Gamma-phi combined approach:

```
>>> K_value(P=1E6, Psat=1938800, phi_l=1.4356, phi_g=0.88427, gamma=0. 92)
2.8958055544121137
```

Gamma-phi combined approach with a Poynting factor:
>>> K_value(P=1E6, Psat=1938800, phi_l=1.4356, phi_g=0.88427, gamma=0.92,
... Poynting=0.999)
2.8929097488577016
chemicals.flash_basic. Wilson_K_value $(T, P, T c, P c$, omega)
Calculates the equilibrium K-value for a component using Wilson's heuristic mode. This is very useful for initialization of stability tests and flashes.

$$
K_{i}=\frac{P_{c}}{P} \exp \left(5.37(1+\omega)\left[1-\frac{T_{c}}{T}\right]\right)
$$

## Parameters

$\mathbf{T}$ [float] System temperature, [K]
$\mathbf{P}$ [float] System pressure, [Pa]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor for fluid, [-]

## Returns

$\mathbf{K}$ [float] Equilibrium K value of component, calculated via the Wilson heuristic [-]

## Notes

There has been little literature exploration of other formlulas for the same purpose. This model may be useful even for activity coefficient models.

Note the K-values are independent of composition; the correlation is applicable up to 3.5 MPa .
A description for how this function was generated can be found in [2].

## References

[1], [2]

## Examples

Ethane at 270 K and 76 bar:

```
>>> Wilson_K_value(270.0, 7600000.0, 305.4, 4880000.0, 0.098)
```

Q. 2963932297479371

The "vapor pressure" predicted by this equation can be calculated by multiplying by pressure:
>>> Wilson_K_value(270.0, 7600000.0, 305.4, 4880000.0, 0.098)*7600000.0 2252588.546084322
chemicals.flash_basic.PR_water_K_value ( $T, P, T c, P c$ )
Calculates the equilibrium K-value for a component against water according to the Peng and Robinson (1976) heuristic.

$$
K_{i}=10^{6} \frac{P_{r i}}{T_{r i}}
$$

## Parameters

$\mathbf{T}$ [float] System temperature, [K]
$\mathbf{P}$ [float] System pressure, $[\mathrm{Pa}]$
Tc [float] Critical temperature of chemical [K]
Pc [float] Critical pressure of chemical [Pa]

## Returns

$\mathbf{K}$ [float] Equilibrium K value of component with water as the other phase ( not as the reference), calculated via this heuristic [-]

## Notes

Note the K-values are independent of composition.

## References

[1]

## Examples

Octane at 300 K and 1 bar:

```
>>> PR_water_K_value(300, 1e5, 568.7, 2490000.0)
```

76131.19143239626

### 1.12 Heat Capacity (chemicals.heat_capacity)

This module contains many heat capacity model equations, heat capacity estimation equations, enthalpy and entropy integrals of those heat capacity equations, enthalpy/entropy flash initialization routines, and many dataframes of coefficients.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Gas Heat Capacity Model Equations
- Gas Heat Capacity Estimation Models
- Gas Heat Capacity Theory
- Liquid Heat Capacity Model Equations
- Liquid Heat Capacity Estimation Models
- Solid Heat Capacity Estimation Models
- Utility methods
- Fit Coefficients


### 1.12.1 Gas Heat Capacity Model Equations

## chemicals.heat_capacity. $\operatorname{TRCCp}(T, a 0, a 1, a 2, a 3, a 4, a 5, a 6, a 7)$

Calculates ideal gas heat capacity using the model developed in [1]. The ideal gas heat capacity is given by:

$$
\begin{gathered}
C_{p}=R\left(a_{0}+\left(a_{1} / T^{2}\right) \exp \left(-a_{2} / T\right)+a_{3} y^{2}+\left(a_{4}-a_{5} /\left(T-a_{7}\right)^{2}\right) y^{j}\right) \\
y=\frac{T-a_{7}}{T+a_{6}} \text { for } T>a_{7} \text { otherwise } 0
\end{gathered}
$$

## Parameters

$\mathbf{T}$ [float] Temperature [K]
a1-a7 [float] Coefficients

## Returns

$\mathbf{C p}$ [float] Ideal gas heat capacity, $[\mathrm{J} / \mathrm{mol} / \mathrm{K}$ ]

## Notes

j is set to 8 . Analytical integrals are available for this expression.

## References

[1]

## Examples

>> $\operatorname{TRCCp}(300,4.0,7.65 E 5,720 ., 3.565,-0.052,-1.55 E 6,52 ., 201$.
42.065271080974654
chemicals.heat_capacity.TRCCp_integral( $T, a 0, a 1, a 2, a 3, a 4, a 5, a 6, a 7, I=0$ )
Integrates ideal gas heat capacity using the model developed in [1]. Best used as a delta only. The difference in enthalpy with respect to 0 K is given by:

$$
\begin{gathered}
\frac{H(T)-H^{\text {ref }}}{R T}=a_{0}+a_{1} x\left(a_{2}\right) /\left(a_{2} T\right)+I / T+h(T) / T \\
h(T)=\left(a_{5}+a_{7}\right)\left[\left(2 a_{3}+8 a_{4}\right) \ln (1-y)+\left\{a_{3}\left(1+\frac{1}{1-y}\right)+a_{4}\left(7+\frac{1}{1-y}\right)\right\} y+a_{4}\left\{3 y^{2}+(5 / 3) y^{3}+y^{4}+(3 / 5) y^{5}+\right.\right. \\
h(T)=0 \text { for } T \leq a_{7} y=\frac{T-a_{7}}{T+a_{6}} \text { for } T>a_{7} \text { otherwise } 0
\end{gathered}
$$

## Parameters

T [float] Temperature [K]
a1-a7 [float] Coefficients
I [float, optional] Integral offset

## Returns

$\mathbf{H}-\mathbf{H}(\mathbf{0})$ [float] Difference in enthalpy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol}]$

## Notes

Analytical integral as provided in [1] and verified with numerical integration.

## References

[1]

## Examples

>>> TRCCp_integral(298.15, 4.0, 7.65E5, 720., 3.565, -0.052, -1.55E6, 52.,
... 201., 1.2)
10802.536262068483
chemicals.heat_capacity.TRCCp_integral_over_T $(T, a 0, a 1, a 2, a 3, a 4, a 5, a 6, a 7, J=0)$
Integrates ideal gas heat capacity over T using the model developed in [1]. Best used as a delta only. The difference in ideal-gas entropy with respect to 0 K is given by:

$$
\frac{S^{\circ}}{R}=J+a_{0} \ln T+\frac{a_{1}}{a_{2}^{2}}\left(1+\frac{a_{2}}{T}\right) x\left(a_{2}\right)+s(T) s(T)=\left[\left\{a_{3}+\left(\frac{a_{4} a_{7}^{2}-a_{5}}{a_{6}^{2}}\right)\left(\frac{a_{7}}{a_{6}}\right)^{4}\right\}\left(\frac{a_{7}}{a_{6}}\right)^{2} \ln z+\left(a_{3}+a_{4}\right) \ln \left(\frac{T+a_{6}}{a_{6}+a}\right.\right.
$$

$$
\begin{gathered}
s(T)=0 \text { for } T \leq a_{7} \\
z=\frac{T}{T+a_{6}} \cdot \frac{a_{7}+a_{6}}{a_{7}} \\
y=\frac{T-a_{7}}{T+a_{6}} \text { for } T>a_{7} \text { otherwise } 0
\end{gathered}
$$

## Parameters

T [float] Temperature [K]
a1-a7 [float] Coefficients
J [float, optional] Integral offset

## Returns

S-S(0) [float] Difference in entropy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$

## Notes

Analytical integral as provided in [1] and verified with numerical integration.

## References

[1]

## Examples

>> TRCCp_integral_over_T(300, 4.0, 124000, 245, 50.539, -49.469,
... 220440000, 560, 78)
213.80156219151888
chemicals.heat_capacity. $\operatorname{Shomate}(T, A, B, C, D, E)$
Calculates heat capacity using the Shomate polynomial model [1]. The heat capacity is given by:

$$
C_{p}=A+B T+C T^{2}+D T^{3}+\frac{E}{T^{2}}
$$

## Parameters

$\mathbf{T}$ [float] Temperature [K]

A [float] Parameter, [J/(mol*K)]
B [float] Parameter, [J/(mol*K^2)]
C [float] Parameter, [J/(mol* $\left.{ }^{\wedge} 3\right)$ ]
D [float] Parameter, [J/(mol* $\left.{ }^{\wedge} 4\right)$ ]
E [float] Parameter, [J*K/(mol)]

## Returns

Cp [float] Heat capacity , [J/mol/K]

## Notes

Analytical integrals are available for this expression. In some sources such as [1], the equation is written with temperature in units of kilokelvin. The coefficients can be easily adjusted to be in the proper SI form.

## References

[1]

## Examples

Coefficients for water vapor from [1]:

```
>>> water_low_gas_coeffs = [30.09200, 6.832514/1e3, 6.793435/1e6, -2.534480/1e9, 0.
->082139*1e6]
>>> Shomate(500, *water_low_gas_coeffs)
35.21836175
```

chemicals.heat_capacity. Shomate_integral( $T, A, B, C, D, E$ )
Calculates the enthalpy integral using the Shomate polynomial model [1]. The difference in enthalpy with respect to 0 K is given by:

$$
H(T)-H^{0}=A T+\frac{B T^{2}}{2}+\frac{C T^{3}}{3}+\frac{D T^{4}}{4}-\frac{E}{T}
$$

## Parameters

$\mathbf{T}$ [float] Temperature [K]
A [float] Parameter, [J/(mol*K)]
B [float] Parameter, [J/(mol*K^2)]
C [float] Parameter, [J/(mol* $\left.\mathrm{K}^{\wedge} 3\right)$ ]
D [float] Parameter, [J/(mol*K^4)]
E [float] Parameter, [J*K/(mol)]

## Returns

$\mathbf{H}-\mathbf{H}(\mathbf{0})$ [float] Difference in enthalpy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol}]$

## References

[1]

## Examples

Coefficients for water vapor from [1]:

```
>>> water_low_gas_coeffs = [30.09200, 6.832514/1e3, 6.793435/1e6, -2.534480/1e9, 0.
๑082139*1e6]
>>> Shomate_integral(500, *water_low_gas_coeffs)
15979.2447
```

chemicals.heat_capacity.Shomate_integral_over_T $(T, A, B, C, D, E)$
Integrates the heat capacity over T using the model developed in [1]. The difference in entropy with respect to 0 K is given by:

$$
s(T)=A \log (T)+B T+\frac{C T^{2}}{2}+\frac{D T^{3}}{3}-\frac{E}{2 T^{2}}
$$

## Parameters

T [float] Temperature [K]
A [float] Parameter, [J/(mol*K)]
B [float] Parameter, [J/(mol* $\left.\left.\mathrm{K}^{\wedge} 2\right)\right]$
C [float] Parameter, [J/(mol*K^3)]
D [float] Parameter, [J/(mol*K^4)]
E [float] Parameter, [ $\mathrm{J} * \mathrm{~K} /(\mathrm{mol})$ ]

## Returns

S-S(0) [float] Difference in entropy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$

## References

[1]

## Examples

Coefficients for water vapor from [1]:
>>> water_low_gas_coeffs $=[30.09200,6.832514 / 1 \mathrm{e} 3,6.793435 / 1 \mathrm{e} 6,-2.534480 / 1 \mathrm{e} 9,0$. $\rightarrow 082139 * 1 \mathrm{e} 6]$
>>> Shomate_integral_over_T(500, *water_low_gas_coeffs)
191.00554
class chemicals.heat_capacity. ShomateRange (coeffs, Tmin, Tmax)
Implementation of a range of the Shomate equation presented in [1] for calculating the heat capacity of a chemical. Implements the enthalpy and entropy integrals as well.

## Parameters

coeffs [list[float]] Six coefficients for the equation, [-]

Tmin [float] Minimum temperature any experimental data was available at, [K]
Tmax [float] Maximum temperature any experimental data was available at, [K]

## References

[1]

Methods

| calculate(T) | Return heat capacity as a function of temperature. |
| :--- | :--- |
| calculate_integral(Ta, Tb) | Return the enthalpy integral of heat capacity from $T a$ <br> to $T b$. |
| calculate_integral_over_T(Ta, Tb$)$ | Return the entropy integral of heat capacity from $T a$ <br> to $T b$. |

## calculate ( $T$ )

Return heat capacity as a function of temperature.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]

## Returns

Cp [float] Liquid heat capacity as $\mathrm{T},[\mathrm{J} / \mathrm{mol} / \mathrm{K}$ ]
calculate_integral ( $T a, T b$ )
Return the enthalpy integral of heat capacity from $T a$ to $T b$.

## Parameters

Ta [float] Initial temperature, [K]
Tb [float] Final temperature, [K]

## Returns

dH [float] Enthalpy difference between $T a$ and $T b,[\mathrm{~J} / \mathrm{mol}]$
calculate_integral_over_T ( $T a, T b$ )
Return the entropy integral of heat capacity from $T a$ to $T b$.

## Parameters

Ta [float] Initial temperature, [K]
Tb [float] Final temperature, [K]

## Returns

dS [float] Entropy difference between $T a$ and $T b,[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$
chemicals.heat_capacity. Poling ( $T, a, b, c, d, e$ )
Return the ideal-gas molar heat capacity of a chemical using polynomial regressed coefficients as described by Poling et. al. [1].

## Parameters

T [float] Temperature, [K]
a,b,c,d,e [float] Regressed coefficients.

## Returns

Cpgm [float] Gas molar heat capacity, [J/mol/K]

## See also:

Poling_integral
Poling_integral_over_T

## Notes

The ideal gas heat capacity is given by:

$$
C_{n}=R *\left(a+b T+c T^{2}+d T^{3}+e T^{4}\right)
$$

The data is based on the Poling data bank.

## References

[1]

## Examples

Compute the gas heat capacity of Methane at 300 K :
>> Poling(T=300., $\mathrm{a}=4.568$, $\mathrm{b}=-0.008975, \mathrm{c}=3.631 \mathrm{e}-05, \mathrm{~d}=-3.407 \mathrm{e}-08$, $\mathrm{e}=1.091 \mathrm{e}-11)$
35.850973388425
chemicals.heat_capacity.Poling_integral ( $T, a, b, c, d, e$ )
Return the integral of the ideal-gas constant-pressure heat capacity of a chemical using polynomial regressed coefficients as described by Poling et. al. [1].

## Parameters

$\mathbf{T}$ [float] Temperature, [K]
a,b,c,d,e [float] Regressed coefficients.

## Returns

H [float] Difference in enthalpy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol}]$
See also:
Poling
Poling_integral_over_T

## Notes

Integral was computed with SymPy.

## References

[1]

## Examples

Compute the gas enthalpy of Methane at 300 K (with reference to 0 K ):
>>> Poling_integral(T=300., $a=4.568$, $b=-0.008975, \mathrm{c}=3.631 \mathrm{e}-05, \mathrm{~d}=-3.407 \mathrm{e}-08$, $\mathrm{e}=1$. $\rightarrow$ 091e-11)
10223.67533722261
chemicals.heat_capacity.Poling_integral_over_T(T, $a, b, c, d, e)$
Return the integral over temperature of the ideal-gas constant-pressure heat capacity of a chemical using polynomial regressed coefficients as described by Poling et. al. [1].

## Parameters

$\mathbf{T}$ [float] Temperature, [K]
$\mathbf{a , b , c , d , e}$ [float] Regressed coefficients.

## Returns

$\mathbf{S}$ [float] Difference in entropy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$
See also:
Poling
Poling_integral

## Notes

Integral was computed with SymPy.

## References

[1]

## Examples

Compute the gas entropy of Methane at 300 K (with reference to 0 K ):

```
>>> Poling_integral_over_T(T=300., a=4.568, b=-0.008975, c=3.631e-05, d=-3.407e-08,生
@=1.091e-11)
205.46526328058
```

chemicals.heat_capacity.PPDS2 ( $T, T s, C_{-}$low, $C_{-} i n f, a 1, a 2, a 3, a 4, a 5$ )
Calculates the ideal-gas heat capacity using the [1] emperical (parameter-regressed) method, called the PPDS 2 equation for heat capacity.

$$
\begin{gathered}
\frac{C_{p}^{0}}{R}=C_{l o w}+\left(C_{\left.\mathrm{inf}-C_{l o w}\right) y^{2}\left(1+(y-1)\left[\sum_{i=0}^{4} a_{i} y^{i}\right]\right)}\right. \\
y=\frac{T}{T+T_{s}}
\end{gathered}
$$

## Parameters

$\mathbf{T}$ [float] Temperature of fluid [K]
Ts [float] Fit temperature; no physical meaning [K]
C_low [float] Fit parameter equal to $\mathrm{Cp} / \mathrm{R}$ at a low temperature, [-]
C_inf [float] Fit parameter equal to $\mathrm{Cp} / \mathrm{R}$ at a high temperature, [-]
a1 [float] Regression parameter, [-]
a2 [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]
a5 [float] Regression parameter, [-]

## Returns

Cpgm [float] Gas molar heat capacity, $[\mathrm{J} / \mathrm{mol} / \mathrm{K}$ ]

## References

[1]

## Examples

n-pentane at 350 K from [1]
>>> PPDS2 (T=350.0, Ts=462.493, C_low=4.54115, C_inf=9.96847, a1=-103.419, a2=695.
$\rightarrow 484, \mathrm{a} 3=-2006.1, \mathrm{a} 4=2476.84, \mathrm{a} 5=-1186.47$ )
136.46338956689

### 1.12.2 Gas Heat Capacity Estimation Models

chemicals.heat_capacity.Lastovka_Shaw(T, similarity_variable, cyclic_aliphatic=False, $M W=$ None, term_A=None)
Calculate ideal-gas constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

$$
\begin{gathered}
\operatorname{term}_{A}=A 1+A 2 * a \text { if cyclic aliphatic } \\
\operatorname{term}_{A}=\left(A_{2}+\frac{A_{1}-A_{2}}{1+\exp \left(\frac{\alpha-A_{3}}{A_{4}}\right)}\right) \text { if not cyclic aliphatic } \\
C_{p}^{0}=\operatorname{term}_{A}+\left(B_{11}+B_{12} \alpha\right)\left(-\frac{\left(C_{11}+C_{12} \alpha\right)}{T}\right)^{2} \frac{\exp \left(-\left(C_{11}+C_{12} \alpha\right) / T\right)}{\left[1-\exp \left(-\left(C_{11}+C_{12} \alpha\right) / T\right)\right]^{2}}+\left(B_{21}+B_{22} \alpha\right)\left(-\frac{\left(C_{21}+C_{22} \alpha\right)}{T}\right)^{2} \frac{}{[1}
\end{gathered}
$$

## Parameters

$\mathbf{T}$ [float] Temperature of gas [K]
similarity_variable [float] Similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
cyclic_aliphatic: bool, optional Whether or not chemical is cyclic aliphatic, [-]
MW [float, optional] Molecular weight, [g/mol]
term_A [float, optional] Term A in Lastovka-Shaw equation, [J/g]

## Returns

Cpg [float] Gas constant-pressure heat capacity, J/mol/K if MW given; J/kg/K otherwise

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$.
A1 $=-0.1793547$ text $\{$ if cyclic aliphatic $\}$
$\mathrm{A} 1=0.58$ text $\{$ if not cyclic aliphatic $\}$
A2 $=3.86944439$ text $\{$ if cyclic aliphatic $\}$
$\mathrm{A} 2=1.25$ text $\{$ if not cyclic aliphatic $\}$
$\mathrm{A} 3=0.17338003$
$\mathrm{A} 4=0.014$
$\mathrm{B} 11=0.73917383$
$\mathrm{B} 12=8.88308889$
C11 $=1188.28051$
$\mathrm{C} 12=1813.04613$
$\mathrm{B} 21=0.0483019$
$B 22=4.35656721$
$\mathrm{C} 21=2897.01927$
$\mathrm{C} 22=5987.80407$

## References

[1]

## Examples

Estimate the heat capacity of n -decane gas in $\mathrm{J} / \mathrm{kg} / \mathrm{K}$ :
>>> Lastovka_Shaw(1000.0, 0.22491)
3730.2807601773725

Estimate the heat capacity of n -decane gas in $\mathrm{J} / \mathrm{mol} / \mathrm{K}$ :
>>> Lastovka_Shaw(1000.0, 0.22491, MW=142.28)
530.7443465580366
chemicals.heat_capacity.Lastovka_Shaw_integral( $T$, similarity_variable, cyclic_aliphatic=False, $M W=$ None, term_A=None)
Calculate the integral of ideal-gas constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

## Parameters

$\mathbf{T}$ [float] Temperature of gas [K]
cyclic_aliphatic: bool, optional Whether or not chemical is cyclic aliphatic, [-]
MW [float, optional] Molecular weight, [ $\mathrm{g} / \mathrm{mol}$ ]
term_A [float, optional] Term A in Lastovka-Shaw equation, [J/g]

## Returns

$\mathbf{H}$ [float] Difference in enthalpy from $0 \mathrm{~K}, \mathrm{~J} / \mathrm{mol}$ if MW given; J/kg otherwise
See also:

Lastovka_Shaw
Lastovka_Shaw_integral_over_T

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Integral was computed with SymPy.

## References

[1]

## Examples

```
>>> Lastovka_Shaw_integral(300.0, 0.1333)
5283095.816018478
```

chemicals.heat_capacity.Lastovka_Shaw_integral_over_T(T, similarity_variable, cyclic_aliphatic=False, $M W=$ None, term_A=None)
Calculate the integral over temperature of ideal-gas constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

## Parameters

$\mathbf{T}$ [float] Temperature of gas [K]
similarity_variable [float] Similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
cyclic_aliphatic: bool, optional Whether or not chemical is cyclic aliphatic, [-]
MW [float, optional] Molecular weight, $[\mathrm{g} / \mathrm{mol}]$
term_A [float, optional] Term A in Lastovka-Shaw equation, [J/g]

## Returns

$\mathbf{S}$ [float] Difference in entropy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol} / \mathrm{K}$ if MW given; $\mathrm{J} / \mathrm{kg} / \mathrm{K}$ otherwise]
See also:
Lastovka_Shaw
Lastovka_Shaw_integral

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model is for predicting mass heat capacity, not molar heat capacity like most other methods! Integral was computed with SymPy.

## References

[1]

## Examples

>>> Lastovka_Shaw_integral_over_T(300.0, 0.1333)
3609.791928945323
chemicals.heat_capacity.Lastovka_Shaw_T_for_Hm(Hm, MW, similarity_variable, T_ref=298.15, factor $=1.0$, cyclic_aliphatic $=$ None, term_A $=$ None)
Uses the Lastovka-Shaw ideal-gas heat capacity correlation to solve for the temperature which has a specified Hm , as is required in PH flashes, as shown in [1].

## Parameters

Hm [float] Molar enthalpy spec, [J/mol]
MW [float] Molecular weight of the pure compound or mixture average, [ $\mathrm{g} / \mathrm{mol}$ ]
similarity_variable [float] Similarity variable as defined in [1], [mol/g]
T_ref [float, optional] Reference enthlapy temperature, [K]
factor [float, optional] A factor to increase or decrease the predicted value of the method, [-]
cyclic_aliphatic: bool, optional Whether or not chemical is cyclic aliphatic, [-]
term_A [float, optional] Term A in Lastovka-Shaw equation, [J/g]

## Returns

$\mathbf{T}$ [float] Temperature of gas to meet the molar enthalpy spec, [K]

## See also:

Lastovka_Shaw
Lastovka_Shaw_integral
Lastovka_Shaw_integral_over_T

## References

[1]

## Examples

>>> Lastovka_Shaw_T_for_Hm(Hm=55000, MW=80.0, similarity_variable=0.23)
600.0943429567602
chemicals.heat_capacity.Lastovka_Shaw_T_for_Sm(Sm, MW, similarity_variable, $T_{-} r e f=298.15$, factor $=1.0$, cyclic_aliphatic $=$ None, term_A=None)
Uses the Lastovka-Shaw ideal-gas heat capacity correlation to solve for the temperature which has a specified $S m$, as is required in PS flashes, as shown in [1].

## Parameters

Sm [float] Molar entropy spec, [J/mol/K]
MW [float] Molecular weight of the pure compound or mixture average, $[\mathrm{g} / \mathrm{mol}$ ]
similarity_variable [float] Similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
T_ref [float, optional] Reference enthlapy temperature, [K]
factor [float, optional] A factor to increase or decrease the predicted value of the method, [-]
cyclic_aliphatic: bool, optional Whether or not chemical is cyclic aliphatic, [-]
term_A [float, optional] Term A in Lastovka-Shaw equation, [J/g]

## Returns

$\mathbf{T}$ [float] Temperature of gas to meet the molar entropy spec, [K]
See also:

```
Lastovka_Shaw
Lastovka_Shaw_integral
Lastovka_Shaw_integral_over_T
```


## References

[1]

## Examples

>>> Lastovka_Shaw_T_for_Sm(Sm=112.80, MW=72.151, similarity_variable=0.2356) 603.4298291570276
chemicals.heat_capacity.Lastovka_Shaw_term_A (similarity_variable, cyclic_aliphatic)
Return Term A in Lastovka-Shaw equation.

## Parameters

similarity_variable [float] Similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
cyclic_aliphatic: bool, optional Whether or not chemical is cyclic aliphatic, [-]

## Returns

term_A [float] Term A in Lastovka-Shaw equation, [J/g]

## See also:

```
Lastovka_Shaw
Lastovka_Shaw_integral
Lastovka_Shaw_integral_over_T
```


## References

[1]

### 1.12.3 Gas Heat Capacity Theory

chemicals.heat_capacity.Cpg_statistical_mechanics(T, thetas, linear=False)
Calculates the ideal-gas heat capacity using of a molecule using its characteristic temperatures, themselves calculated from each of the frequencies of vibration of the molecule. These can be obtained from spectra or quantum mechanical calculations.

$$
\begin{gathered}
\frac{C_{p}^{0}}{R}=\frac{C_{p}^{0}}{R} \text { rotational }+\frac{C_{p}^{0}}{R} \text { translational }+\frac{C_{p}^{0}}{R} \text { vibrational } \\
\qquad \frac{C_{p}^{0}}{R} \text { rotational }=2.5 \\
\frac{C_{p}^{0}}{R} \text { translational }=1 \text { if linear else } 1.5 \\
\frac{C_{p}^{0}}{R} \text { vibrational }=\sum_{i=1}^{3 n_{A}-6+\delta}\left(\frac{\theta_{i}}{T}\right)^{2}\left[\frac{\exp \left(\theta_{i} / T\right)}{\left(\exp \left(\theta_{i} / T\right)-1\right)^{2}}\right]
\end{gathered}
$$

In the above equation, delta is 1 if the molecule is linear otherwise 0 .

## Parameters

$\mathbf{T}$ [float] Temperature of fluid [K]
thetas [list[float]] Characteristic temperatures, [K]

## Returns

Cpgm [float] Gas molar heat capacity at specified temperature, $[\mathrm{J} / \mathrm{mol} / \mathrm{K}]$

## Notes

This equation implies that there is a maximum heat capacity for an ideal gas, and all diatomic or larger gases Monoatomic gases have a simple heat capacity of 2.5 R , the lower limit for ideal gas heat capacity. This function does not cover that type of a gas. At very low temperatures hydrogen behaves like a monoatomic gas as well.

## References

[1]

## Examples

Sample calculation in [1] for ammonia:

```
>>> thetas = [1360, 2330, 2330, 4800, 4880, 4880]
>>> Cpg_statistical_mechanics(300.0, thetas)
35.55983440173097
```

chemicals.heat_capacity.Cpg_statistical_mechanics_integral( $T$, thetas, linear=False)
Calculates the integral of ideal-gas heat capacity using of a molecule using its characteristic temperatures.

$$
\begin{gathered}
\int C_{p}^{0}=2.5 R T+R T \text { if linear else } 1.5 R T+\int C_{p}^{0} \text { vibrational } \\
\int C_{p}^{0} \text { vibrational }=R \sum_{i=1}^{3 n_{A}-6+\delta} \frac{\theta_{i}}{\exp \left(\theta_{i} / T\right)-1}
\end{gathered}
$$

## Parameters

T [float] Temperature of fluid [K]
thetas [list[float]] Characteristic temperatures, [K]

## Returns

H [float] Integrated gas molar heat capacity at specified temperature, [J/mol]

## Examples

```
>>> thetas = [1360, 2330, 2330, 4800, 4880, 4880]
>>> Cpg_statistical_mechanics_integral(300.0, thetas)
10116.6053294
```

chemicals.heat_capacity.Cpg_statistical_mechanics_integral_over_T( $T$, thetas, linear=False)
Calculates the integral over $\mathbf{T}$ of ideal-gas heat capacity using of a molecule using its characteristic temperatures.

$$
\begin{aligned}
& \int \frac{C_{p}^{0}}{T}=2.5 R \log (T)+1 R \log (T) \text { if linear else } 1.5 R \log (T)+\int \frac{C_{p}^{0}}{T} \text { vibrational } \\
& \int \frac{C_{p}^{0}}{T} \text { vibrational }=\sum_{i=1}^{3 n_{A}-6+\delta} \frac{\theta_{i}}{T \exp \left(\theta_{i} / T\right)-T}-\log \left(\exp \left(\theta_{i} / T\right)-1\right)+\theta_{i} / T
\end{aligned}
$$

## Parameters

T [float] Temperature of fluid [K]
thetas [list[float]] Characteristic temperatures, [K]

## Returns

$\mathbf{S}$ [float] Entropy integral of gas molar heat capacity at specified temperature, [ $\mathrm{J} / \mathrm{mol} / \mathrm{K}$ ]

## Examples

>>> thetas $=[1360,2330,2330,4800,4880,4880]$
>>> Cpg_statistical_mechanics_integral_over_T(300.0, thetas)
190. 25658088

## chemicals.heat_capacity.vibration_frequency_cm_to_characteristic_temperature(frequency,

 scale=1)Convert a vibrational frequency in units of $1 / \mathrm{cm}$ to a characteristic temperature for use in calculating heat capacity.

$$
\theta=\frac{100 \cdot h \cdot c \cdot \text { scale }}{k}
$$

## Parameters

frequency [float] Vibrational frequency, [1/cm]
scale [float] A scale factor used to adjust the frequency for differences in experimental vs. calculated values, [-]

## Returns

theta [float] Characteristic temperature [K]

## Notes

In the equation, $k$ is Boltzmann's constant, $c$ is the speed of light, and $h$ is the Planck constant.
A scale factor for the MP2/6-31G** method recommended by NIST is 0.9365 . Using this scale factor will not improve results in all cases however.

## Examples

>>> vibration_frequency_cm_to_characteristic_temperature(667)
959.6641613636505

### 1.12.4 Liquid Heat Capacity Model Equations

chemicals.heat_capacity.Zabransky_quasi_polynomial ( $T, T c, a 1, a 2, a 3, a 4, a 5, a 6$ )
Calculates liquid heat capacity using the model developed in [1].

$$
\frac{C}{R}=A_{1} \ln \left(1-T_{r}\right)+\frac{A_{2}}{1-T_{r}}+\sum_{j=0}^{m} A_{j+3} T_{r}^{j}
$$

## Parameters

$\mathbf{T}$ [float] Temperature [K]
Te [float] Critical temperature of fluid, [K]
a1-a6 [float] Coefficients

## Returns

Cp [float] Liquid heat capacity, [J/mol/K]

## Notes

Used only for isobaric heat capacities, not saturation heat capacities. Designed for reasonable extrapolation behavior caused by using the reduced critical temperature. Used by the authors of [1] when critical temperature was available for the fluid. Analytical integrals are available for this expression.

## References

[1]

## Examples

>>> Zabransky_quasi_polynomial(330, 591.79, -3.12743, 0.0857315, 13.7282, 1.28971,七
$\rightarrow 6.42297,4.10989)$
165.472878778683
chemicals.heat_capacity.Zabransky_quasi_polynomial_integral( $T, T c, a 1, a 2, a 3, a 4, a 5, a 6$ )
Calculates the integral of liquid heat capacity using the quasi-polynomial model developed in [1].

## Parameters

T [float] Temperature [K]
a1-a6 [float] Coefficients

## Returns

H [float] Difference in enthalpy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol}]$

## Notes

The analytical integral was derived with SymPy; it is a simple polynomial plus some logarithms.

## References

[1]

## Examples

```
>>> H2 = Zabransky_quasi_polynomial_integral(300, 591.79, -3.12743,
... 0.0857315, 13.7282, 1.28971, 6.42297, 4.10989)
>>> H1 = Zabransky_quasi_polynomial_integral(200, 591.79, -3.12743,
...0.0857315, 13.7282, 1.28971, 6.42297, 4.10989)
>>> H2 - H1
14662.031376528757
```

chemicals.heat_capacity.Zabransky_quasi_polynomial_integral_over_T $(T, T c, a 1, a 2, a 3, a 4, a 5, a 6)$
Calculates the integral of liquid heat capacity over T using the quasi-polynomial model developed in [1].

## Parameters

T [float] Temperature [K]
a1-a6 [float] Coefficients

## Returns

$\mathbf{S}$ [float] Difference in entropy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$

## Notes

The analytical integral was derived with Sympy. It requires the Polylog(2,x) function, which is unimplemented in SciPy. A very accurate numerical approximation was implemented as fluids.numerics.polylog2. Relatively slow due to the use of that special function.

## References

[1]

## Examples

>>> S2 = Zabransky_quasi_polynomial_integral_over_T(300, 591.79, -3.12743,
... 0.0857315, 13.7282, 1.28971, 6.42297, 4.10989)
>>> S1 = Zabransky_quasi_polynomial_integral_over_T(200, 591.79, -3.12743,
$\because$.. 0.0857315, 13.7282, 1.28971, 6.42297, 4.10989)
>> S2 - S1
59.16999297436473
chemicals.heat_capacity.Zabransky_cubic (T, al, a2, a3, a4)
Calculates liquid heat capacity using the model developed in [1].

$$
\frac{C}{R}=\sum_{j=0}^{3} A_{j+1}\left(\frac{T}{100 \mathrm{~K}}\right)^{j}
$$

## Parameters

T [float] Temperature [K]
a1 [float] Coefficient, [-]
a2 [float] Coefficient, [-]
a3 [float] Coefficient, [-]
a4 [float] Coefficient, [-]

## Returns

Cp [float] Liquid heat capacity, [J/mol/K]

## Notes

Most often form used in [1]. Analytical integrals are available for this expression.

## References

[1]

## Examples

>>> Zabransky_cubic(298.15, 20.9634, -10.1344, 2.8253, -0.256738)
75.31465144297
chemicals.heat_capacity.Zabransky_cubic_integral( $T, a 1, a 2, a 3, a 4$ )
Calculates the integral of liquid heat capacity using the model developed in [1].

## Parameters

T [float] Temperature [K]
a1 [float] Coefficient, [-]
a2 [float] Coefficient, [-]
a3 [float] Coefficient, [-]
a4 [float] Coefficient, [-]

## Returns

H [float] Difference in enthalpy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol}]$

## Notes

The analytical integral was derived with Sympy; it is a simple polynomial.

## References

[1]

## Examples

>>> Zabransky_cubic_integral(298.15, 20.9634, -10.1344, 2.8253, -0.256738)
31051.690370364
chemicals.heat_capacity.Zabransky_cubic_integral_over_T (T, al, a2, a3, a4)
Calculates the integral of liquid heat capacity over T using the model developed in [1].

## Parameters

T [float] Temperature [K]
a1 [float] Coefficient, [-]
a2 [float] Coefficient, [-]
a3 [float] Coefficient, [-]
a4 [float] Coefficient, [-]

## Returns

S [float] Difference in entropy from $0 \mathrm{~K},[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$

## Notes

The analytical integral was derived with Sympy; it is a simple polynomial, plus a logarithm

## References

[1]

## Examples

>>> Zabransky_cubic_integral_over_T(298.15, 20.9634, -10.1344, 2.8253,
‥ -0.256738)
24.732465342840
class chemicals.heat_capacity.ZabranskySpline(coeffs, Tmin, Tmax)
Implementation of the cubic spline method presented in [1] for calculating the heat capacity of a chemical. Implements the enthalpy and entropy integrals as well.

$$
\frac{C}{R}=\sum_{j=0}^{3} A_{j+1}\left(\frac{T}{100}\right)^{j}
$$

## Parameters

coeffs [list[float]] Six coefficients for the equation, [-]
Tmin [float] Minimum temperature any experimental data was available at, [K]
Tmax [float] Maximum temperature any experimental data was available at, [K]

## References

[1]

## Methods

| calculate $(\mathrm{T})$ | Return heat capacity as a function of temperature. |
| :--- | :--- |
| calculate_integral $(\mathrm{Ta}, \mathrm{Tb})$ | Return the enthalpy integral of heat capacity from $T a$ <br> to $T b$. |
| calculate_integral_over_T(Ta, Tb$)$ | Return the entropy integral of heat capacity from $T a$ <br> to $T b$. |

## calculate $(T)$

Return heat capacity as a function of temperature.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]

## Returns

Cp [float] Liquid heat capacity as T, [J/mol/K]
calculate_integral ( $T a, T b$ )
Return the enthalpy integral of heat capacity from $T a$ to $T b$.

## Parameters

Ta [float] Initial temperature, $[\mathrm{K}]$
Tb [float] Final temperature, [K]

## Returns

dH [float] Enthalpy difference between $T a$ and $T b,[J / m o l]$
calculate_integral_over_T ( $T a, T b$ )
Return the entropy integral of heat capacity from $T a$ to $T b$.

## Parameters

Ta [float] Initial temperature, [K]
Tb [float] Final temperature, [K]

## Returns

dS [float] Entropy difference between Ta and Tb , [J/mol/K]
class chemicals.heat_capacity.ZabranskyQuasipolynomial(coeffs, Tc, Tmin, Tmax)
Quasi-polynomial object for calculating the heat capacity of a chemical. Implements the enthalpy and entropy integrals as well.

$$
\frac{C}{R}=A_{1} \ln \left(1-T_{r}\right)+\frac{A_{2}}{1-T_{r}}+\sum_{j=0}^{m} A_{j+3} T_{r}^{j}
$$

## Parameters

coeffs [list[float]] Six coefficients for the equation, [-]
Tc [float] Critical temperature of the chemical, as used in the formula, [K]
Tmin [float] Minimum temperature any experimental data was available at, [K]
Tmax [float] Maximum temperature any experimental data was available at, [K]

## References

[1]

## Methods

| calculate $(\mathbf{T})$ | Return the heat capacity as a function of temperature. |
| :--- | :--- |
| calculate_integral(Ta, Tb$)$ | Return the enthalpy integral of heat capacity from $T a$ <br> to $T b$. |
| calculate_integral_over_T(Ta, Tb$)$ | Return the entropy integral of heat capacity from $T a$ <br> to $T b$. |

## calculate ( $T$ )

Return the heat capacity as a function of temperature.

## Parameters

T [float] Temperature, [K]

## Returns

Cp [float] Liquid heat capacity as T, [J/mol/K]
calculate_integral ( $T a, T b$ )
Return the enthalpy integral of heat capacity from $T a$ to $T b$.

## Parameters

Ta [float] Initial temperature, [K]
Tb [float] Final temperature, [K]

## Returns

$\mathbf{d H}$ [float] Enthalpy difference between $T a$ and $T b,[\mathrm{~J} / \mathrm{mol}]$
calculate_integral_over_T ( $T a, T b$ )
Return the entropy integral of heat capacity from $T a$ to $T b$.

## Parameters

Ta [float] Initial temperature, [K]
Tb [float] Final temperature, [K]

## Returns

dS [float] Entropy difference between $T a$ and $T b,[\mathrm{~J} / \mathrm{mol} / \mathrm{K}]$
chemicals.heat_capacity.PPDS15 (T, Tc, a0, al, a2, a3, a4, a5)
Calculates the saturation liquid heat capacity using the [1] emperical (parameter-regressed) method, called the PPDS 15 equation for heat capacity.

$$
\frac{C_{p, l}}{R}=\frac{a_{0}}{\tau}+a_{1}+a_{2} \tau+a_{3} \tau^{2}+a_{4} \tau^{3}+a_{5} \tau^{4}
$$

## Parameters

$\mathbf{T}$ [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
a0 [float] Regression parameter, [-]
a1 [float] Regression parameter, [-]
$\mathbf{a} 2$ [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]
a5 [float] Regression parameter, [-]

## Returns

Cplm [float] Liquid molar saturation heat capacity, [J/mol/K]

## References

[1]

## Examples

Benzene at 400 K from [1]
$\gg$ PPDS15 (T=400.0, Tc=562.05, $\mathrm{a} 0=0.198892, \mathrm{a} 1=24.1389, \mathrm{a} 2=-20.2301, \mathrm{a}=5.72481$, -
$\hookrightarrow \mathrm{a} 4=4.43613 \mathrm{e}-7, \mathrm{a} 5=-3.10751 \mathrm{e}-7$ )
161.8983143509
chemicals.heat_capacity.TDE_CSExpansion $(T, T c, b, a 1, a 2=0.0, a 3=0.0, a 4=0.0$ )
Calculates the saturation liquid heat capacity using the [1] CSExpansion method from NIST's TDE:

$$
C_{p, l}=\frac{b}{\tau}+a_{1}+a_{2} T+a_{3} T^{2}+a_{4} T^{3}
$$

## Parameters

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
b [float] Regression parameter, [-]
a1 [float] Regression parameter, [-]
a2 [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]

## Returns

Cplm [float] Liquid molar saturation heat capacity, [J/mol/K]

## References

[1]

## Examples

2-methylquinoline at 550 K from [1]

```
>>> TDE_CSExpansion(550.0, 778.0, 0.626549, 120.705, 0.255987, 0.000381027, -3.
403077e-7)
328.472042686
```


### 1.12.5 Liquid Heat Capacity Estimation Models

## chemicals.heat_capacity.Rowlinson_Poling(T, Tc, omega, Cpgm)

Calculate liquid constant-pressure heat capacity with the [1] CSP method. This equation is not terrible accurate.
The heat capacity of a liquid is given by:

$$
\frac{C p^{L}-C p^{g}}{R}=1.586+\frac{0.49}{1-T_{r}}+\omega\left[4.2775+\frac{6.3\left(1-T_{r}\right)^{1 / 3}}{T_{r}}+\frac{0.4355}{1-T_{r}}\right]
$$

## Parameters

$\mathbf{T}$ [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor for fluid, [-]
Cpgm [float] Constant-pressure gas heat capacity, [J/mol/K]

## Returns

Cplm [float] Liquid constant-pressure heat capacity, [J/mol/K]

## Notes

Poling compared 212 substances, and found error at 298 K larger than $10 \%$ for 18 of them, mostly associating. Of the other 194 compounds, AARD is $2.5 \%$.

## References

[1]

## Examples

>>> Rowlinson_Poling(350.0, 435.5, 0.203, 91.21)
143.80196224081436
chemicals.heat_capacity.Rowlinson_Bondi(T, Tc, omega, Cpgm)
Calculate liquid constant-pressure heat capacity with the CSP method shown in [1].
The heat capacity of a liquid is given by:

$$
\frac{C p^{L}-C p^{i g}}{R}=1.45+0.45\left(1-T_{r}\right)^{-1}+0.25 \omega\left[17.11+25.2\left(1-T_{r}\right)^{1 / 3} T_{r}^{-1}+1.742\left(1-T_{r}\right)^{-1}\right]
$$

## Parameters

$\mathbf{T}$ [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor for fluid, [-]
Cpgm [float] Constant-pressure gas heat capacity, [J/mol/K]

## Returns

Cplm [float] Liquid constant-pressure heat capacity, [J/mol/K]

## Notes

Less accurate than Rowlinson_Poling.

## References

[1], [2], [3]

## Examples

>>> Rowlinson_Bondi( $\mathrm{T}=373.28$, $\mathrm{Tc}=535.55$, omega=0.323, Cpgm=119.342)
175.3976263003074
chemicals.heat_capacity.Dadgostar_Shaw (T, similarity_variable, $M W=$ None, terms=None)
Calculate liquid constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

$$
C_{p}=24.5\left(a_{11} \alpha+a_{12} \alpha^{2}\right)+\left(a_{21} \alpha+a_{22} \alpha^{2}\right) T+\left(a_{31} \alpha+a_{32} \alpha^{2}\right) T^{2}
$$

## Parameters

T [float] Temperature of liquid [K]
similarity_variable [float] similarity variable as defined in [1], [mol/g]
MW [float, optional] Molecular weight of the pure compound or mixture average, $[\mathrm{g} / \mathrm{mol}]$
terms [float, optional] Terms in Dadgostar-Shaw equation as computed by Dadgostar_Shaw_terms

## Returns

Cpl [float] Liquid constant-pressure heat capacity, J/mol/K if MW given; $\mathrm{J} / \mathrm{kg} / \mathrm{K}$ otherwise

## Notes

Many restrictions on its use. Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model is for predicting mass heat capacity, not molar heat capacity like most other methods! a11 $=-0.3416 ; \mathrm{a} 12=2.2671 ; \mathrm{a} 21=0.1064 ; \mathrm{a} 22=$ $-0.38741 ; \mathrm{a} 31=-9.8231 \mathrm{E}-05 ; \mathrm{a} 32=4.182 \mathrm{E}-04$

## References

[1]

## Examples

```
>>> Dadgostar_Shaw(355.6, 0.139)
```

1802.5291501191516
chemicals.heat_capacity.Dadgostar_Shaw_integral ( $T$, similarity_variable, $M W=$ None, terms=None)
Calculate the integral of liquid constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

## Parameters

$\mathbf{T}$ [float] Temperature of gas [K]
similarity_variable [float] similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
MW [float, optional] Molecular weight of the pure compound or mixture average, [ $\mathrm{g} / \mathrm{mol}$ ]
terms [float, optional] Terms in Dadgostar-Shaw equation as computed by Dadgostar_Shaw_terms

## Returns

H [float] Difference in enthalpy from $0 \mathrm{~K}, \mathrm{~J} / \mathrm{mol}$ if MW given; J/kg otherwise
See also:
Dadgostar_Shaw
Dadgostar_Shaw_integral_over_T

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model is for predicting mass heat capacity, not molar heat capacity like most other methods! Integral was computed with SymPy.

## References

[1]

## Examples

>>> Dadgostar_Shaw_integral(300.0, 0.1333)
238908.15142664989

## chemicals.heat_capacity.Dadgostar_Shaw_integral_over_T (T, similarity_variable, $M W=$ None, terms $=$ None)

Calculate the integral of liquid constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

## Parameters

T [float] Temperature of gas [K]
similarity_variable [float] similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
MW [float, optional] Molecular weight of the pure compound or mixture average, $[\mathrm{g} / \mathrm{mol}]$
terms [float, optional] Terms in Dadgostar-Shaw equation as computed by Dadgostar_Shaw_terms

## Returns

$\mathbf{S}$ [float] Difference in entropy from $0 \mathrm{~K}, \mathrm{~J} / \mathrm{mol} / \mathrm{K}$ if MW given; $\mathrm{J} / \mathrm{kg} / \mathrm{K}$ otherwise

## See also:

Dadgostar_Shaw
Dadgostar_Shaw_integral

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model is for predicting mass heat capacity, not molar heat capacity like most other methods! Integral was computed with SymPy.

## References

[1]

## Examples

>>> Dadgostar_Shaw_integral_over_T(300.0, 0.1333)
1201.1409113147918

## chemicals.heat_capacity.Dadgostar_Shaw_terms(similarity_variable)

Return terms for the computation of Dadgostar-Shaw heat capacity equation.

## Parameters

similarity_variable [float] Similarity variable, [ $\mathrm{mol} / \mathrm{g}$ ]

## Returns

first [float] First term, [-]
second [float] Second term, [-]
third [float] Third term, [-]
See also:
Dadgostar_Shaw

### 1.12.6 Solid Heat Capacity Estimation Models

chemicals.heat_capacity.Perry_151( $T, a, b, c, d$ )
Return the solid molar heat capacity of a chemical using the Perry 151 method, as described in [1].

## Parameters

$\mathbf{a , b , c , d}$ [float] Regressed coefficients.

## Returns

Cps [float] Solid constant-pressure heat capacity, [J/mol/K]

## Notes

The solid heat capacity is given by:

$$
C_{n}=4.184\left(a+b T+\frac{c}{T^{2}}+d T^{2}\right)
$$

Coefficients are listed in section 2, table 151 of [1]. Note that the original model was in a Calorie basis, but has been translated to Joules.

## References

[1]

## Examples

Heat capacity of solid aluminum at 300 K :

```
>>> Perry_151(300, 4.8, 0.00322, 0., 0.)
```

24.124944

## chemicals.heat_capacity.Lastovka_solid(T, similarity_variable, $M W=$ None)

Calculate solid constant-pressure heat capacity with the similarity variable concept and method as shown in [1].

$$
C_{p}=3\left(A_{1} \alpha+A_{2} \alpha^{2}\right) R\left(\frac{\theta}{T}\right)^{2} \frac{\exp (\theta / T)}{[\exp (\theta / T)-1]^{2}}+\left(C_{1} \alpha+C_{2} \alpha^{2}\right) T+\left(D_{1} \alpha+D_{2} \alpha^{2}\right) T^{2}
$$

## Parameters

$\mathbf{T}$ [float] Temperature of solid [K]
similarity_variable [float] similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
MW [float, optional] Molecular weight of the pure compound or mixture average, [g/mol]

## Returns

Cps [float] Solid constant-pressure heat capacity, J/mol/K if MW given; J/kg/K otherwise

## Notes

Many restrictions on its use. Trained on data with MW from $12.24 \mathrm{~g} / \mathrm{mol}$ to $402.4 \mathrm{~g} / \mathrm{mol}, \mathrm{C}$ mass fractions from $61.3 \%$ to $95.2 \%$, H mass fractions from $3.73 \%$ to $15.2 \%$, N mass fractions from 0 to $15.4 \%$, O mass fractions from 0 to $18.8 \%$, and $S$ mass fractions from 0 to $29.6 \%$. Recommended for organic compounds with low mass fractions of hetero-atoms and especially when molar mass exceeds $200 \mathrm{~g} / \mathrm{mol}$. This model does not show and effects of phase transition but should not be used passed the triple point. Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model s for predicting mass heat capacity, not molar heat capacity like most other methods!
$\mathrm{A} 1=0.013183$
$\mathrm{A} 2=0.249381$
$\theta=151.8675$
$\mathrm{C} 1=0.026526$
$\mathrm{C} 2=-0.024942$
D1 $=0.000025$
D2 $=-0.000123$

## References

[1]

## Examples

>>> Lastovka_solid(300, 0.2139)
1682.0637469909211
chemicals.heat_capacity.Lastovka_solid_integral( $T$, similarity_variable, $M W=$ None)
Integrates solid constant-pressure heat capacity with the similarity variable concept and method as shown in [1].
uses an explicit form as derived with Sympy.

## Parameters

$\mathbf{T}$ [float] Temperature of solid [K]
similarity_variable [float] similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
MW [float, optional] Molecular weight of the pure compound or mixture average, [ $\mathrm{g} / \mathrm{mol}$ ]

## Returns

$\mathbf{H}$ [float] Difference in enthalpy from $0 \mathrm{~K}, \mathrm{~J} / \mathrm{mol}$ if MW given; J/kg otherwise

## See also:

Lastovka_solid

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model is for predicting mass heat capacity, not molar heat capacity like most other methods!

## References

[1]

## Examples

```
>>> Lastovka_solid_integral(300, 0.2139)
283246.1519409122
```

chemicals.heat_capacity.Lastovka_solid_integral_over_T( $T$, similarity_variable, $M W=$ None)
Integrates over T solid constant-pressure heat capacity with the similarity variable concept and method as shown in [1].
uses an explicit form as derived with Sympy.

## Parameters

T [float] Temperature of solid [K]
similarity_variable [float] similarity variable as defined in [1], [ $\mathrm{mol} / \mathrm{g}$ ]
MW [float, optional] Molecular weight of the pure compound or mixture average, [g/mol]

## Returns

$\mathbf{S}$ [float] Difference in entropy from $0 \mathrm{~K}, \mathrm{~J} / \mathrm{mol} / \mathrm{K}$ if MW given; $\mathrm{J} / \mathrm{kg} / \mathrm{K}$ otherwise

## See also:

Lastovka_solid

## Notes

Original model is in terms of $\mathrm{J} / \mathrm{g} / \mathrm{K}$. Note that the model is for predicting mass heat capacity, not molar heat capacity like most other methods!

## References

[1]

## Examples

>>> Lastovka_solid_integral_over_T(300, 0.2139)
1947.5537561495564

### 1.12.7 Utility methods

class chemicals.heat_capacity.PiecewiseHeatCapacity(models)
Create a PiecewiseHeatCapacity object for calculating heat capacity and the enthalpy and entropy integrals using piecewise models.

## Parameters

models [Iterable[HeatCapacity]] Piecewise heat capacity objects, [-]

## Attributes

Tmax
Tmin
models

## Methods

| calculate(T) | Return the heat capacity as a function of temperature. |
| :--- | :--- |
| calculate_integral(Ta, Tb$)$ | Return the enthalpy integral of heat capacity from $T a$ <br> to $T b$. |
| calculate_integral_over_T(Ta, Tb$)$ | Return the entropy integral of heat capacity from $T a$ <br> to $T b$. |
| force_calculate(T) | Return the heat capacity as a function of temperature. |
| force_calculate_integral(Ta, Tb$)$ | Return the enthalpy integral of heat capacity from $T a$ <br> to $T b$. |
| force_calculate_integral_over_T(Ta, Tb$)$ | Return the entropy integral of heat capacity from $T a$ <br> to $T b$. |

### 1.12.8 Fit Coefficients

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.heat_capacity.Cp_data_Poling
Constains data for gases and liquids from [3]. Simple polynomials for gas heat capacity (not suitable for extrapolation) are available for 308 chemicals. Additionally, constant values in at 298.15 K are available for 348 gases. Constant values in at 298.15 K are available for 245 liquids.
chemicals.heat_capacity.TRC_gas_data
A rigorous expression from [1] for modeling gas heat capacity. Coefficients for 1961 chemicals are available.
chemicals.heat_capacity.CRC_standard_data
Constant values tabulated in [4] at 298.15 K. Data is available for 533 gases. Data is available for 433 liquids. Data is available for 529 solids.
chemicals.heat_capacity.Cp_dict_PerryI
Simple polynomials from [5] with vaious exponents selected for each expression. Coefficients are in units of calories $/ \mathrm{mol} / \mathrm{K}$. The full expression is $C_{p}=a+b T+c / T^{2}+d T^{2}$. Data is available for 284 compounds. Some compounds have gas data, some have liquid data, and have solid (crystal structure) data, sometimes multiple coefficients for different solid phases.

```
chemicals.heat_capacity.zabransky_dicts
```

Complicated fits covering different cases and with different forms from [2].

```
chemicals.heat_capacity.Cp_dict_characteristic_temperatures_adjusted_psi4_2022a
```

Theoretically calculated chatacteristic temperatures from vibrational frequencies using psi4
chemicals.heat_capacity.Cp_dict_characteristic_temperatures_psi4_2022a
Theoretically calculated chatacteristic temperatures from vibrational frequencies using psi4, adjusted using a recommended coefficient

```
In [1]: import chemicals
In [2]: chemicals.heat_capacity.Cp_data_Poling
Out[2]:
        Chemical Tmin ... Cpg Cpl
CAS
56-23-5
60-29-7
62-53-3
64-17
64-18-
    methanoic acid (formic acid)
    50.0 \ldots.. 53.45 99.17
... ... ... ... ... ... ...
lritium oxide rran-65-9 NaN (.. 
20291-95-6 2,2,5-trimethylheptane 200.0 ... 229.20 306.40
800000-51-5 hydrogen, normal NaN ... 28.83 NaN
800000-54-8 deuterium, normal NaN ... 29.20 NaN
[368 rows x 10 columns]
In [3]: chemicals.heat_capacity.TRC_gas_data
Out[3]:
CAS
    Chemical Tmin ... J Hfg
    Methanal 50.0 ... 3.46-104700.0
```

(continues on next page)

| 50-32-8 | Benzo[a]pyrene | 298.0 | 13.44 | 324000 |
| :---: | :---: | :---: | :---: | :---: |
| 53-70-3 | Dibenz[a,h]anthracene | 298.0 | 16.63 | 375000 |
| 56-23-5 | Tetrachloromethane | 200.0 | 9.58 | -93700 |
| 56-55-3 | Benz[a]anthracene | 298.0 | 11.45 | 328000 |
|  |  |  |  |  |
| 800000-46-8 | 2,2,(3RS,4RS)-Tetramethylhexane | 200.0 | 22.45 | -188600 |
| 800000-47-9 | 2, (3RS, 4SR),5-Tetramethylhexane | 200.0 | 22.32 | 193700 |
| 800000-48-0 | 2, (3RS, 4RS),5-Tetramethylhexane | 200.0 | 22.14 | -194600 |
| 800000-56-0 | 1-Methylbutyl radical | 200.0 | 22.25 | 54600 |
| 800002-32-8 | Propenoic acid (Dimer) | 50.0 | 13.83 | -686000 |
| [1961 rows x 14 columns] |  |  |  |  |
| In [4]: chemicals.heat_capacity. CRC_standard_dataOut [4]: |  |  |  |  |
|  |  |  |  |  |
|  | Chemical | Hfs | SOg | Cpg |
| CAS |  |  |  |  |
| 50-00-0 | Formaldehyde | NaN | 218.8 | 35.4 |
| 50-32-8 | Benzo[a]pyrene | NaN | NaN | 254.8 |
| 50-69-1 | D-Ribose -1047 | 7200.0 | NaN | NaN |
| 50-78-2 | 2-(Acetyloxy) benzoic acid -815 | 5600.0 | NaN | NaN |
| 50-81-7 | L-Ascorbic acid -116 | 4600.0 | NaN | NaN |
|  |  |  | $\cdots$ | $\cdots$ |
| 92141-86-1 | Cesium metaborate -97 | 2000.0 | NaN | NaN |
| 99685-96-8 | Carbon [fullerene-C60] 2327 | 7000.0 | 544.0 | 512.0 |
| 114489-96-2 | Isobutyl 2-chloropropanoate | NaN | NaN | NaN |
| 115383-22-7 | Carbon [fullerene-C70] 255 | 5000.0 | 614.0 | 585.0 |
| 116836-32-9 | sec-Butyl pentanoate | NaN | NaN | NaN |

[2470 rows x 13 columns]
In [5]: chemicals.heat_capacity.Cp_dict_PerryI['124-38-9'] \# gas only Out[5]:

```
{'g': {'Formula': 'CO2',
```

    'Phase': 'g',
    'Subphase': None,
    'Const': 10.34,
    'Lin': 0.00274,
    'Quadinv': -195500.0,
    'Quad': 0,
    'Tmin': 273.0,
    'Tmax': 1200.0,
    'Error': '1a'\}\}
    In [6]: chemicals.heat_capacity.Cp_dict_PerryI['7704-34-9'] \# crystal and gas
Out [6]:
\{'g': \{'Formula': 'H2S',
'Phase': 'g',
'Subphase': None,
'Const': 7.2,
'Lin': 0.0036,
'Quadinv': 0 ,
(continued from previous page)

```
    'Quad': 0,
    'Tmin': 300.0,
    'Tmax': 600.0,
    'Error': 8.0},
'c': {'Formula': 'S',
    'Phase': 'c',
    'Subphase': 'monoclinic',
    'Const': 4.38,
    'Lin': 0.0044,
    'Quadinv': 0,
    'Quad': 0,
    'Tmin': 368.0,
    'Tmax': 392.0,
    'Error': 3.0}}
In [7]: chemicals.heat_capacity.Cp_dict_PerryI['7440-57-5'] # crystal and liquid
Out[7]:
{'c': {'Formula': 'Au',
    'Phase': 'c',
    'Subphase': None,
    'Const': 5.61,
    'Lin': 0.00144,
    'Quadinv': 0,
    'Quad': 0,
    'Tmin': 273.0,
    'Tmax': 1336.0,
    'Error': 2.0},
    'l': {'Formula': 'Au',
    'Phase': 'l',
    'Subphase': None,
    'Const': 7.0,
    'Lin': 0,
    'Quadinv': 0,
    'Quad': 0,
    'Tmin': 1336.0,
    'Tmax': 1573.0,
    'Error': 5.0}}
In [8]: chemicals.heat_capacity.zabransky_dicts.keys()
Out[8]: dict_keys(['Zabransky spline, averaged heat capacity', 'Zabransky
    ↔quasipolynomial, averaged heat capacity', 'Zabransky spline, constant-pressure',
    \rightarrow ' Z a b r a n s k y ~ q u a s i p o l y n o m i a l , ~ c o n s t a n t - p r e s s u r e ' , ~ ' Z a b r a n s k y ~ s p l i n e , ~ s a t u r a t i o n ' ,
    \hookrightarrow'Zabransky quasipolynomial, saturation'])
```


### 1.13 IAPWS: International Association for the Properties of Water and Steam (chemicals.iapws)

This module contains the core of the IAPWS-95 and IAPWS-97 standards. The objective of this module is to contain extremely fast functions to calculate several basic properties of water.
The simplest interfaces are iapws95_rho for density calculation only and iapws95_properties for some basic properties.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

```
- IAPWS-95 Basic Solvers
- IAPWS-97 Basic Solvers
- IAPWS-95 Properties
- IAPWS Saturation Pressure/Temperature
- IAPWS Saturation Density
- IAPWS Constants
- IAPWS-97 Region 1
- IAPWS-97 Region 2
- IAPWS-97 Region 3
- IAPWS-97 Region 3 PT Backwards Equation Boundaries
- IAPWS-97 Region 3 PT Backwards Equations
- IAPWS-97 Region 5
- IAPWS-95 Ideal Gas Terms
- IAPWS-95 Residual Terms
```


### 1.13.1 IAPWS-95 Basic Solvers

chemicals.iapws.iapws95_rho $(T, P)$
Calculate the density of water according to the IAPWS-95 standard given a temperature $T$ and pressure $P$. The phase is determined in this calculation.

## Parameters

$$
\mathbf{T} \text { [float] Temperature, [K] }
$$

$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$
See also:

```
iapws95_rhol_sat
iapws95_rhog_sat
```


## Notes

There is a sudden transition at the saturation pressure between liquid and vapor density, by design.
This solution is iterative due to the nature of the equation. The solution procedure begins with IAPWS-97's explicit equations as an initial guess, extrapolating when out of range. If the temperature is under the critical temperature, the saturation density is calculated, and used to ensure the solver begins in the feasible region. Newton's method converges extremely, normally after 2 or 3 iterations.

Temperatures under 273.15 K are not officially supported by [1], but a solution is still attempted down to 235 K .

## References

[1]

## Examples

```
>>> iapws95_rho(T=300.0, P=1e6)
```

996.96002269499

1 GPa and 5000 K are suggested as upper limits of [1] although there are no hardcoded limits for temperature and pressure.
>>> iapws95_rho(T=5000.0, $\mathrm{P}=1 \mathrm{e} 9)$
326.79451662743

## chemicals.iapws.iapws95_P (T, rho)

Calculate the pressure of water according to the IAPWS-95 standard given a temperature $T$ and mass density rho.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]
rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## Returns

$\mathbf{P}$ [float] Pressure, [Pa]

## Notes

The IAPWS-95 model is explicit with inputs of temperature and density, so this is a direct calculation with no iteration required.

## References

[1]

## Examples

>>> iapws95_P(330.0, iapws95_rho(T=330.0, $\mathrm{P}=8 \mathrm{e} 5)$ )
8 e 5
>>> iapws95_P(823.0, 40.393893559703734)
14 e 6

Not all temperature and density inputs provide a stable solution; for example anything between the vapor and gas saturation curves. In some but not all of these cases a negative pressure is returned:

```
>>> iapws95_P(T=300, rho=300)
```

-1.526394720e+23

## chemicals.iapws.iapws95_T(P,rho)

Calculate the temperature of water according to the IAPWS-95 standard given a density rho and pressure $P$.

## Parameters

$\mathbf{P}$ [float] Pressure, [Pa]
rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## Returns

$\mathbf{T}$ [float] Temperature, [K]

## Notes

This solution is iterative due to the nature of the equation. The solution procedure begins with IAPWS-97's equations as an initial guess, extrapolating when out of range. Newton's method converges extremely, normally after 2 or 3 iterations.

Due to water's unique density curve, there is a temperature region spanning 273.15 K to 280.005 K where there are two solutions. No guarantee is made as to which solution will be returned.

## References

[1]

## Examples

>>> iapws95_T(P=1e6, rho=995.0)
306.461547194

### 1.13.2 IAPWS-97 Basic Solvers

chemicals.iapws.iapws97_rho( $T, P$, use_95_boundary=False)
Calculate the density of water in $\mathrm{kg} / \mathrm{m}^{\wedge} 3$ according to the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]
use_95_boundary [bool, optional] If True, respect the IAPWS-95 vapor pressure curve instead of the IF-97 one, [-]

## Returns

rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

The range of validity of this formulation is as follows:
For $P \leq 100 \mathrm{MPa}$ :

$$
273.15 \mathrm{~K} \leq T \leq 1073.15 \mathrm{~K}
$$

For $P \leq 50 \mathrm{MPa}$ :

$$
1073.15 \mathrm{~K} \leq T \leq 2273.15 \mathrm{~K}
$$

A ValueError is raised if the temperature or the pressure is out of bounds.
IAPWS is implemented in four regions in the $T-P$ domain: Region 1 (liquid), region 2 (gas and supercritical gas), region 5 (high temperature gas), and region 3 (near-critical). Significant discontinuities exist between the transitions of each regions. In region 3, there are 26 sub-regions and the correlation has the least accuracy.
For many applications, the discontinuities in IF-97 can be problematic and the slower IAPWS-95 must be used. IAPWS-95 also has a wider range of applicability.

## References

## [1]

## Examples

```
>>> iapws97_rho(648.6, 22.5e6)
353.06081088726
>>> iapws97_rho(330.0, 8e5)
985.10498080770
>>> iapws97_rho(823.0, 14e6)
40.39293607288123
>>> iapws97_rho(2000.0, 3e7)
32.11456228328856
```

```
chemicals.iapws.iapws97_P(T,rho)
```

Calculate the pressure of water according to the IAPWS-97 standard given a temperature $T$ and mass density rho.

## Parameters

T [float] Temperature, [K]
rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## Returns

$\mathbf{P}$ [float] Pressure, [Pa]

## Notes

The range of validity of this formulation is as follows:
For $P \leq 100 \mathrm{MPa}$ :

$$
273.15 \mathrm{~K} \leq T \leq 1073.15 \mathrm{~K}
$$

For $P \leq 50 \mathrm{MPa}$ :

$$
1073.15 \mathrm{~K} \leq T \leq 2273.15 \mathrm{~K}
$$

A ValueError is raised if the temperature or density is out of bounds.
Newton's method with analytical derivatives is used here to solve these equations. The solver tolerance is as tight as it can be without causing wasted iterations that do not improve the result at all. Pressure changes quickly with density however, and some discrepancy between solvers is to be expected.
For region 3, there are really two formulations present in IAPWS-97. There is a Helmholtz energy equation (Temperature and density dependent), and also 26 separate backwards equations for $r h o$ which depend on $T$ and $P$. The Helmholtz energy equation is much more accurate and does not have discontinuities. The two sets of equations agree closely not not perfectly. By design, iapws97_rho implements the 26 T-P equations and this implements the Helmholtz energy equation. This means that in region 3 solutions will not be consistent. For consistency requirements, IAPWS-95 is recommended.

This solver does not have any issues with multiple solutions. The solvers have been checked to achieve a relative solution tolerance of $5 \mathrm{e}-9$ on 100 million points.

## References

[1]

## Examples

```
>>> iapws97_P(330.0, iapws97_rho(T=330.0, P=8e5))
8e5
>>> iapws97_P(823.0, 40.39293607288123)
14e6
>>> iapws97_P(T=2000.0, rho=32.11456228328856)
3e7
```

Region 3 point - does not implement the same equations as iapws97_rho!

```
>>> iapws97_P(648.6, iapws97_rho(T=648.6, P=22.5e6))
22499974.093936257
```

chemicals.iapws.iapws97_T ( $P$, rho)
Calculate the temperature of water according to the IAPWS-97 standard given a pressure $P$ and mass density rho.

## Parameters

$\mathbf{P}$ [float] Pressure, [Pa]
rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## Returns

T [float] Temperature, [K]

## Notes

The range of validity of this formulation is as follows:
For $P \leq 100 \mathrm{MPa}$ :

$$
273.15 \mathrm{~K} \leq T \leq 1073.15 \mathrm{~K}
$$

For $P \leq 50 \mathrm{MPa}$ :

$$
1073.15 \mathrm{~K} \leq T \leq 2273.15 \mathrm{~K}
$$

A ValueError is raised if the pressure or density is out of bounds.
Newton's method with analytical derivatives is used here to solve these equations. The solver tolerance is as tight as it can be without causing wasted iterations that do not improve the result at all.
Due to water's unique density curve, there is a temperature region spanning 273.15 K to 280.005 K where there are two solutions. No guarantee is made as to which solution will be returned.

## References

[1]

## Examples

```
>>> iapws97_T(8e5, iapws97_rho(T=330.0, P=8e5))
330.0
>>> iapws97_T(14e6, 40.39293607288123)
823.0
>>> iapws97_T(P=3e7, rho=32.11456228328856)
2000.0
```


### 1.13.3 IAPWS-95 Properties

chemicals.iapws.iapws95_properties $(T, P)$
Calculate some basic properties of water according to the IAPWS-95 standard given a temperature $T$ and pressure $P$.

The properties are density rho, internal energy $U$, entropy $S$, enthalpy $H$, isochoric heat capacity $C v$, isobaric heat capacity $C p$, speed of sound $w$, Joule-Thomson coefficient $J T$, isothermal throttling coefficient delta_T, isentropic temperature-pressure coefficient beta_s, and the derivative of mass density with respect to pressure at constant temperature $d r h o \_d P$.

This function is intended as a demonstration of how to use the IAPWS-95 equations. For that reason, mass-units are used in all returned variables.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$
$\mathbf{U}$ [float] Internal energy of water, [J/(kg)]
S [float] Entropy of water, [J/(kg*K)]
H [float] Enthalpy of water, [J/(kg)]
Cv [float] Isochoric heat capacity, [J/(kg*K)]
Cp [float] Isobaric heat capacity, [J/(kg*K)]
$\mathbf{w}$ [float] Speed of sound, [ $\mathrm{m} / \mathrm{s}$ ]
JT [float] Joule-Thomson coefficient, [K/Pa]
delta_T [float] Isothermal throttling coefficient, [J/(kg*Pa)]
beta_s [float] Isentropic temperature-pressure coefficient, $[\mathrm{K} / \mathrm{Pa}$ ]
drho_dP [float] Derivative of mass density with respect to pressure at constant temperature, $\left[\mathrm{kg} /\left(\mathrm{m}^{\wedge} 3 * \mathrm{~Pa}\right)\right]$

## Notes

Hundreds of useful properties can be obtained from the IAPWS-95 model. It is intended for this function to serve as a useful starting point to those. Calculating every property with every set of units is beyond the scope of chemicals. The functions like iapws95_dAr_ddelta can be used directly in your own implementation - where you can calculate only those properties which are necessary, for maximum speed.
The formulas are as follows:

$$
\begin{gathered}
\frac{u(\delta, \tau)}{R T}=\tau\left(\phi_{\tau}^{\mathrm{o}}+\phi_{\tau}^{\mathrm{r}}\right) \\
\frac{s(\delta, \tau)}{R}=\tau\left(\phi_{\tau}^{\mathrm{o}}+\phi_{\tau}^{\mathrm{r}}\right)-\phi^{\mathrm{o}}-\phi^{\mathrm{r}} \\
\frac{h(\delta, \tau)}{R T}=1+\tau\left(\phi_{\tau}^{\mathrm{o}}+\phi_{\tau}^{\mathrm{r}}\right)+\delta \phi_{\delta}^{\mathrm{r}} \\
\frac{c_{v}(\delta, \tau)}{R}=-\tau^{2}\left(\phi_{\tau \tau}^{\mathrm{o}}+\phi_{\tau \tau}^{\mathrm{r}}\right)
\end{gathered}
$$

$$
\begin{gathered}
\frac{c_{p}(\delta, \tau)}{R}=-\tau^{2}\left(\phi_{\tau \tau}^{\mathrm{o}}+\phi_{\tau \tau}^{\mathrm{r}}\right)+\frac{\left(1+\delta \phi_{\delta}^{\mathrm{r}}-\delta \tau \phi_{\delta \tau}^{\mathrm{r}}\right)^{2}}{1+2 \delta \phi_{\delta}^{\mathrm{r}}+\delta^{2} \phi_{\delta \delta}^{\mathrm{r}}} \\
\frac{w^{2}(\delta, \tau)}{R T}=1+2 \delta \phi_{\delta}^{\mathrm{r}}+\delta^{2} \phi_{\delta \delta}^{\mathrm{r}}-\frac{\left(1+\delta \phi_{\delta}^{\mathrm{r}}-\delta \tau \phi_{\delta \tau}^{\mathrm{r}}\right)^{2}}{\tau^{2}\left(\phi_{\tau \tau}^{\mathrm{o}}+\phi_{\tau \tau}^{\mathrm{r}}\right)} \\
\mu R \rho=\frac{-\left(\delta \phi_{\delta}^{\mathrm{r}}+\delta^{2} \phi_{\delta \delta}^{\mathrm{r}}+\delta \tau \phi_{\delta \tau}^{\mathrm{r}}\right)}{\left(1+\delta \phi_{\delta}^{\mathrm{r}}-\delta \tau \phi_{\delta \tau}^{\mathrm{r}}\right)^{2}-\tau^{2}\left(\phi_{\tau \tau}^{\mathrm{o}}+\phi_{\tau \tau}^{\mathrm{r}}\right)\left(1+2 \delta \phi_{\delta}^{\mathrm{r}}+\delta^{2} \phi_{\delta \delta}^{\mathrm{r}}\right)} \\
\delta_{T} \rho=1-\frac{1+\delta \phi_{\delta}^{\mathrm{r}}-\delta \tau \phi_{\delta \tau}^{\mathrm{r}}}{1+2 \delta \phi_{\delta}^{\mathrm{r}}+\delta^{2} \phi_{\delta \delta}^{\mathrm{r}}} \\
\beta_{S} \rho R=\frac{1+\delta \phi_{\delta}^{\mathrm{r}}-\delta \tau \phi_{\delta \tau}^{\mathrm{r}}}{\left(1+\delta \phi_{\delta}^{\mathrm{r}}-\delta \tau \phi_{\delta \tau}^{\mathrm{r}}\right)^{2}-\tau^{2}\left(\phi_{\tau \tau}^{o}+\phi_{\tau \tau}^{\mathrm{r}}\right)\left(1+2 \delta \phi_{\delta}^{\mathrm{r}}+\delta^{2} \phi_{\delta \delta}^{\mathrm{r}}\right)}
\end{gathered}
$$

This derivative isn't part of the same table of properties, but it is needed by the transport calculation routines:

$$
\left(\frac{\partial \rho}{\partial P}\right)_{T}=\frac{1}{R T\left(1+2 \delta \alpha_{\delta}^{\mathrm{r}}+\delta^{2} \alpha_{\delta \delta}^{\mathrm{r}}\right)}
$$

## References

[1]

## Examples

```
>>> iapws95_properties(T=300.0, P=1e6)
(996.96002269, 112478.998245, 392.813902893, 113482.047492, 4127.21730497, 4178.
๑103605593, 1503.035983829, -2.202166728257e-07, 0.000920088074745, 1.
\hookrightarrow985617879134e-08, 4.48108429028e-07)
```

>>> rho, U, S, H, Cv, Cp, w, JT, delta_T, beta_s, drho_dP = iapws95_
$\rightarrow$ properties $(T=500.0, \mathrm{P}=1 \mathrm{e} 5)$
>>> w
548.3138393244

### 1.13.4 IAPWS Saturation Pressure/Temperature

## chemicals.iapws.iapws95_Psat ( $T$ )

Compute the saturation pressure of the IAPWS-95 equation using high- fidelity polynomial fits. These have a relative accuracy of under $1 \mathrm{e}-12$, and are generated by solving the saturation equations under the high-precision environment of mpmath. The range of the fit is 235 K to 647.096 K , the critical point.

$$
P_{\text {sat }}=P_{c} \exp (\operatorname{polynomial}(a(T-b)))
$$

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition, [K]

## Returns

Psat [float] Saturation vapor pressure, [Pa]

## See also:

```
iapws95_saturation
```


## Notes

This method should be used in preference to iapws95_saturation. Although using mpmath generates slightly different results than using plain floating point numbers, the requirement for the saturation curve is to be smooth, and continuous; mpmath makes this easy and the saturation equations were solved extremely high precision, well under a floating point's error.

The polynomial coefficients have been carefully chosen to be able to be evaluated accurately with horner's method, although they are derived as a Chebyshev approximation originally.

## Examples

```
>>> iapws95_Psat(400.0)
```

245769. 3455

## chemicals.iapws.iapws95_dPsat_dT(T)

Compute the temperature derivative of saturation pressure of the IAPWS-95 equation using high- fidelity polynomial fits. The range of the fit is 235 K to 647.096 K , the critical point.

$$
\begin{gathered}
P_{\text {sat }}=P_{c} \exp (\operatorname{polynomial}(a(T-b))) \\
\frac{\partial P_{\text {sat }}}{\partial T}=a P_{c} \exp (\operatorname{polynomial}(a(T-b))) \exp \left(\frac{\partial \operatorname{polynomial}(a(T-b))}{\partial T}\right)
\end{gathered}
$$

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition and its temperature derivative, [K]

## Returns

dPsat_dT [float] First temperature derivative of Saturation vapor pressure, $[\mathrm{Pa} / \mathrm{K}]$
Psat [float] Saturation vapor pressure, [Pa]

## Notes

Psat must be calculated in the calculation of the derivative, so it is returned as well which may be useful in some applications.

## Examples

```
>>> iapws95_dPsat_dT(400.0)
(7483.62075827, 245769.3455657)
```

chemicals.iapws.iapws92_Psat ( $T$ )
Compute the saturation pressure of the IAPWS-92 equation.

$$
P_{\text {sat }}=P_{c} \exp \left(\frac{T_{c}}{T}\left[a_{1} \tau+a_{2} \tau^{1.5}+a_{3} \tau^{3}+a_{4} \tau^{3.5} a_{5} \tau^{4}+a_{6} \tau^{7.5}\right]\right)
$$

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition and its temperature derivative, $[\mathrm{K}]$

## Returns

Psat [float] Saturation vapor pressure, [Pa]

## Notes

The coefficients are $[-7.85951783,1.84408259,-11.7866497,22.6807411,-15.9618719,1.80122502]$

## Examples

```
>>> iapws92_Psat(400.0)
245765.2635418
```


## chemicals.iapws.iapws92_dPsat_dT(T)

Compute the temperature derivative of saturation pressure of the IAPWS-92 equation.

$$
P_{\text {sat }}=P_{c} \exp \left(\frac{T_{c}}{T}\left[a_{1} \tau+a_{2} \tau^{1.5}+a_{3} \tau^{3}+a_{4} \tau^{3.5} a_{5} \tau^{4}+a_{6} \tau^{7.5}\right]\right)
$$

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition and its temperature derivative, [K]

## Returns

dPsat_dT [float] First temperature derivative of saturation vapor pressure, $[\mathrm{Pa} / \mathrm{K}]$
Psat [float] Saturation vapor pressure, [Pa]

## Notes

The coefficients are [-7.85951783, 1.84408259, -11.7866497, 22.6807411, -15.9618719, 1.80122502]

## Examples

>>> iapws92_dPsat_dT(400.0)
(7483.47094105, 245765.263541)
chemicals.iapws.iapws95_Tsat $(P)$
Compute the saturation temperature of the IAPWS-95 equation. The range of the fit is 235 K to 647.096 K , the critical point.

## Parameters

Psat [float] Saturation vapor pressure specified, [Pa]

## Returns

T [float] Temperature at which the saturation pressure occurs, [K]
See also:
iapws95_Psat
Tsat_IAPWS

## Notes

This method is quite fast and precise because it starts with great initial guesses and the equation is well-bounded. The precision of this calculation should be the same as iapws95_Psat.

## Examples

>>> iapws95_Tsat(iapws95_Psat(400.0))
400.0

## chemicals.iapws.iapws95_saturation(T, xtol=le-05, rhol_guess=None, rhog_guess=None)

Solve the vapor-liquid saturation equations of IAPWS-95 given a specified temperature. With floating point numbers, the achievable tolerance is somewhat low so xtol is exposed as a setting - it can be adjusted somewhat. Density guesses may be provided, otherwise they will be estimated.

$$
\begin{aligned}
& G_{l i q}\left(T, \rho_{l}\right)=G_{v a p}\left(T, \rho_{g}\right) \\
& P_{l i q}\left(T, \rho_{l}\right)=P_{v a p}\left(T, \rho_{g}\right)
\end{aligned}
$$

## Parameters

T [float] Temperature at which to solve for saturation condition, [K]
xtol [float] Tolerance for solver, [-]
rhol_guess [float, optional] Liquid density of water at saturation (guess), $[\mathrm{kg} / \mathrm{m} \wedge 3]$
rhog_guess [float, optional] Vapor density of water at saturation (guess), $[\mathrm{kg} / \mathrm{m} \wedge 3$ ]

## Returns

Psat [float] Saturation vapor pressure, 3[Pa]
rhol [float] Saturation liquid water density, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$
rhog [float] Saturation vapor water density, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.$ ]

## Notes

This is not a perfect function.
With mpmath multiple precision, the equation can be solved down to 233.6 K and up to 647.095999995 K within 10 parts in a billion of the critical point exactly.

Reasons for non-convergence include floating point issues as delta becomes 1 , and zero division errors in the matrix inverse.

## Examples

```
>>> iapws95_saturation(400.0, xtol=1e-6)
(245769.345, 937.4860, 1.3694075)
>>> iapws95_saturation(647.0955, xtol=1e-7)
(22063866.35, 325.70, 318.277)
```


## chemicals.iapws.iapws11_Psub ( $T$ )

Compute the sublimation pressure of the frozen water using the IAPWS-11 equation from the Revised Release on the Pressure along the Melting and Sublimation Curves of Ordinary Water Substance.

$$
\begin{gathered}
P_{s u b}=P_{t} \exp \left(\theta^{-1} \sum_{i=1}^{3} a_{i} \theta^{b_{i}}\right) \\
\theta=\frac{T}{T_{t}}
\end{gathered}
$$

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the sublimation condition [K]

## Returns

Psub [float] Sublimation vapor pressure, [Pa]

## Notes

The triple temperature is 273.16 K , and triple pressure 611.657 Pa .
The coefficients are as follows:

$$
\text { ais }=[-0.212144006 \mathrm{E} 2,0.273203819 \mathrm{E} 2,-0.610598130 \mathrm{E} 1]
$$

$$
\text { bis }=[0.333333333 \mathrm{E}-2,0.120666667 \mathrm{E} 1,0.170333333 \mathrm{E} 1]
$$

The equation is valid from 50 K to the triple temperature.

## Examples

```
>>> iapws11_Psub(230.0)
8.947352740189151
```


### 1.13.5 IAPWS Saturation Density

chemicals.iapws.iapws95_rhol_sat ( $T$ )
Compute the saturation liquid density of the IAPWS-95 equation using high- fidelity polynomial fits. These have a relative accuracy of under $1 \mathrm{e}-13$, except near the critical point where it rises to $1 \mathrm{e}-10$, and are generated by solving the saturation equations under the high-precision environment of mpmath. The range of the fit is 235 K to 647.096 K , the critical point.

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition, [K]

## Returns

rhol [float] Saturation liquid density, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## See also:

```
iapws92_rhol_sat
```


## Notes

This method should be used in preference to iapws92_rhol_sat.

## Examples

```
>>> iapws95_rhol_sat(400.0)
```

937.48603939

## chemicals.iapws.iapws95_rhog_sat (T)

Compute the saturation vapor density of the IAPWS-95 equation using high- fidelity polynomial fits. These have a relative accuracy of under $1 \mathrm{e}-13$, except near the critical point where it rises to $1 \mathrm{e}-10$, and are generated by solving the saturation equations under the high-precision environment of mpmath. The range of the fit is 235 K to 647.096 K , the critical point.

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition, [K]

## Returns

rhol [float] Saturation vapor density, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.$ ]

## See also:

iapws92_rhog_sat

## Notes

This method should be used in preference to iapws92_rhog_sat.

## Examples

>>> iapws95_rhog_sat(400.0)
1.3694075410
chemicals.iapws.iapws95_drhol_sat_dT ( $T$ )
Compute the first temperature derivative of saturation liquid density of the IAPWS-95 equation using highfidelity polynomial fits. The actual saturated liquid density is returned as well.

The range of the fit is 235 K to 647.096 K , the critical point.

## Parameters

$\mathbf{T}$ [float] Temperature at which to calculate the saturation condition and its derivative, [K]

## Returns

drhol_dT [float] First temperature derivative of saturation liquid density, $\left[\mathrm{kg} /\left(\mathrm{m} \wedge 3^{*} \mathrm{~K}\right)\right.$ ]
rhol [float] Saturation liquid density, $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]$

## Examples

>>> iapws95_drhol_sat_dT(400.0)
(-0.835194603380, 937.486039392)

## chemicals.iapws.iapws92_rhol_sat( $T$ )

Calculates saturation liquid mass density of water using the IAPWS SR1-86(1992) [1] [2] explicit equation.

$$
\begin{gathered}
\frac{\rho_{l}^{s a t}}{\rho_{c}}=1+b_{1} \tau^{1 / 3}+b_{2} \tau^{2 / 3}+b_{3} \tau^{5 / 3}+b_{4} \tau^{16 / 3}+b_{5} \tau^{43 / 3}+b_{6} \tau^{110 / 3} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
$$

## Parameters

T [float] Temperature of water, [K]

## Returns

rhol_sat [float] Saturation liquid mass density of water $\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.$ ]
See also:

```
iapws95_rhol_sat
```


## Notes

This equation is fit to experimental data to within its accuracy. It does not satisfy the equilibrium conditions for the IAPWS-95 or IAPWS-97 formulations.

The values of the constants are as follows:
b1 = 1.99274064; b2 = 1.09965342; b3 $=-0.510839303 ;$ b4 $=-1.75493479 ;$ b5 $=-45.5170352 ;$ b6 $=-$ 6.74694450 e 5

## References

[1], [2]

## Examples

```
>>> iapws92_rhol_sat(300.)
996.5089712803
```

chemicals.iapws.iapws92_rhog_sat ( $T$ )
Calculates saturation vapor mass density of water using the IAPWS SR1-86(1992) [1] [2] explicit equation.

$$
\begin{gathered}
\ln \left(\frac{\rho_{g}^{\text {sat }}}{\rho_{c}}\right)=1+c_{1} \tau^{2 / 6}+c_{2} \tau^{4 / 6}+c_{3} \tau^{8 / 6}+c_{4} \tau^{18 / 6}+c_{5} \tau^{37 / 6}+c_{6} \tau^{71 / 6} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
$$

## Parameters

$\mathbf{T}$ [float] Temperature of water, [K]

## Returns

rhog_sat [float] Saturation vapor mass density of water [ $\mathrm{kg} / \mathrm{m}^{\wedge} 3$ ]

## See also:

iapws95_rhog_sat

## Notes

This equation is fit to experimental data to within its accuracy. It does not satisfy the equilibrium conditions for the IAPWS-95 or IAPWS-97 formulations.

The values of the constants are as follows:
$\mathrm{c} 1=-2.03150240 ; \mathrm{c} 2=-2.68302940 ; \mathrm{c} 3=-5.38626492 ; \mathrm{c} 4=-17.2991605 ; \mathrm{c} 5=-44.7586581 ; \mathrm{c} 6=-63.9201063$

## References

[1], [2]

## Examples

```
>>> iapws92_rhog_sat(300.)
0.0255887212886
```


### 1.13.6 IAPWS Constants

```
chemicals.iapws.iapws95_Tc = 647.096
```

Critical temperature of water in K according to IAPWS-95, also used in IAPWS-97
chemicals.iapws.iapws95_Pc $=22064000.0$
Critical pressure of water in Pa according to IAPWS-95, also used in IAPWS-97
chemicals.iapws.iapws95_rhoc $=322.0$
Critical density of water in $\mathrm{kg} / \mathrm{m}^{\wedge} 3$ according to IAPWS-95, also used in IAPWS-97
chemicals.iapws.iapws95_MW = 18.015268
Molecular weight of water in $\mathrm{g} / \mathrm{mol}$ according to IAPWS-95, also used in IAPWS-97
chemicals.iapws.iapws95_R $=461.51805$
Specific gas constant in $\mathrm{J} /(\mathrm{kg} * \mathrm{~K})$ according to IAPWS-95
chemicals.iapws.iapws97_R = 461.526
Specific gas constant in $\mathrm{J} /(\mathrm{kg} * \mathrm{~K})$ according to IAPWS-97
chemicals.iapws.iapws95_Tt = 273.16
Triple temperature of water in K according to IAPWS

### 1.13.7 IAPWS-97 Region 1

chemicals.iapws.iapws97_G_region1 (tau, pi)
Calculates the dimensionless Gibbs free energy for water according to the IAPWS-97 standard (for region 1).

$$
\gamma=\sum_{i=1}^{34} I_{i}(7.1-\pi)^{I_{i}}(\tau-1.222)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (1386 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(16.53 \mathrm{MPa}),[-]$

## Returns

G [float] Dimensionless Gibbs energy G/(RT), [-]

## Examples

```
>>> iapws97_G_region1(1386/277.15, 101325/16.53E6)
-0.00016341033954414
```

chemicals.iapws.iapws97_dG_dpi_region1(tau, pi)
Calculates the derivative of dimensionless Gibbs free energy with respect to pi for water according to the IAPWS97 standard (for region 1).

$$
\frac{\partial \gamma}{\partial \pi}=\sum_{i=1}^{34}-n_{i} I_{i}(7.1-\pi)^{I_{i}-1}(\tau-1.222)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (1386 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(16.53 \mathrm{MPa}),[-]$

## Returns

dG_dpi [float] Derivative of dimensionless Gibbs energy G/(RT) with respect to pi, [-]

## Notes

Used in density solution. This contains a hand-optimized implementation with a single division, no power operations, 65 multiplications, 16 local variables, and a minimum number of additions.

## Examples

```
>>> iapws97_dG_dpi_region1(1386/277.15, 101325/16.53E6)
0.1292327182544
```

chemicals.iapws.iapws97_d2G_dpi2_region1(tau, pi)
Calculates the second derivative of dimensionless Gibbs free energy with respect to pi for water according to the IAPWS-97 standard (for region 1).

$$
\frac{\partial^{2} \gamma}{\partial \pi^{2}}=\sum_{i=1}^{34} n_{i} I_{i}\left(I_{i}-1\right)(7.1-\pi)^{I_{i}-2}(\tau-1.222)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (1386 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(16.53 \mathrm{MPa})$, [-]

## Returns

d2G_dpi2 [float] Second Derivative of dimensionless Gibbs energy G/(RT) with respect to pi, [-]

## Examples

```
>>> iapws97_d2G_dpi2_region1(1386/277.15, 101325/16.53E6)
    -0.0010570100274769
```

chemicals.iapws.iapws97_dG_dtau_region1(tau, pi)
Calculates the derivative of dimensionless Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 1).

$$
\frac{\partial \gamma}{\partial \tau}=\sum_{i=1}^{34} n_{i}(7.1-\pi)^{I_{i}} J_{i}(\tau-1.222)^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, (1386 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(16.53 \mathrm{MPa}),[-]$

## Returns

dG_dtau [float] Derivative of dimensionless Gibbs energy G/(RT) with respect to tau, [-]

## Examples

```
>>> iapws97_dG_dtau_region1(1386/277.15, 101325/16.53E6)
0.026440334282967
```


## chemicals.iapws.iapws97_d2G_dtau2_region1(tau, pi)

Calculates the second derivative of dimensionless Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 1).

$$
\frac{\partial^{2} \gamma}{\partial \tau^{2}}=\sum_{i=1}^{34} n_{i}(7.1-\pi)^{I_{i}} J_{i}\left(J_{i}-1\right)(\tau-1.222)^{J_{i}-2}
$$

## Parameters

tau [float] Dimensionless temperature, (1386 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(16.53 \mathrm{MPa}),[-]$

## Returns

d2G_dtau2 [float] Second Derivative of dimensionless Gibbs energy G/(RT) with respect to tau, [-]

## Examples

```
>>> iapws97_d2G_dtau2_region1(1386/277.15, 101325/16.53E6)
```

-0. 3645169808573

## chemicals.iapws.iapws97_d2G_dpidtau_region1(tau, pi)

Calculates the second derivative of dimensionless Gibbs free energy with respect to tau and pi for water according to the IAPWS-97 standard (for region 1).

$$
\frac{\partial^{2} \gamma}{\partial \tau \partial \pi}=\sum_{i=1}^{34}-n_{i} I_{i}(7.1-\pi)^{I_{i}} J_{i}(\tau-1.222)^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, (1386 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(16.53 \mathrm{MPa}),[-]$

## Returns

d2G_dpidtau [float] Second Derivative of dimensionless Gibbs energy G/(RT) with respect to tau and pi, [-]

## Examples

```
>>> iapws97_d2G_dpidtau_region1(1386/277.15, 101325/16.53E6)
0.025837659858819
```


### 1.13.8 IAPWS-97 Region 2

chemicals.iapws.iapws97_GO_region2 (tau, pi)
Calculates the dimensionless ideal gas Gibbs free energy for water according to the IAPWS-97 standard (for region 2 ).

$$
\gamma^{\circ}=\ln \pi+\sum_{i=1}^{9} n_{i}^{\circ} \tau^{J_{i}^{\circ}}
$$

## Parameters

tau [float] Dimensionless temperature, (540 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

G0 [float] Dimensionless ideal gas Gibbs energy G0/(RT), [-]

## Examples

>>> iapws97_G0_region2(540/300.0, 101325/1e6)
3.3180953922351
chemicals.iapws.iapws97_dG0_dtau_region2(tau, pi)
Calculates the first derivative of dimensionless ideal gas Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial \gamma^{\circ}}{\partial \tau}=\sum_{i=1}^{9} n_{i}^{\circ} J_{i}^{\circ} \tau^{J_{i}^{\circ}-1}
$$

## Parameters

tau [float] Dimensionless temperature, (540 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}$ ), [-]

## Returns

dG0_dtau [float] First derivative of dimensionless ideal gas Gibbs energy G0/(RT) with respect to tau, [-]

## Notes

This function does not depend on pi but it is accepted for consistency.

## Examples

```
>>> iapws97_dG0_dtau_region2(540/300.0, 101325/1e6)
```

10. 2374188173906
chemicals.iapws.iapws97_d2G0_dtau2_region2 (tau, pi)
Calculates the second derivative of dimensionless ideal gas Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial^{2} \gamma^{\circ}}{\partial \tau^{2}}=\sum_{i=1}^{9} n_{i}^{\circ} J_{i}^{\circ}\left(J_{i}^{\circ}-1\right) \tau^{J_{i}^{\circ}-2}
$$

## Parameters

tau [float] Dimensionless temperature, (540 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

d2G0_dtau2 [float] Second derivative of dimensionless ideal gas Gibbs energy G0/(RT) with respect to tau, [-]

## Notes

This function does not depend on pi but it is accepted for consistency.

## Examples

```
>>> iapws97_d2G0_dtau2_region2(540/300.0, 101325/1e6)
```

-1.2472096479372

## chemicals.iapws.iapws97_Gr_region2(tau, pi)

Calculates the dimensionless residual Gibbs free energy for water according to the IAPWS-97 standard (for region 2).

$$
\gamma^{r}=\sum_{i=1}^{43} n_{i} \pi^{I_{i}}(\tau-0.5)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, $(540 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

Gr [float] Dimensionless residual Gibbs energy Gr/(RT), [-]

## Examples

```
>>> iapws97_Gr_region2(540/300.0, 101325/1e6)
-0.71851548053980
```

chemicals.iapws.iapws97_dGr_dpi_region2 (tau, pi)
Calculates the first derivative of dimensionless residual Gibbs free energy with respect to pi for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial \gamma^{r}}{\partial \pi}=\sum_{i=1}^{43} n_{i} I_{i} \pi^{I_{i}-1}(\tau-0.5)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (540 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

dGr_dpi [float] Derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to $p i$, [-]

## Notes

Used in density solution.

## Examples

```
>>> iapws97_dGr_dpi_region2(540/300.0, 101325/1e6)
```

-27.7714056629532

## chemicals.iapws.iapws97_d2Gr_dpi2_region2(tau, pi)

Calculates the second derivative of dimensionless residual Gibbs free energy with respect to $p i$ for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial^{2} \gamma^{r}}{\partial \pi^{2}}=\sum_{i=1}^{43} n_{i} I_{i}\left(I_{i}-1\right) \pi^{I_{i}-2}(\tau-0.5)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, $(540 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

d2Gr_dpi2 [float] Second Derivative of dimensionless residual Gibbs energy Gr/(RT) with respect to $p i,[-]$

## Examples

```
>>> iapws97_d2Gr_dpi2_region2(540/300.0, 101325/1e6)
```

-983.15187604898
chemicals.iapws.iapws97_dGr_dtau_region2 (tau, pi)
Calculates the first derivative of dimensionless residual Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial \gamma^{r}}{\partial \tau}=\sum_{i=1}^{43} n_{i} \pi^{I_{i}} J_{i}(\tau-0.5)^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, $(540 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

dGr_dtau [float] Derivative of dimensionless residual Gibbs energy Gr/(RT) with respect to tau, [-]

## Examples

>>> iapws97_dGr_dtau_region2(540/300.0, 101325/1e6)
-18.1535856049444

## chemicals.iapws.iapws97_d2Gr_dtau2_region2(tau, pi)

Calculates the second derivative of dimensionless residual Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial^{2} \gamma^{r}}{\partial \tau^{2}}=\sum_{i=1}^{43} n_{i} \pi^{I_{i}} J_{i}\left(J_{i}-1\right)(\tau-0.5)^{J_{i}-2}
$$

## Parameters

tau [float] Dimensionless temperature, $(540 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

d2Gr_dtau2 [float] Second derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to tau, [-]

## Examples

```
>>> iapws97_d2Gr_dtau2_region2(540/300.0, 101325/1e6)
-470.9302933324787
```

chemicals.iapws.iapws97_d2Gr_dpidtau_region2 (tau, pi)
Calculates the second derivative of dimensionless residual Gibbs free energy with respect to tau and pi for water according to the IAPWS-97 standard (for region 2).

$$
\frac{\partial^{2} \gamma^{r}}{\partial \tau \partial \pi}=\sum_{i=1}^{43} n_{i} I_{i} \pi^{I_{i}-1} J_{i}(\tau-0.5)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, $(540 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

d2Gr_dpidtau_ [float] Second derivative of dimensionless residual Gibbs energy Gr/(RT) with respect to tau and pi, [-]

## Examples

```
>>> iapws97_d2Gr_dpidtau_region2(540/300.0, 101325/1e6)
-735.391845360247
```


### 1.13.9 IAPWS-97 Region 3

chemicals.iapws.iapws97_A_region3(tau, delta)
Calculates the dimensionless Helmholtz free energy for water according to the IAPWS-97 standard (for region $3)$.

$$
\frac{f(\rho, T)}{R T}=\phi(\delta, \tau)=n_{1} \ln \delta+\sum_{i=2}^{40} n_{i} \delta^{I_{i}} \tau^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/( $\left.322 \mathrm{~kg} / \mathrm{m}^{\wedge} 3\right),[-]$

## Returns

A [float] Helmholtz free energy A/(RT), [-]

## Examples

```
>>> iapws97_A_region3(647.096/500.0, 400.0/322.0)
-3.0336402168865
```

chemicals.iapws.iapws97_dA_ddelta_region3(tau, delta)
Calculates the derivative of dimensionless Helmholtz free energy with respect to delta for water according to the IAPWS-97 standard (for region 3).

$$
\frac{\partial \phi(\delta, \tau)}{\partial \delta}=\frac{n_{1}}{\delta}+\sum_{i=2}^{40} n_{i} I_{i} \delta^{I_{i}-1} \tau^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

dA_ddelta [float] Derivative of dimensionless Helmholtz free energy with respect to delta, [-]

## Examples

>>> iapws97_dA_ddelta_region3(647.096/500.0, 400.0/322.0)
7.35562435092
chemicals.iapws.iapws97_d2A_ddelta2_region3(tau, delta)
Calculates the second derivative of dimensionless Helmholtz free energy with respect to delta for water according to the IAPWS-97 standard (for region 3).

$$
\frac{\partial^{2} \phi(\delta, \tau)}{\partial \delta^{2}}=\frac{-n_{1}}{\delta^{2}}+\sum_{i=2}^{40} n_{i} I_{i}\left(I_{i}-1\right) \delta^{I_{i}-2} \tau^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2A_ddelta2 [float] Second derivative of dimensionless Helmholtz free energy with respect to delta, [-]

## Examples

>>> iapws97_d2A_ddelta2_region3(647.096/500.0, 400.0/322.0)
-2.2858869882497
chemicals.iapws.iapws97_dA_dtau_region3(tau, delta)
Calculates the derivative of dimensionless Helmholtz free energy with respect to tau for water according to the IAPWS-97 standard (for region 3).

$$
\frac{\partial \phi(\delta, \tau)}{\partial \tau}=+\sum_{i=2}^{40} n_{i} J_{i} \delta^{I_{i}} \tau^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

dA_dtau [float] Derivative of dimensionless Helmholtz free energy with respect to tau, [-]

## Examples

```
>>> iapws97_dA_dtau_region3(647.096/500.0, 400.0/322.0)
-24.9687028688
```

chemicals.iapws.iapws97_d2A_dtau2_region3(tau, delta)
Calculates the second derivative of dimensionless Helmholtz free energy with respect to tau for water according to the IAPWS-97 standard (for region 3).

$$
\frac{\partial^{2} \phi(\delta, \tau)}{\partial \tau^{2}}=+\sum_{i=2}^{40} n_{i} J_{i}\left(J_{i}-1\right) \delta^{I_{i}} \tau^{J_{i}-2}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2A_dtau2 [float] Second derivative of dimensionless Helmholtz free energy with respect to tau, [-]

## Examples

>>> iapws97_d2A_dtau2_region3(647.096/500.0, 400.0/322.0)
-373.6565823701

## chemicals.iapws.iapws97_d2A_ddeltadtau_region3(tau,delta)

Calculates the second derivative of dimensionless Helmholtz free energy with respect to tau and delta for water according to the IAPWS-97 standard (for region 3).

$$
\frac{\partial^{2} \phi(\delta, \tau)}{\partial \tau \partial \delta}=+\sum_{i=2}^{40} n_{i} J_{i} \delta^{I_{i}-1} \tau^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2A_ddeltadtau [float] Second derivative of dimensionless Helmholtz free energy with respect to tau and delta, [-]

## Examples

>>> iapws97_d2A_ddeltadtau_region3(647.096/500.0, 400.0/322.0)
145.85190014717

### 1.13.10 IAPWS-97 Region 3 PT Backwards Equation Boundaries

chemicals.iapws.iapws97_boundary_3uv ( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3uv(22.3E6)
647.7996121480069
chemicals.iapws.iapws97_boundary_3ef( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3ef(40E6)
713.959399239744
chemicals.iapws.iapws97_boundary_3cd $(P)$
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3cd(25E6)
649.3659208321279
chemicals.iapws.iapws97_boundary_3gh( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3gh(25E6)
656.69805722612
chemicals.iapws.iapws97_boundary_3ij ( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3ij(25E6)
660.7865756716819
chemicals.iapws.iapws97_boundary_3jk ( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3jk(25E6)
668.1915358826951
chemicals.iapws.iapws97_boundary_3mn ( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3mn(22.8E6)
649.6054132953997
chemicals.iapws.iapws97_boundary_3qu( $P$ )
Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3qu(22E6)
645.6355027340121

## chemicals.iapws.iapws97_boundary_3rx ( $P$ )

Calculates the transition temperature for a region 3 PT backwards equation transition.

## Parameters

$\mathbf{P}$ [float] Pressure [Pa]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3rx(22E6)
648.26227536701
chemicals.iapws.iapws97_boundary_3wx (logP_MPa, logP_MPa_inv)
Calculates the transition temperature for a region 3 PT backwards equation transition (for one of "wx", "ab", or "op"; the others do not use a log fit). The parameters are provided in the specific units for speed savings only.

## Parameters

$\log \mathbf{P}$ _MPa [float] Natural logarithm of pressure in units of MPa [log(MPa)]
$\log \mathbf{P}$ _MPa_inv [float] Inverse of Natural logarithm of pressure in units of $\mathrm{MPa}[1 / \log (\mathrm{MPa})$ ]

## Returns

T_trans [float] Transition temperature [K]

## Examples

```
>>> iapws97_boundary_3wx(log(22.3), 1/log(22.3))
```

648.204947950734
chemicals.iapws.iapws97_boundary_3ab ( $\log P$ _ $\left.M P a, \log P \_M P a \_i n v\right)$
Calculates the transition temperature for a region 3 PT backwards equation transition (for one of "wx", "ab", or "op"; the others do not use a log fit). The parameters are provided in the specific units for speed savings only.

## Parameters

$\log \mathbf{P}$ _MPa [float] Natural logarithm of pressure in units of MPa [log(MPa)]
$\operatorname{logP}$ _MPa_inv [float] Inverse of Natural logarithm of pressure in units of MPa [1/log(MPa)]

## Returns

T_trans [float] Transition temperature [K]

## Examples

>>> iapws97_boundary_3ab(log(40), 1/log(40))
693.0341408296053
chemicals.iapws.iapws97_boundary_3op(logP_MPa, logP_MPa_inv)
Calculates the transition temperature for a region 3 PT backwards equation transition (for one of "wx", "ab", or "op"; the others do not use a log fit). The parameters are provided in the specific units for speed savings only.

## Parameters

$\log \mathbf{P}$ _MPa [float] Natural logarithm of pressure in units of MPa [log(MPa)]
$\log \mathbf{P}$ _MPa_inv [float] Inverse of Natural logarithm of pressure in units of MPa [1/log(MPa)]

## Returns

T_trans [float] Transition temperature [K]

## Examples

```
>>> iapws97_boundary_3op(log(22.8), 1/log(22.8))
650.010694314133
```


### 1.13.11 IAPWS-97 Region 3 PT Backwards Equations

```
chemicals.iapws.iapws97_region3_a(T, P)
```

Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_b $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_c ( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right.$ ]

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_d $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

$\mathbf{T}$ [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_e ( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_f( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_g $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_h $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_i $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right.$ ]

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_j $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_k $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_1 $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_m $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_n $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_o ( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right.$ ]

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_p $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_q $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_r $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_s $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_t ( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_u ( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right.$ ]

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_v $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_w ( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_x $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_y $(T, P)$
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS-97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.
chemicals.iapws.iapws97_region3_z( $T, P$ )
Calculate the mass density water in one of the 26 region 3 backwards regions of the IAPWS- 97 standard.

## Parameters

T [float] Temperature, [K]
$\mathbf{P}$ [float] Pressure, [Pa]

## Returns

rho [float] Mass density of water in region $3,\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]$

## Notes

Significant discontinuities exist between each region. These functions are automatically generated and are not to be edited directly.

### 1.13.12 IAPWS-97 Region 5

chemicals.iapws.iapws97_G0_region5(tau, pi)
Calculates the dimensionless ideal gas Gibbs free energy for water according to the IAPWS-97 standard (for region 5).

$$
\gamma^{\circ}=\ln \pi+\sum_{i=1}^{6} n_{i}^{\circ} \tau^{J_{i}^{\circ}}
$$

## Parameters

tau [float] Dimensionless temperature, (1000 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

G0 [float] Dimensionless ideal gas Gibbs energy G/(RT), [-]

## Examples

>>> iapws97_G0_region5(1000.0/1500, 101325/1e6)
-14.9741430290056
chemicals.iapws.iapws97_dG0_dtau_region5(tau, pi)
Calculates the first derivative of dimensionless ideal gas Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial \gamma^{\circ}}{\partial \tau}=\sum_{i=1}^{6} n_{i}^{\circ} J_{i}^{\circ} \tau^{J_{i}^{\circ}-1}
$$

## Parameters

tau [float] Dimensionless temperature, $(1000 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

dG0_dtau [float] First derivative of dimensionless ideal gas Gibbs energy G/(RT) with respect to tau, [-]

## Notes

This function does not depend on pi but it is accepted for consistency.

## Examples

>>> iapws97_dG0_dtau_region5(1000.0/1500, 101325/1e6)
11.311766995978
chemicals.iapws.iapws97_d2G0_dtau2_region5(tau, pi)
Calculates the second derivative of dimensionless ideal gas Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial^{2} \gamma^{\circ}}{\partial \tau^{2}}=\sum_{i=1}^{6} n_{i}^{\circ} J_{i}^{\circ}\left(J_{i}^{\circ}-1\right) \tau^{J_{i}^{\circ}-2}
$$

## Parameters

tau [float] Dimensionless temperature, (1000 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

d2G0_dtau2 [float] Second derivative of dimensionless ideal gas Gibbs energy G/(RT) with respect to tau, [-]

## Notes

This function does not depend on pi but it is accepted for consistency.

## Examples

```
>>> iapws97_d2G0_dtau2_region5(1000.0/1500, 101325/1e6)
-12.744650271463655
```

chemicals.iapws.iapws97_Gr_region5 (tau, pi)
Calculates the dimensionless residual Gibbs free energy for water according to the IAPWS-97 standard (for region 5).

$$
\gamma^{r}=\sum_{i=1}^{6} n_{i} \pi^{I_{i}}(\tau)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (1000 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

Gr [float] Dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT}),[-]$

## Examples

>>> iapws97_Gr_region5 (1000/300.0, 101325/1e6)
-0.0194648291645718

## chemicals.iapws.iapws97_dGr_dpi_region5(tau, pi)

Calculates the first derivative of dimensionless residual Gibbs free energy with respect to $p i$ for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial \gamma^{r}}{\partial \pi}=\sum_{i=1}^{6} n_{i} I_{i} \pi^{I_{i}-1}(\tau)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, (1000 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

dGr_dpi [float] Derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to $p i$, [-]

## Notes

Used in density solution.

## Examples

```
>>> iapws97_dGr_dpi_region5(1000/300.0, 101325/1e6)
    -0.213281155629998
```

chemicals.iapws.iapws97_d2Gr_dpi2_region5(tau, pi)
Calculates the second derivative of dimensionless residual Gibbs free energy with respect to $p i$ for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial^{2} \gamma^{r}}{\partial \pi^{2}}=\sum_{i=1}^{6} n_{i} I_{i}\left(I_{i}-1\right) \pi^{I_{i}-2}(\tau)^{J_{i}}
$$

## Parameters

tau [float] Dimensionless temperature, ( 540 K )/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa})$, [-]

## Returns

d2Gr_dpi2 [float] Second derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to $p i$, [-]

## Examples

>>> iapws97_d2Gr_dpi2_region5(1000/300.0, 101325/1e6)
-0.4179905782304291

## chemicals.iapws.iapws97_dGr_dtau_region5(tau, pi)

Calculates the first derivative of dimensionless residual Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial \gamma^{r}}{\partial \tau}=\sum_{i=1}^{6} n_{i} \pi^{I_{i}} J_{i}(\tau)^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, (1000 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}$ ), [-]

## Returns

dGr_dtau [float] Derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to tau, [-]

## Examples

```
>>> iapws97_dGr_dtau_region5(1000/300.0, 101325/1e6)
-0.02200629869194
```

chemicals.iapws.iapws97_d2Gr_dtau2_region5(tau, pi)
Calculates the second derivative of dimensionless residual Gibbs free energy with respect to tau for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial^{2} \gamma^{r}}{\partial \tau^{2}}=\sum_{i=1}^{6} n_{i} \pi^{I_{i}} J_{i}\left(J_{i}-1\right)(\tau)^{J_{i}-2}
$$

## Parameters

tau [float] Dimensionless temperature, (1000 K)/T [-]
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

d2Gr_dtau2 [float] Second derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to tau, [-]

## Examples

```
>>> iapws97_d2Gr_dtau2_region5(1000/300.0, 101325/1e6)
-0.0239165867999155
```

chemicals.iapws.iapws97_d2Gr_dpidtau_region5(tau, pi)
Calculates the second derivative of dimensionless residual Gibbs free energy with respect to tau and pi for water according to the IAPWS-97 standard (for region 5).

$$
\frac{\partial^{2} \gamma^{r}}{\partial \tau \partial \pi}=\sum_{i=1}^{6} n_{i} I_{i} \pi^{I_{i}-1} J_{i}(\tau)^{J_{i}-1}
$$

## Parameters

tau [float] Dimensionless temperature, $(1000 \mathrm{~K}) / \mathrm{T}[-]$
pi [float] Dimensionless pressure, $\mathrm{P} /(1 \mathrm{MPa}),[-]$

## Returns

d2Gr_dpidtau [float] Second derivative of dimensionless residual Gibbs energy $\mathrm{Gr} /(\mathrm{RT})$ with respect to tau and pi, [-]

## Examples

```
>>> iapws97_d2Gr_dpidtau_region5(1000/300.0, 101325/1e6)
-0.27438379131103097
```


### 1.13.13 IAPWS-95 Ideal Gas Terms

## chemicals.iapws.iapws95_AO (tau, delta)

Calculates the ideal gas Helmholtz energy of water according to the IAPWS-95 standard.

$$
\phi^{\circ}=\ln \delta+n_{1}+n_{2} \tau+n_{3} \ln \tau+\sum_{i=4}^{8} n_{i} \ln \left[1-\exp \left(-\gamma_{i} \tau\right)\right]
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

A0 [float] Ideal gas dimensionless Helmholtz energy A/(RT) [-]

## Notes

This implementation is checked to have a relative error always under $1 \mathrm{e}-15$.

## Examples

>>> iapws95_A0(647.096/300.0, 999.0/322)
9.537075529761053
chemicals.iapws.iapws95_dAO_dtau(tau, delta)
Calculates the first derivative of ideal gas Helmholtz energy of water with respect to tau according to the IAPWS95 standard.

$$
\frac{\partial \phi^{\circ}}{\partial \tau}=n_{2}+\frac{n_{3}}{\tau}+\sum_{i=4}^{8} n_{i} \gamma_{i}\left[\left(1-\exp \left(-\gamma_{i} \tau\right)\right)^{-1}-1\right]
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

dA0_dtau [float] First derivative of ideal gas dimensionless Helmholtz energy A/(RT) with respect to tau [-]

## Notes

This implementation is checked to have a relative error always under $1 \mathrm{e}-15$.

## Examples

>>> iapws95_dA0_dtau(647.096/300.0, 999.0/322)
8.079705548882

## chemicals.iapws.iapws95_d2AO_dtau2(tau, delta)

Calculates the second derivative of ideal gas Helmholtz energy of water with respect to tau according to the IAPWS-95 standard.

$$
\frac{\partial^{2} \phi^{\circ}}{\partial \tau^{2}}=\frac{n_{3}}{\tau^{2}}+\sum_{i=4}^{8} n_{i} \gamma_{i}^{2} \exp \left(-\gamma_{i} \tau\right)\left[\left(1-\exp \left(-\gamma_{i} \tau\right)\right)^{-2}\right]
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2A0_dtau2 [float] Second derivative of ideal gas dimensionless Helmholtz energy A/(RT) with respect to tau [-]

## Notes

This implementation is checked to have a relative error always under 1e-15.

## Examples

>>> iapws95_d2AQ_dtau2(647.096/300.0, 999.0/322)
-0.653543047751809

## chemicals.iapws.iapws95_d3AQ_dtau3(tau, delta)

Calculates the third derivative of ideal gas Helmholtz energy of water with respect to tau according to the IAPWS95 standard.

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d3A0_dtau3 [float] Third derivative of ideal gas dimensionless Helmholtz energy A/(RT) with respect to tau [-]

## Notes

This implementation is checked to have a relative error always under $1 \mathrm{e}-15$. This equation is not explicitly in IAPWS-95, but is needed to compute some second derivatives.

## Examples

>>> iapws95_d3A0_dtau3(647.096/300.0, 999.0/322)
0.6222542507278

## chemicals.iapws.iapws95_AO_tau_derivatives(tau,delta)

Calculates the ideal gas Helmholtz energy of water and its first three derivatives with respect to tau according to the IAPWS-95 standard. As each of those calls spends most of their time computing exponentials which are the same for each function, function offers a time saving.

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/( $\left.322 \mathrm{~kg} / \mathrm{m}^{\wedge} 3\right),[-]$

## Returns

A0 [float] Ideal gas dimensionless Helmholtz energy A/(RT) [-]
dA0_dtau [float] First derivative of ideal gas dimensionless Helmholtz energy A/(RT) with respect to tau [-]
d2A0_dtau2 [float] Second derivative of ideal gas dimensionless Helmholtz energy A/(RT) with respect to tau [-]
d3A0_dtau3 [float] Third derivative of ideal gas dimensionless Helmholtz energy A/(RT) with respect to tau [-]

## Notes

The extra cost of calling this function vs iapws95_A0 alone is $\sim 15 \%$ with numba, $\sim 40 \%$ with PyPy, and $120 \%$ with CPython.

## Examples

>>> iapws95_A0_tau_derivatives(647.096/300.0, 999.0/322)
( $9.53707552976,8.0797055488,-0.65354304775,0.62225425072$ )

### 1.13.14 IAPWS-95 Residual Terms

## chemicals.iapws.iapws95_Ar(tau, delta)

Calculates the residual Helmholtz energy of water according to the IAPWS-95 standard.

$$
\begin{gathered}
\phi^{\mathrm{r}}=\sum_{i=1}^{7} n_{i} \delta^{d_{i}} \tau^{t_{i}}+\sum_{i=8}^{51} n_{i} \delta^{d_{i}} \tau^{t_{i}} \mathrm{e}^{-\delta^{c_{i}}}+\sum_{i=52}^{54} n_{i} \delta^{d_{i}} \tau^{t_{i}} \mathrm{e}^{-\alpha_{i}\left(\delta-\varepsilon_{i}\right)^{2}-\beta_{i}\left(\tau-\gamma_{i}\right)^{2}}+\sum_{i=55}^{56} n_{i} \Delta^{b_{i}} \delta \psi \\
\Delta=\theta^{2}+B_{i}\left[(\delta-1)^{2}\right]^{a_{i}}
\end{gathered}
$$

$$
\begin{gathered}
\theta=(1-\tau)+A_{i}\left[(\delta-1)^{2}\right]^{\frac{1}{2 \beta_{i}}} \\
\psi=e^{-C_{i}(\delta-1)^{2}-D_{i}(\tau-1)^{2}}
\end{gathered}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

Ar [float] Residual Helmholtz energy A/(RT) [-]

## Notes

This is an optimized implementatation taking 9 exp calls, 4 sqrts, and 3 powers. It was generated using SymPy's CSE functionality, with select polynomial optimizations by hand as well. It is over 10x faster than a naive implementation.

This implementation has been tested against a straightforward implementation with the equations given in IAPWS-95.

Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3$, 4 E 6 points were evaluated. The mean relative error was $5.0416 \mathrm{E}-15$, with a maximum relative error of $1.118 \mathrm{E}-9$ and a standard deviation of $5.773 \mathrm{e}-13$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 90000 points, the mean relative error was $3.14 \mathrm{E}-15$, with a maximum relative error of $3.54 \mathrm{e}-12$ and a standard deviation of $3.017 \mathrm{E}-14$.

This comparison indicates that this implementation is more accurate than the straightforward implementation.

## Examples

```
>>> iapws95_Ar(647.096/300.0, 999.0/322)
-9.57577716026768
```

chemicals.iapws.iapws95_dAr_ddelta(tau, delta)
Calculates the first derivative of residual Helmholtz energy of water with respect to delta according to the IAPWS95 standard.
$\phi_{\delta}^{\mathrm{r}}=\sum_{i=1}^{7} n_{i} d_{i} \delta^{d_{i}-1} \tau^{t_{i}}+\sum_{i=8}^{51} n_{i} \mathrm{e}^{-\delta^{c_{i}}}\left[\delta^{d_{i}-1} \tau^{t_{i}}\left(d_{i}-c_{i} \delta^{c_{i}}\right)\right]+\sum_{i=52}^{54} n_{i} \delta^{d_{i}} \tau^{t_{i}} \mathrm{e}^{-\alpha_{i}\left(\delta-\varepsilon_{i}\right)^{2}-\beta_{i}\left(\tau-\gamma_{i}\right)^{2}}\left[\frac{d_{i}}{\delta}-2 \alpha_{i}\left(\delta-\varepsilon_{i}\right)\right]+\sum_{i=55}^{56}$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

dAr_ddelta [float] First derivative of residual Helmholtz energy A/(RT) with respect to delta, [-]

## Notes

This is an optimized implementatation taking 8 exp calls, 4 sqrts, and 2 powers. It was generated using SymPy’s CSE functionality, with select polynomial optimizations by hand as well. It is over 10x faster than a naive implementation.
This implementation has been tested against a straightforward implementation with the equations given in IAPWS-95.

Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3$, 4E6 points were evaluated. The mean relative error was $4.033 \mathrm{E}-15$, with a maximum relative error of $3.8765 \mathrm{e}-10$ and a standard deviation of $3.189 \mathrm{e}-13$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 90000 points, the mean relative error was $6.046 \mathrm{E}-15$, with a maximum relative error of $3.39 \mathrm{E}-10$ and a standard deviation of $7.056 \mathrm{E}-13$.

There was a singularity at $\operatorname{tau}=d e l t a=1$, but the limit is correctly returned.

## Examples

```
>>> iapws95_dAr_ddelta(647.096/300.0, 999.0/322)
```

-0. 3093321202374

## chemicals.iapws.iapws95_d2Ar_ddelta2(tau, delta)

Calculates the second derivative of residual Helmholtz energy of water with respect to delta according to the IAPWS-95 standard.

$$
\begin{aligned}
\phi_{\delta \delta}^{\mathrm{r}}= & \sum_{i=1}^{7} n_{i} d_{i}\left(d_{i}-1\right) \delta^{d_{i}-2} \tau^{t_{i}}+\sum_{i=8}^{51} n_{i} \mathrm{e}^{-\delta^{6}}\left[\delta^{d_{i}-2} \tau^{t_{i}}\left(\left(d_{i}-c_{i} \delta^{c_{i}}\right)\left(d_{i}-1-c_{i} \delta^{c_{i}}\right)-c_{i}^{2} \delta^{c_{i}}\right)\right]+\sum_{i=52}^{54} n_{i} \tau^{t_{i}} \mathrm{e}^{-\alpha_{i}\left(\delta-\varepsilon_{i}\right)^{2}-\beta_{i}(\tau-} \\
& \cdot\left[-2 \alpha_{i} \delta^{d_{i}}+4 \alpha_{i}^{2} \delta^{d_{i}}\left(\delta-\varepsilon_{i}\right)^{2}-4 d_{i} \alpha_{i} \delta^{d_{i}-1}\left(\delta-\varepsilon_{i}\right)+d_{i}\left(d_{i}-1\right) \delta^{d_{i}-2}\right]+\sum_{i=55}^{56} n_{i}\left[\Delta^{b_{i}}\left(2 \frac{\partial \psi}{\partial \delta}+\delta \frac{\partial^{2} \psi}{\partial \delta^{2}}\right)+2 \frac{\partial \Delta^{b_{i}}}{\partial \delta}\right.
\end{aligned}
$$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2Ar_ddelta2 [float] Second derivative of residual Helmholtz energy A/(RT) with respect to delta, [-]

## Notes

This is an optimized implementatation taking 4 exp calls, 4 sqrts, and 2 powers. It was generated using SymPy's CSE functionality, with select polynomial optimizations by hand as well. It is over 10x faster than a naive implementation.

This implementation has been tested against a straightforward implementation with the equations given in IAPWS-95.

Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3$, 4E6 points were evaluated. The mean relative error was $9.566 \mathrm{e}-16$, with a maximum relative error of $1.0518 \mathrm{E}-10$ and a standard deviation of $6.20265 \mathrm{E}-14$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 250000 points, the mean relative error was $1.039 \mathrm{E}-15$, with a maximum relative error of $2.431 \mathrm{E}-11$ and a standard deviation of $5.31708 \mathrm{E}-14$.

## Examples

>>> iapws95_d2Ar_ddelta2(647.096/300.0, 999.0/322)
1.7862535141735987

## chemicals.iapws.iapws95_d3Ar_ddelta3(tau, delta)

Calculates the third derivative of residual Helmholtz energy of water with respect to delta according to the IAPWS-95 standard.

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/( $\left.322 \mathrm{~kg} / \mathrm{m}^{\wedge} 3\right),[-]$

## Returns

d3Ar_ddelta3 [float] Third derivative of residual Helmholtz energy A/(RT) with respect to delta, [-]

## Notes

No equation is given for this in IAPWS-95, and the derivative was symbolically computed with SymPy.
This is an optimized implementatation. It was generated using SymPy's CSE functionality.
Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-4 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3,90000$ points were evaluated. The mean relative error was $5.41 \mathrm{E}-13$, with a maximum relative error of $6.3957 \mathrm{e}-11$ and a standard deviation of 3.346e-12.

90000 points were also evaluated with mpmath. The mean relative error was $1.41959 \mathrm{E}-14$, with a maximum relative error of $5.8878 \mathrm{E}-10$ and a standard deviation of $1.978 \mathrm{E}-12$.

Evaluating 10000 points in the $1 \mathrm{e}-10$ to $1 \mathrm{e}-4$ range, the mean relative error was $1.2 \mathrm{E}-16$, maximum relative error $1.2 \mathrm{e}-16$, and standard deviation $6.66 \mathrm{e}-16$.

## Examples

```
>>> iapws95_d3Ar_ddelta3(647.096/300.0, 999.0/322)
0.33621190578
```

chemicals.iapws.iapws95_dAr_dtau(tau, delta)
Calculates the first derivative of residual Helmholtz energy of water with respect to tau according to the IAPWS95 standard.
$\phi_{\tau}^{\mathrm{r}}=\sum_{i=1}^{7} n_{i} t_{i} \delta^{d_{i}} \tau^{t_{i}-1}+\sum_{i=8}^{51} n_{i} t_{i} \delta^{d_{i}} \tau^{t_{i}-1} \mathrm{e}^{-\delta^{c_{i}}}+\sum_{i=52}^{54} n_{i} \delta^{d_{i}} \tau^{t_{i}} \mathrm{e}^{-\alpha_{i}\left(\delta-\varepsilon_{i}\right)^{2}-\beta_{i}\left(\tau-\gamma_{i}\right)^{2}}\left[\frac{t_{i}}{\tau}-2 \beta_{i}\left(\tau-\gamma_{i}\right)\right]+\sum_{i=55}^{56} n_{i} \delta\left[\frac{\partial \Delta^{b_{i}}}{\partial \tau} \psi\right.$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

dAr_dtau [float] Derivative of residual Helmholtz energy A/(RT) with respect to tau, [-]

## Notes

This is an optimized implementatation taking 9 exp calls, 4 sqrts, and 2 powers. It was generated using SymPy's CSE functionality, with a limited amount of horner polynomial optimizations as well. It is over 10x faster than a naive implementation.
This implementation has been tested against a straightforward implementation with the equations given in IAPWS-95.

Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3,250000$ points were evaluated. The mean relative error was $5.68 \mathrm{E}-14$, with a maximum relative error of $6.73 \mathrm{E}-9$ and a standard deviation of $1.35 \mathrm{E}-11$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 90000 points, the mean relative error was $4.66 \mathrm{E}-14$, with a maximum relative error of $4.25 \mathrm{E}-10$ and a standard deviation of $1.77 \mathrm{E}-12$.

The maximum error ocurs in the extremely low density regime, $\rho<1 e-6$.

## Examples

>>> iapws95_dAr_dtau(647.096/300.0, 999.0/322)
-7.7043336309570
chemicals.iapws.iapws95_d2Ar_dtau2 (tau, delta)
Calculates the second derivative of residual Helmholtz energy of water with respect to tau according to the IAPWS-95 standard.
$\phi_{\tau \tau}^{\mathrm{r}}=\sum_{i=1}^{7} n_{i} t_{i}\left(t_{i}-1\right) \delta^{d_{i}} \tau^{t_{i}-2}+\sum_{i=8}^{51} n_{i} t_{i}\left(t_{i}-1\right) \delta^{d_{i}} \tau^{t_{i}-2} \mathrm{e}^{-\delta^{c_{i}}}+\sum_{i=52}^{54} n_{i} \delta^{d_{i}} \tau^{t_{i}} \mathrm{e}^{-\alpha_{i}\left(\delta-\varepsilon_{i}\right)^{2}-\beta_{i}\left(\tau-\gamma_{i}\right)^{2}}\left[\left(\frac{t_{i}}{\tau}-2 \beta_{i}\left(\tau-\gamma_{i}\right)\right)\right.$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2Ar_dtau2 [float] Second derivative of residual Helmholtz energy A/(RT) with respect to tau, [-]

## Notes

This is an optimized implementatation taking 9 exp calls, 4 sqrts, and 2 powers. It was generated using SymPy's CSE functionality, with a limited amount of horner polynomial optimizations as well. It is over 10x faster than a naive implementation.

This implementation has been tested against a straightforward implementation with the equations given in IAPWS-95.

Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3$, 4E6 points were evaluated. The mean relative error was $4.595 \mathrm{E}-16$, with a maximum relative error of $1.835 \mathrm{e}-10$ and a standard deviation of $1.209 \mathrm{E}-13$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 250000 points, the mean relative error was $2.6026 \mathrm{E}-16$, with a maximum relative error of $2.36 \mathrm{E}-12$ and a standard deviation of $8.055 \mathrm{E}-15$.

This comparison indicates this implementation is more accurate than the straightforward implementation.

## Examples

```
>>> iapws95_d2Ar_dtau2(647.096/300.0, 999.0/322)
-1.2616419775539
```


## chemicals.iapws.iapws95_d2Ar_ddeltadtau(tau, delta)

Calculates the second derivative of residual Helmholtz energy of water with respect to tau and also delta according to the IAPWS-95 standard.
$\phi_{\delta \tau}^{\mathrm{r}}=\sum_{i=1}^{7} n_{i} d_{i} t_{i} \delta^{d_{i}-1} \tau^{t_{i}-1}+\sum_{i=8}^{51} n_{i} t_{i} \delta^{d_{i}-1} \tau^{t_{i}-1}\left(d_{i}-c_{i} \delta^{c_{i}}\right) \mathrm{e}^{-\delta^{c_{i}}}+\sum_{i=52}^{54} n_{i} \delta^{d_{i}} \tau^{t_{i}} \mathrm{e}^{-\alpha_{i}\left(\delta-\varepsilon_{i}\right)^{2}-\beta_{i}\left(\tau-\gamma_{i}\right)^{2}}\left[\frac{d_{i}}{\delta}-2 \alpha_{i}\left(\delta-\varepsilon_{i}\right)\right]$

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d2Ar_ddeltadtau [float] Second derivative of residual Helmholtz energy A/(RT) with respect to tau and delta, [-]

## Notes

This is an optimized implementatation taking 11 exp calls, 4 sqrts, and 3 powers. It was generated using SymPy’s CSE functionality, with select polynomial optimizations by hand as well. It is over 10x faster than a naive implementation.

This implementation has been tested against a straightforward implementation with the equations given in IAPWS-95.

Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3$, 4E6 points were evaluated. The mean relative error was $2.82 \mathrm{E}-14$, with a maximum relative error of $8.404 \mathrm{E}-9$ and a standard deviation of $5.166 \mathrm{e}-12$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 90000 points, the mean relative error was $6.974 \mathrm{E}-14$, with a maximum relative error of $4.286 \mathrm{E}-9$ and a standard deviation of 4.286E-12.

## Examples

```
>>> iapws95_d2Ar_ddeltadtau(647.096/300.0, 999.0/322)
-0.198403562385
```

chemicals.iapws.iapws95_d3Ar_ddeltadtau2 (tau, delta)
Calculates the third derivative of residual Helmholtz energy of water with respect to delta once and tau twice according to the IAPWS-95 standard.

## Parameters

1.13. IAPWS: International Association for the Properties of Water and Steam (chemicals.iapws)81
tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d3Ar_ddeltadtau2 [float] Third derivative of residual Helmholtz energy A/(RT) with respect to delta once and tau twice, [-]

## Notes

This is an optimized implementatation. It was generated using SymPy's CSE functionality.
No equation is given for this in IAPWS-95, and the derivative was symbolically computed with SymPy.
Like many higher-order derivatives of functions with exponentials, this one balloons to use many, many terms.
Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3,250000$ points were evaluated. The mean relative error was $7.936 \mathrm{e}-16$, with a maximum relative error of $1.965 \mathrm{E}-11$ and a standard deviation of $4.7938 \mathrm{E}-14$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 90000 points, the mean relative error was $6.08 \mathrm{E}-16$, with a maximum relative error of $3.537 \mathrm{E}-12$ and a standard deviation of $1.85197 \mathrm{E}-14$.

## Examples

>>> iapws95_d3Ar_ddeltadtau2(647.096/300.0, 999.0/322)
1.081479970332
chemicals.iapws.iapws95_d3Ar_ddelta2dtau(tau, delta)
Calculates the third derivative of residual Helmholtz energy of water with respect to delta twice and tau one according to the IAPWS-95 standard.

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d3Ar_ddeltadtau2 [float] Third derivative of residual Helmholtz energy A/(RT) with respect to delta twice and tau once, [-]

## Notes

This is an optimized implementatation. It was generated using SymPy's CSE functionality.
No equation is given for this in IAPWS-95, and the derivative was symbolically computed with SymPy.
Like many higher-order derivatives of functions with exponentials, this one balloons to use many, many terms.
Over a linear temperature range of 200 K to 5000 K and a logarithmic density range of $1 \mathrm{E}-10 \mathrm{~kg} / \mathrm{m}^{\wedge} 3$ to 5000 $\mathrm{kg} / \mathrm{m}^{\wedge} 3,250000$ points were evaluated. The mean relative error was $3.629 \mathrm{e}-15$, with a maximum relative error of $8.38 \mathrm{E}-11$ and a standard deviation of $2.1214 \mathrm{E}-13$.

Over the same range, the model was evaluated to a precision of 50 decimal places with mpmath, and on 10000 points, the mean relative error was $2.4 \mathrm{e}-15$, with a maximum relative error of $7.62 \mathrm{E}-12$ and a standard deviation of $7.818 \mathrm{E}-14$.

## Examples

```
>>> iapws95_d3Ar_ddelta2dtau(647.096/300.0, 999.0/322)
```

0.015646982949077

## chemicals.iapws.iapws95_d4Ar_ddelta2dtau2(tau, delta)

Calculates the fourth derivative of residual Helmholtz energy of water with respect to tau twice and delta twice according to the IAPWS-95 standard.

## Parameters

tau [float] Dimensionless temperature, (647.096 K)/T [-]
delta [float] Dimensionless density, rho/(322 kg/m^3), [-]

## Returns

d4Ar_ddelta2dtau2 [float] Fourth derivative of residual Helmholtz energy A/(RT) with respect to tau and delta, [-]

## Examples

```
>>> iapws95_d4Ar_ddelta2dtau2(647.096/300.0, 999.0/322)
-2.656422915480
```


### 1.14 Chemical Metadata (chemicals.identifiers)

This module contains a database of metadata on $\sim 70000$ chemicals from the PubChem datase. It contains comprehensive feature for searching the metadata. It also includes a small database of common mixture compositions.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

- Search Functions
- CAS Number Utilities
- Database Objects
- Chemical Groups


### 1.14.1 Search Functions

## chemicals.identifiers.CAS_from_any (ID, autoload=False, cache=True)

Wrapper around search_chemical which returns the CAS number of the found chemical directly.

## Parameters

ID [str] One of the name formats described by search_chemical, [-]
autoload [bool, optional] Whether to load new chemical databanks during the search if a hit is not immediately found, [-]
cache [bool, optional] Whether or not to cache the search for faster lookup in subsequent queries, [-]

## Returns

CASRN [str] A three-piece, dash-separated set of numbers

## Notes

An exception is raised if the name cannot be identified. The PubChem database includes a wide variety of other synonyms, but these may not be present for all chemcials. See search_chemical for more details.

## Examples

```
>>> CAS_from_any('water')
    '7732-18-5'
    >>> CAS_from_any('InChI=1S/C2H60/c1-2-3/h3H,2H2,1H3')
    '64-17-5'
    >>> CAS_from_any(' CCCCCCCCCC')
    '124-18-5'
    >>> CAS_from_any ('InChIKey=LFQSCWFLJHTTHZ-UHFFFAOYSA-N')
    '64-17-5'
    >>> CAS_from_any('pubchem=702')
    '64-17-5'
    >>> CAS_from_any('0') # only elements can be specified by symbol
    '17778-80-2'
```

chemicals.identifiers.MW(ID, autoload=False, cache=True)
Wrapper around search_chemical which returns the molecular weight of the found chemical directly.

## Parameters

ID [str] One of the name formats described by search_chemical

## Returns

MW [float] Molecular weight of chemical, $[\mathrm{g} / \mathrm{mol}]$

## Notes

An exception is raised if the name cannot be identified. The PubChem database includes a wide variety of other synonyms, but these may not be present for all chemcials. See search_chemical for more details.

## Examples

```
>>> MW('water')
18.01528
>>> MW('InChI=1S/C2H60/c1-2-3/h3H, 2H2,1H3')
46.06844
>>> MW('CCCCCCCCCC')
142.286
>>> MW('InChIKey=LFQSCWFLJHTTHZ-UHFFFAOYSA-N')
46.06844
>>> MW('pubchem=702')
46.06844
```

>>> MW('O') \# only elements can be specified by symbol 15.9994
chemicals.identifiers.search_chemical(ID, autoload=False, cache=True)
Looks up metadata about a chemical by searching and testing for the input string being any of the following types of chemical identifiers:

- Name, in IUPAC form or common form or a synonym registered in PubChem
- InChI name, prefixed by 'InChI=1S/' or 'InChI=1/'
- InChI key, prefixed by 'InChIKey='
- PubChem CID, prefixed by 'PubChem='
- SMILES (prefix with 'SMILES=' to ensure smiles parsing; ex. ' $C$ ' will return Carbon as it is an element whereas the SMILES interpretation for ' C ' is methane)
- CAS number (obsolete numbers may point to the current number)

If the input is an ID representing an element, the following additional inputs may be specified as

- Atomic symbol (ex ‘Na')
- Atomic number (as a string)


## Parameters

ID [str] One of the name formats described above
autoload [bool, optional] Whether to load new chemical databanks during the search if a hit is not immediately found, [-]
cache [bool, optional] Whether or not to cache the search for faster lookup in subsequent queries, [-]

## Returns

chemical_metadata [ChemicalMetadata] A class containing attributes which describe the chemical's metadata, [-]

## Notes

An exception is raised if the name cannot be identified. The PubChem database includes a wide variety of other synonyms, but these may not be present for all chemcials.

## Examples

```
>>> search_chemical('water')
<ChemicalMetadata, name=water, formula=H2O, smiles=0, MW=18.0153>
>>> search_chemical('InChI=1S/C2H60/c1-2-3/h3H,2H2,1H3')
<ChemicalMetadata, name=ethanol, formula=C2H60, smiles=CCO, MW=46.0684>
>>> search_chemical('CCCCCCCCC'')
<ChemicalMetadata, name=DECANE, formula=C10H22, smiles=CCCCCCCCCC, MW=142.286>
>>> search_chemical('InChIKey=LFQSCWFLJHTTHZ-UHFFFAOYSA-N')
<ChemicalMetadata, name=ethanol, formula=C2H60, smiles=CCO, MW=46.0684>
>>> search_chemical('pubchem=702')
```

(continued from previous page)
<ChemicalMetadata, name=ethanol, formula=C2H60, smiles=CCO, MW=46.0684>
>>> search_chemical('0') \# only elements can be specified by symbol
<ChemicalMetadata, name=oxygen, formula=0, smiles=[0], MW=15.9994>
chemicals.identifiers.IDs_to_CASs(IDs)
Find the CAS numbers for multiple chemicals names at once. Also supports having a string input which is a common mixture name in the database. An error will be raised if any of the chemicals cannot be found.

## Parameters

IDs [list[str] or str] A string or 1-element list containing the name which may represent a mixture.

## Returns

CASs [list[str]] CAS numbers of found chemicals, [-]

## Notes

White space, '-', and upper case letters are removed in the search.

## Examples

>>> IDs_to_CASs('R512A')
['811-97-2', '75-37-6']
>>> IDs_to_CASs(['norflurane', '1,1-difluoroethane'])
['811-97-2', '75-37-6']

### 1.14.2 CAS Number Utilities

## chemicals.identifiers.check_CAS (CASRN)

Checks if a CAS number is valid. Returns False if the parser cannot parse the given string.

## Parameters

CASRN [str] A three-piece, dash-separated set of numbers

## Returns

result [bool] Boolean value if CASRN was valid. If parsing fails, return False also.

## Notes

Check method is according to Chemical Abstract Society. However, no lookup to their service is performed; therefore, this function cannot detect false positives.
Function also does not support additional separators, apart from '-'.
CAS numbers up to the series 1 XXX XXX-XX-X are now being issued.
A long can hold CAS numbers up to 2147 483-64-7

## Examples

>>> check_CAS('7732-18-5')
True
>>> check_CAS('77332-18-5')
False
chemicals.identifiers.CAS_to_int( $i$ )
Converts CAS number of a compounds from a string to an int. This is helpful when storing large amounts of CAS numbers, as their strings take up more memory than their numerical representational. All CAS numbers fit into 64 bit ints.

## Parameters

CASRN [str] CASRN [-]

## Returns

CASRN [int] CASRN [-]

## Notes

Accomplishes conversion by removing dashes only, and then converting to an int. An incorrect CAS number will change without exception.

## Examples

>>> CAS_to_int('7704-34-9')
7704349
chemicals.identifiers.int_to_CAS ( $i$ )
Converts CAS number of a compounds from an int to an string. This is helpful when dealing with int CAS numbers.

## Parameters

CASRN [int] CASRN [-]

## Returns

CASRN [str] CASRN [-]

## Notes

Handles CAS numbers with an unspecified number of digits. Does not work on floats.

## Examples

>>> int_to_CAS(7704349)
'7704-34-9'

## chemicals.identifiers.sorted_CAS_key(CASs)

Takes a list of CAS numbers as strings, and returns a tuple of the same CAS numbers, sorted from smallest to largest. This is very convenient for obtaining a unique hash of a set of compounds, so as to see if two groups of compounds are the same.

## Parameters

CASs [list[str]] CAS numbers as strings [-]

## Returns

CASs_sorted [tuple[str]] Sorted CAS numbers from lowest (first) to highest (last) [-]

## Notes

Does not check CAS numbers for validity.

## Examples

```
>>> sorted_CAS_key(['7732-18-5', '64-17-5', '108-88-3', '98-00-0'])
('64-17-5', '98-00-0', '108-88-3', '7732-18-5')
```


### 1.14.3 Database Objects

There is an object used to represent a chemical's metadata, an object used to represent a common mixture's composition, and an object used to hold the mixture metadata.

```
class chemicals.identifiers.ChemicalMetadata(pubchemid, CAS, formula, MW, smiles,InChI,InChI_key,
``` iupac_name, common_name, synonyms)
Class for storing metadata on chemicals.

\section*{Attributes}
pubchemid [int] Identification number on pubchem database; access their information online at https://pubchem.ncbi.nlm.nih.gov/compound/<pubchemid> [-]
formula [str] Formula of the compound; in the same format as chemicals.elements. serialize_formula generates, [-]

MW [float] Molecular weight of the compound as calculated with the standard atomic abundances; consistent with the element weights in chemicals.elements.periodic_table, [ \(\mathrm{g} / \mathrm{mol}\) ]
smiles [str] SMILES identification string, [-]
InChI [str] InChI identification string as given in pubchem (there can be multiple valid InChI strings for a compound), [-]
InChI_key [str] InChI key identification string (meant to be unique to a compound), [-]
iupac_name [str] IUPAC name as given in pubchem, [-]
common_name [str] Common name as given in pubchem, [-]
synonyms [list[str]] List of synonyms of the compound, [-]
CAS [int] CAS number of the compound; stored as an int for memory efficiency, [-]
class chemicals.identifiers.CommonMixtureMetadata(name, CASs, \(N\), source, names, ws, zs, synonyms)
Class for storing metadata on predefined chemical mixtures.

\section*{Attributes}
name [str] Name of the mixture, [-]
source [str] Source of the mixture composition, [-]
\(\mathbf{N}\) [int] Number of chemicals in the mixture, [-]
CASs [list[str]] CAS numbers of the mixture, [-]
ws [list[float]] Mass fractions of chemicals in the mixture, [-]
zs [list[float]] Mole fractions of chemicals in the mixture, [-]
names [list[str]] List of names of the chemicals in the mixture, [-]
synonyms [list[str]] List of synonyms of the mixture which can also be used to look it up, [-]
class chemicals.identifiers.ChemicalMetadataDB(elements=True,
main_db='/home/docs/checkouts/readthedocs.org/user_builds/chemicals/e
packages/chemicals-1.1.4-
py3.7.egg/chemicals/Identifiers/chemical identifiers
pubchem large.tsv',
user_dbs=['/home/docs/checkouts/readthedocs.org/user_builds/chemicals
packages/chemicals-1.1.4-
py3.7.egg/chemicals/Identifiers/chemical identifiers
pubchem small.tsv',
'/home/docs/checkouts/readthedocs.org/user_builds/chemicals/envs/stable
packages/chemicals-1.1.4-
py3.7.egg/chemicals/Identifiers/chemical identifiers
example user db.tsv',
'/home/docs/checkouts/readthedocs.org/user_builds/chemicals/envs/stable
packages/chemicals-1.1.4-
py3.7.egg/chemicals/Identifiers/Cation db.tsv',
'/home/docs/checkouts/readthedocs.org/user_builds/chemicals/envs/stable
packages/chemicals-1.1.4-
py3.7.egg/chemicals/Identifiers/Anion db.tsv',
'/home/docs/checkouts/readthedocs.org/user_builds/chemicals/envs/stable
packages/chemicals-1.1.4-
py3.7.egg/chemicals/Identifiers/Inorganic
db.tsv'])
Object which holds the main database of chemical metadata.

Warning: To allow the chemicals to grow and improve, the details of this class may change in the future without notice!

\section*{Attributes}
finished_loading Whether or not the database has loaded the main database.

Methods
\begin{tabular}{ll}
\hline autoload_main_db() & Load the main database when needed. \\
\hline finish_loading() & \begin{tabular}{l} 
Complete loading the main database, if it has not \\
been fully loaded.
\end{tabular} \\
\hline load(file_name) & Load a particular file into the indexes. \\
\hline load_elements() & Load elements into the indexes. \\
\hline search_CAS(CAS[, autoload]) & Search for a chemical by its CAS number. \\
\hline search_InChI(InChI[, autoload]) & Search for a chemical by its InChI string. \\
\hline search_InChI_key(InChI_key[, autoload]) & Search for a chemical by its InChI key. \\
\hline search_formula(formula[, autoload]) & Search for a chemical by its serialized formula. \\
\hline search_name(name[, autoload]) & Search for a chemical by its name. \\
\hline search_pubchem(pubchem[, autoload]) & Search for a chemical by its pubchem number. \\
\hline search_smiles(smiles[, autoload]) & Search for a chemical by its smiles string. \\
\hline
\end{tabular}
chemicals.identifiers.get_pubchem_db()
Helper function to delay the creation of the pubchem_db object.
This avoids loading the database when it is not needed.

\subsection*{1.14.4 Chemical Groups}

It is convenient to tag some chemicals with labels like "refrigerant", or in a certain database or not. The following chemical groups are available.
```

chemicals.identifiers.cryogenics = {'132259-10-0': 'Air', '1333-74-0': 'hydrogen',
'630-08-0': 'carbon monoxide', '74-82-8': 'methane', '7439-90-9': 'krypton', '7440-01-9':
'neon', '7440-37-1': 'Argon', '7440-59-7': 'helium', '7440-63-3': 'xenon', '7727-37-9':
'nitrogen', '7782-39-0': 'deuterium', '7782-41-4': 'fluorine', '7782-44-7': 'oxygen'}
chemicals.identifiers.inerts = {'10043-92-2': 'radon', '10102-43-9': 'Nitric Oxide',
'10102-44-0': 'Nitrogen Dioxide', '124-38-9': 'Carbon Dioxide', '132259-10-0': 'Air',
'7439-90-9': 'krypton', '7440-01-9': 'Neon', '7440-37-1': 'Argon', '7440-59-7': 'Helium',
'7440-63-3': 'Xenon', '7727-37-9': 'Nitrogen', '7732-18-5': 'water', '7782-41-4':
'fluorine', '7782-44-7': 'Oxygen', '7782-50-5': 'chlorine'}
chemicals.identifiers.dippr_compounds()
Loads and returns a set of compounds known in the DIPPR database. This can be useful for knowing if a chemical is of industrial relevance.

```

\section*{Returns}
dippr_compounds [set([str])] A set of CAS numbers from the 2014 edition of the DIPPR database.

\subsection*{1.15 Surface Tension (chemicals.interface)}

This module contains various surface tension estimation routines, dataframes of fit coefficients, fitting model equations, mixing rules, and water-hydrocarbon interfacial tension estimation routines.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Pure Component Correlations
- Mixing Rules
- Correlations for Specific Substances
- Petroleum Correlations
- Oil-Water Interfacial Tension Correlations
- Fit Correlations
- Fit Coefficients

\subsection*{1.15.1 Pure Component Correlations}

\section*{chemicals.interface.Brock_Bird ( \(T, T b, T c, P c\) )}

Calculates air-liquid surface tension using the [1] emperical method. Old and tested.
\[
\begin{gathered}
\sigma=P_{c}^{2 / 3} T_{c}^{1 / 3} Q\left(1-T_{r}\right)^{11 / 9} \\
Q=0.1196\left[1+\frac{T_{b r} \ln \left(P_{c} / 1.01325\right)}{1-T_{b r}}\right]-0.279
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

Numerous arrangements of this equation are available. This is DIPPR Procedure 7A: Method for the Surface Tension of Pure, Nonpolar, Nonhydrocarbon Liquids The exact equation is not in the original paper. If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}
p-dichloribenzene at 412.15 K , from DIPPR; value differs due to a slight difference in method.
>>> Brock_Bird(412.15, 447.3, 685, 3.952E6)
0.02208448325192495

Chlorobenzene from Poling, as compared with a \% error value at 293 K .
>>> Brock_Bird(293.15, 404.75, 633.0, 4530000.0)
0.032985686413713036
chemicals.interface.Pitzer_sigma ( \(T, T c, P c\), omega)
Calculates air-liquid surface tension using the correlation derived by [1] from the works of [2] and [3]. Based on critical property CSP methods.
\[
\sigma=P_{c}^{2 / 3} T_{c}^{1 / 3} \frac{1.86+1.18 \omega}{19.05}\left[\frac{3.75+0.91 \omega}{0.291-0.08 \omega}\right]^{2 / 3}\left(1-T_{r}\right)^{11 / 9}
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

The source of this equation has not been reviewed. Internal units of presure are bar, surface tension of \(\mathrm{mN} / \mathrm{m}\). If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1], [2], [3]

\section*{Examples}

Chlorobenzene from Poling, as compared with a \% error value at 293 K .
>>> Pitzer_sigma(293., 633.0, 4530000.0, 0.249)
0.03458453513446388

\section*{chemicals.interface.Sastri_Rao( \(T, T b, T c, P c\), chemicaltype=None)}

Calculates air-liquid surface tension using the correlation derived by [1] based on critical property CSP methods and chemical classes.
\[
\sigma=K P_{c}^{x} T_{b}^{y} T_{c}^{z}\left[\frac{1-T_{r}}{1-T_{b r}}\right]^{m}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

The source of this equation has not been reviewed. Internal units of presure are bar, surface tension of \(\mathrm{mN} / \mathrm{m}\). If Tc is larger than T, 0 is returned as the model would return complex numbers.

\section*{References}

\section*{[1]}

\section*{Examples}

Chlorobenzene from Poling, as compared with a \% error value at 293 K .
>>> Sastri_Rao(293.15, 404.75, 633.0, 4530000.0)
0.03234567739694441
chemicals.interface.Zuo_Stenby ( \(T, T c, P c\), omega)
Calculates air-liquid surface tension using the reference fluids methods of [1].
\[
\begin{gathered}
\sigma^{(1)}=40.520\left(1-T_{r}\right)^{1.287} \\
\sigma^{(2)}=52.095\left(1-T_{r}\right)^{1.21548} \\
\sigma_{r}=\sigma_{r}^{(1)}+\frac{\omega-\omega^{(1)}}{\omega^{(2)}-\omega^{(1)}}\left(\sigma_{r}^{(2)}-\sigma_{r}^{(1)}\right) \\
\sigma=T_{c}^{1 / 3} P_{c}^{2 / 3}\left[\exp \left(\sigma_{r}\right)-1\right]
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

Presently untested. Have not personally checked the sources. The reference values for methane and n-octane are from the DIPPR database. If Tc is larger than T, 0 is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

Chlorobenzene
>> Zuo_Stenby(293., 633.0, 4530000.0, 0.249)
0.03345569011871088
chemicals.interface.Hakim_Steinberg_Stiel(T,Tc, Pc, omega, StielPolar=0.0)
Calculates air-liquid surface tension using the reference fluids methods of [1].
\[
\begin{gathered}
\sigma=4.60104 \times 10^{-7} P_{c}^{2 / 3} T_{c}^{1 / 3} Q_{p}\left(\frac{1-T_{r}}{0.4}\right)^{m} \\
Q_{p}=0.1574+0.359 \omega-1.769 \chi-13.69 \chi^{2}-0.51 \omega^{2}+1.298 \omega \chi \\
m=1.21+0.5385 \omega-14.61 \chi-32.07 \chi^{2}-1.65 \omega^{2}+22.03 \omega \chi
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor for fluid, [-]
StielPolar [float, optional] Stiel Polar Factor, [-]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

Original equation for m and Q are used. Internal units are atm and \(\mathrm{mN} / \mathrm{m}\). If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

1-butanol, as compared to value in CRC Handbook of 0.02493 .
>>> Hakim_Steinberg_Stiel(298.15, 563.0, 4414000.0, 0.59, StielPolar=-0.07872)
0.02190790257519
chemicals.interface. Miqueu ( \(T, T c, V c\), omega)
Calculates air-liquid surface tension using the methods of [1].
\[
\sigma=k T_{c}\left(\frac{N_{a}}{V_{c}}\right)^{2 / 3}(4.35+4.14 \omega) t^{1.26}\left(1+0.19 t^{0.5}-0.487 t\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

Uses Avogadro's constant and the Boltsman constant. Internal units of volume are \(\mathrm{mL} / \mathrm{mol}\) and \(\mathrm{mN} / \mathrm{m}\). However, either a typo is in the article or author's work, or my value of \(k\) is off by 10 ; this is corrected nonetheless. Created with 31 normal fluids, none polar or hydrogen bonded. Has an AARD of \(3.5 \%\). If Tc is larger than T, 0 is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

Bromotrifluoromethane, \(2.45 \mathrm{mN} / \mathrm{m}\)
>>> Miqueu(300., 340.1, 0.000199, 0.1687)
0.003474100774091376

\section*{chemicals.interface.Aleem ( \(T, M W, T b, r h o l, H v a p \_T b, C p l\) )}

Calculates vapor-liquid surface tension using the correlation derived by [1] based on critical property CSP methods.
\[
\begin{aligned}
\sigma & =\phi \frac{M W^{1 / 3}}{6 N_{A}^{1 / 3}} \rho_{l}^{2 / 3}\left[H_{v a p}+C_{p, l}\left(T_{b}-T\right)\right] \\
\phi & =1-0.0047 M W+6.8 \times 10^{-6} M W^{2}
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
MW [float] Molecular weight [ \(\mathrm{g} / \mathrm{mol}\) ]
Tb [float] Boiling temperature of the fluid [K]
rhol [float] Liquid density at \(T\) and \(P\left[k g / \mathrm{m}^{\wedge} 3\right.\) ]
Hvap_Tb [float] Mass enthalpy of vaporization at the normal boiling point [kg/m^3]
Cpl [float] Liquid heat capacity of the chemical at T [J/kg/K]

\section*{Returns}
sigma [float] Liquid-vapor surface tension [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

Internal units of molecuar weight are \(\mathrm{kg} / \mathrm{mol}\). This model is dimensionally consistent.
This model does not use the critical temperature. After it predicts a surface tension of 0 at a sufficiently high temperature, it returns negative results. The temperature at which this occurs (the "predicted" critical temperature) can be calculated as follows:
\[
\sigma=0 \rightarrow T_{c, \text { predicted }} \text { at } T_{b}+\frac{H_{v a p}}{C p_{l}}
\]

To handle this case, if Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.
Because of its dependence on density, it has the potential to model the effect of pressure on surface tension.
Claims AAD of 4.3\%. Developed for normal alkanes. Total of 472 data points. Behaves worse for higher alkanes. Behaves very poorly overall.

\section*{References}
[1]

\section*{Examples}

Methane at 90 K
>>> Aleem( \(\mathrm{T}=90\), \(\mathrm{MW}=16.04246, \mathrm{~Tb}=111.6\), \(\mathrm{rhol}=458.7\), Hvap_Tb=510870.,
... Cpl=2465.)
0.01669970230131523
chemicals.interface.Mersmann_Kind_sigma( \(T, T m, T b, T c, P c, n \_\)associated=1)
Estimates the surface tension of organic liquid substances according to the method of [1].
\[
\begin{gathered}
\sigma^{*}=\frac{\sigma n_{a s s}^{1 / 3}}{\left(k T_{c}\right)^{1 / 3} T_{r m} P_{c}^{2 / 3}} \\
\sigma^{*}=\left(\frac{T_{b}-T_{m}}{T_{m}}\right)^{1 / 3}\left[6.25\left(1-T_{r}\right)+31.3\left(1-T_{r}\right)^{4 / 3}\right]
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
Tm [float] Melting temperature [K]
Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
n_associated [float] Number of associated molecules in a cluster (2 for alcohols, 1 otherwise), [-]

\section*{Returns}
sigma [float] Liquid-vapor surface tension [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

In the equation, all quantities must be in SI units. \(k\) is the boltzman constant. If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

MTBE at STP (the actual value is 0.0181 ):
>>> Mersmann_Kind_sigma(298.15, 164.15, 328.25, 497.1, 3430000.0)
0.016744311449290426
chemicals.interface.sigma_Gharagheizi_1 (T, Tc, MW,omega)
Calculates air-liquid surface tension using the equation 4 derived in [1] by gene expression programming.
\[
\begin{gathered}
\sigma=8.948226 \times 10^{-4}\left[\frac{A^{2}}{M W} \sqrt{\frac{A \omega}{M W}}\right]^{0.5} \\
A=\left(T_{c}-T-\omega\right)
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
MW [float] Molecular weight [ \(\mathrm{g} / \mathrm{mol}\) ]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

This equation may fail before the critical point. In this case it returns 0.0 If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}

\section*{[1]}

\section*{Examples}

Methane at 93 K , point from [1]'s supporting material:
```

>>> sigma_Gharagheizi_1(T=95, Tc=190.564, MW=16.04, omega=0.012)
0.0110389739

```
chemicals.interface.sigma_Gharagheizi_2 \((T, T b, T c, P c, V c)\)
Calculates air-liquid surface tension using the equation 6 derived in [1] by gene expression programming.
\[
\frac{\sigma}{\mathrm{N} / \mathrm{m}}=10^{-4}\left(\frac{P_{c}}{\mathrm{bar}}\right)^{2 / 3}\left(\frac{T_{c}}{\mathrm{~K}}\right)^{1 / 3}\left(1-T_{r}\right)^{11 / 9}\left[7.728729 T_{b r}+2.476318\left(T_{b r}^{3}+\frac{V_{c}}{\mathrm{~m}^{3} / \mathrm{kmol}}\right)\right]
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tb [float] Boiling temperature of the fluid [K]

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
MW [float] Molecular weight \([\mathrm{g} / \mathrm{mol}\) ]
Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

This expression gives does converge to 0 at the critical point. If Tc is larger than T, 0 is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

Methane at 93 K , point from [1]'s supporting material:
>>> sigma_Gharagheizi_2 ( \(\mathrm{T}=95, \mathrm{~Tb}=111.66, \mathrm{Tc}=190.564, \mathrm{Pc}=45.99 \mathrm{e} 5, \mathrm{Vc}=0.0986 \mathrm{e}-3)\) 0.01674894057

\subsection*{1.15.2 Mixing Rules}

\section*{chemicals.interface.Winterfeld_Scriven_Davis(xs, sigmas, rhoms)}

Calculates surface tension of a liquid mixture according to mixing rules in [1] and also in [2].
\[
\sigma_{M}=\sum_{i} \sum_{j} \frac{1}{V_{L}^{L 2}}\left(x_{i} V_{i}\right)\left(x_{j} V_{j}\right) \sqrt{\sigma_{i} \cdot \sigma_{j}}
\]

\section*{Parameters}
\(\mathbf{x s}\) [array-like] Mole fractions of all components, [-]
sigmas [array-like] Surface tensions of all components, [N/m]
rhoms [array-like] Molar densities of all components, \(\left[\mathrm{mol} / \mathrm{m}^{\wedge} 3\right]\)

\section*{Returns}
sigma [float] Air-liquid surface tension of mixture, [N/m]

\section*{Notes}

DIPPR Procedure 7C: Method for the Surface Tension of Nonaqueous Liquid Mixtures
Becomes less accurate as liquid-liquid critical solution temperature is approached. DIPPR Evaluation: 3-4\% AARD, from 107 nonaqueous binary systems, 1284 points. Internally, densities are converted to \(\mathrm{kmol} / \mathrm{m}^{\wedge} 3\). The Amgat function is used to obtain liquid mixture density in this equation.
Raises a ZeroDivisionError if either molar volume are zero, and a ValueError if a surface tensions of a pure component is negative.

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Winterfeld_Scriven_Davis([0.1606, 0.8394], [0.01547, 0.02877],
... [8610., 15530.])
0.02496738845043982

```
chemicals.interface. Weinaug_Katz (parachors, Vml, Vmg, xs, ys)
Calculates surface tension of a liquid mixture according to mixing rules in [1] and also in [2]. This is based on the Parachor concept. This is called the Macleod-Sugden model in some places.
\[
\sigma_{M}=\left[\sum_{i} P_{i}\left(\frac{x_{i}}{V_{m, l}}-\frac{y_{i}}{V_{m, g}}\right)\right]^{4}
\]

\section*{Parameters}
parachors [list[float]] Parachors of each component, [ \(\mathrm{N}^{\wedge} 0.25 * \mathrm{~m}^{\wedge} 2.75 / \mathrm{mol}\) ]
Vml [float] Liquid mixture molar volume, [m^3/mol]
Vmg [float] Gas mixture molar volume; this can be set to zero at low pressures, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
xs [list[float]] Mole fractions of all components in liquid phase, [-]
xs [list[float]] Mole fractions of all components in gas phase, [-]

\section*{Returns}
sigma [float] Air-liquid surface tension of mixture, [N/m]

\section*{Notes}

This expression is efficient and does not require pure component surface tensions. Its accuracy is dubious.

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Weinaug_Katz([5.1e-5, 7.2e-5], Vml=0.000125, Vmg=0.02011, xs=[.4, .6], ys=[.6, .
๑4])
0.06547479150776776

```

Neglect the vapor phase density by setting Vmg to a high value:
>> Weinaug_Katz([5.1e-5, 7.2e-5], Vml=0.000125, Vmg=1e100, xs=[.4, .6], ys=[.6, .
\(\rightarrow 4]\) )
0.06701752894095361
chemicals.interface.Diguilio_Teja(T, xs, sigmas_Tb,Tbs, Tcs)
Calculates surface tension of a liquid mixture according to mixing rules in [1].
\[
\begin{gathered}
\sigma=1.002855\left(T^{*}\right)^{1.118091} \frac{T}{T_{b}} \sigma_{r} \\
T^{*}=\frac{\left(T_{c} / T\right)-1}{\left(T_{c} / T_{b}\right)-1} \\
\sigma_{r}=\sum x_{i} \sigma_{i} \\
T_{b}=\sum x_{i} T_{b, i} \\
T_{c}=\sum x_{i} T_{c, i}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
xs [array-like] Mole fractions of all components
sigmas_Tb [array-like] Surface tensions of all components at the boiling point, [N/m]
Tbs [array-like] Boiling temperatures of all components, [K]
Tcs [array-like] Critical temperatures of all components, [K]

\section*{Returns}
sigma [float] Air-liquid surface tension of mixture, \([\mathrm{N} / \mathrm{m}]\)

\section*{Notes}

Simple model, however it has 0 citations. Gives similar results to the Winterfeld_Scriven_Davis model.
Raises a ValueError if temperature is greater than the mixture's critical temperature or if the given temperature is negative, or if the mixture's boiling temperature is higher than its critical temperature.
[1] claims a 4.63 percent average absolute error on 21 binary and 4 ternary non-aqueous systems. [1] also considered Van der Waals mixing rules for \(T c\), but found it provided a higher error of 5.58\%

\section*{References}
[1]

Examples
>>> Diguilio_Teja(T=298.15, xs=[0.1606, 0.8394],
... sigmas_Tb=[0.01424, 0.02530], Tbs=[309.21, 312.95], Tcs=[469.7, 508.0])
0.025716823875045505

\subsection*{1.15.3 Correlations for Specific Substances}
chemicals.interface.sigma_IAPWS ( \(T\) )
Calculate the surface tension of pure water as a function of . temperature. Assumes the 2011 IAPWS [1] formulation.
\[
\begin{gathered}
\sigma=B \tau^{\mu}(1+b \tau) \\
\tau=1-T / T_{c} \\
B=0.2358 \mathrm{~N} / \mathrm{m} \\
b=-0.625 \\
\mu=1.256
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of liquid [K]

\section*{Returns}
sigma [float] Air-liquid surface tension, [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

This function is valid from the triple temperature to the critical temperature. No effects for pressure are included in the formulation. Test values are from IAPWS 2010 book.

The equation is valid from the triple point to the critical point, 647.096 K ; but [1] also recommends its use down to \(-25^{\circ} \mathrm{C}\).

If a value larger than the critical temperature is input, 0.0 is returned.

\section*{References}
[1]

\section*{Examples}
```

>>> sigma_IAPWS(300.)
0.0716859625271
>>> sigma_IAPWS(450.)
0.0428914991565
>>> sigma_IAPWS(600.)
0.0083756108728

```

\subsection*{1.15.4 Petroleum Correlations}
chemicals.interface.API10A32 ( \(T, T c, K_{-} W\) )
Calculates the interfacial tension between a liquid petroleum fraction and air, using the oil's pseudocritical temperature and Watson K Characterization factor.
\[
\sigma=\frac{673.7\left[\frac{\left(T_{c}-T\right)}{T_{c}}\right]^{1.232}}{K_{W}}
\]

\section*{Parameters}

T [float] Liquid temperature, [K]
Tc [float] Pseudocritical temperature (or critical temperature if using the equation with a pure component), [K]
\(\mathbf{K}\) _W [float] Watson characterization factor

\section*{Returns}
sigma [float] Air-liquid surface tension, [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}
[1] cautions that this should not be applied to coal liquids, and that it will give higher errors at pressures above 500 psi . [1] claims this has an average error of \(10.7 \%\).

This function converges to zero at \(T c\). If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

Sample problem in Comments on Procedure 10A3.2.1 of [1];
```

>>> from fluids.core import F2K, R2K
>>> API10A32(T=F2K(60), Tc=R2K(1334), K_W=12.4)
29.577333312096968

```

\subsection*{1.15.5 Oil-Water Interfacial Tension Correlations}

\section*{chemicals.interface.Meybodi_Daryasafar_Karimi (rho_water, rho_oil, T, Tc)}

Calculates the interfacial tension between water and a hydrocabon liquid according to the correlation of [1].
\[
\gamma_{h w}=\left(\frac{A_{1}+A_{2} \Delta \rho+A_{3} \Delta \rho^{2}+A_{4} \Delta \rho^{3}}{A_{5}+A_{6} \frac{T^{A_{7}}}{T_{c, h}}+A_{8} T^{A_{9}}}\right)^{A_{10}}
\]

\section*{Parameters}
rho_water [float] The density of the aqueous phase, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]\)
rho_oil [float] The density of the hydrocarbon phase, [kg/m^3]
\(\mathbf{T}\) [float] Temperature of the fluid, [K]
Tc [float] Critical temperature of the hydrocarbon mixture, [K]

\section*{Returns}
sigma [float] Hydrocarbon-water surface tension [N/m]

\section*{Notes}

Internal units of the equation are \(\mathrm{g} / \mathrm{mL}\) and \(\mathrm{mN} / \mathrm{m}\).

\section*{References}
[1]

\section*{Examples}
```

>>> Meybodi_Daryasafar_Karimi(980, 760, 580, 914)

```
0.02893598143089256

\subsection*{1.15.6 Fit Correlations}
chemicals.interface.REFPROP_sigma ( \(T, T c\), sigma0, \(n 0\), sigmal \(=0.0, n 1=0.0\), sigma \(2=0.0, n 2=0.0\) )
Calculates air-liquid surface tension using the REFPROP_sigma [1] regression-based method. Relatively recent, and most accurate.
\[
\sigma(T)=\sigma_{0}\left(1-\frac{T}{T_{c}}\right)^{n_{0}}+\sigma_{1}\left(1-\frac{T}{T_{c}}\right)^{n_{1}}+\sigma_{2}\left(1-\frac{T}{T_{c}}\right)^{n_{2}}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
sigma0 [float] First emperical coefficient of a fluid
n0 [float] First emperical exponent of a fluid
sigma1 [float, optional] Second emperical coefficient of a fluid.
n1 [float, optional] Second emperical exponent of a fluid.
sigma1 [float, optional] Third emperical coefficient of a fluid.
n2 [float, optional] Third emperical exponent of a fluid.

\section*{Returns}
sigma [float] Liquid surface tension, [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

Function as implemented in [1]. No example necessary; results match literature values perfectly. Form of function returns imaginary results when \(\mathrm{T}>\mathrm{Tc} ; 0\) is returned if this is the case.

When fitting parameters to this function, it is easy to end up with a fit that returns negative surface tension near but not quite at the critical point.

\section*{References}
[1]

\section*{Examples}

Parameters for water at 298.15 K
>> REFPROP_sigma(298.15, 647.096, -0.1306, 2.471, 0.2151, 1.233)
0.07205503890847453
chemicals.interface. Somayajulu ( \(T, T c, A, B, C\) )
Calculates air-liquid surface tension using the [1] emperical (parameter-regressed) method. Well regressed, no recent data.
\[
\begin{gathered}
\sigma=a X^{5 / 4}+b X^{9 / 4}+c X^{13 / 4} \\
X=\left(T_{c}-T\right) / T_{c}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
A [float] Regression parameter
B [float] Regression parameter
C [float] Regression parameter

\section*{Returns}
sigma [float] Liquid surface tension, \(\mathrm{N} / \mathrm{m}\)

\section*{Notes}

Presently untested, but matches expected values. Internal units are \(\mathrm{mN} / \mathrm{m}\). Form of function returns imaginary results when \(\mathrm{T}>\mathrm{Tc}\); 0.0 is returned if this is the case. Function is claimed valid from the triple to the critical point. Results can be evaluated beneath the triple point.
This function can be accidentally fit to return negative values of surface tension.

\section*{References}

\section*{[1]}

\section*{Examples}

Water at 300 K
```

>>> Somayajulu(300, 647.126, 232.713514, -140.18645, -4.890098)

```
0.07166386387996758
chemicals.interface.Jasper \((T, a, b)\)
Calculates surface tension of a fluid given two parameters, a linear fit in Celcius from [1] with data reprinted in [2].
\[
\sigma=a-b T
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
a [float] Parameter for equation. Chemical specific.
b [float] Parameter for equation. Chemical specific.

\section*{Returns}
sigma [float] Surface tension [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

Internal units are \(\mathrm{mN} / \mathrm{m}\), and degrees Celcius. This function has been checked against several references.
As this is a linear model, negative values of surface tension will eventually arise. 0 is returned in these cases.

\section*{References}
[1], [2]

\section*{Examples}
>>> Jasper (298.15, 24, 0.0773)
0.0220675
chemicals.interface.PPDS14 ( \(T, T c, a 0, a 1, a 2\) )
Calculates air-liquid surface tension using the [1] emperical (parameter-regressed) method, called the PPDS 14 equation for surface tension.
\[
\sigma=a_{0} \tau^{a_{1}}\left(1+a_{2} \tau\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
a0 [float] Regression parameter, [N/m]
a1 [float] Regression parameter, [-]
\(\mathbf{a} 2\) [float] Regression parameter, [-]

\section*{Returns}
sigma [float] Liquid surface tension, [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

If Tc is larger than T, 0 is returned as the model would return complex numbers.
If this model is fit with \(a 0\) and \(a 2\) as positive values, it is guaranteed to predict only positive values of sigma right up to the critical point. However, \(a 2\) is often fit to be a negative value.

\section*{References}
[1], [2]

\section*{Examples}

Benzene at 280 K from [1]
>> PPDS14 (T=280, Tc=562.05, \(\mathrm{a} 0=0.0786269, \mathrm{a} 1=1.28646, \mathrm{a} 2=-0.112304)\)
0.030559764256249854
chemicals.interface.Watson_sigma \((T, T c, a 1, a 2, a 3=0.0, a 4=0.0, a 5=0.0)\)
Calculates air-liquid surface tension using the Watson [1] emperical (parameter-regressed) method developed by NIST.
\[
\sigma=\exp \left[a_{1}+\ln \left(1-T_{r}\right)\left(a_{2}+a_{3} T_{r}+a_{4} T_{r}^{2}+a_{5} T_{r}^{3}\right)\right]
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
a1 [float] Regression parameter, [-]
a2 [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]
a5 [float] Regression parameter, [-]

\section*{Returns}
sigma [float] Liquid surface tension, [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

This expression is also used for enthalpy of vaporization in [1]. The coefficients from NIST TDE for enthalpy of vaporization are \(\mathrm{kJ} / \mathrm{mol}\).

This model is coded to return 0 values at \(\mathrm{Tr}>=1\). It is otherwise not possible to evaluate this expression at \(\mathrm{Tr}=\) 1 , as \(\log (0)\) is undefined (although the limit shows the expression converges to 0 ).
This equation does not have any term forcing it to become near-zero at the critical point, but it cannot be fit so as to produce negative values.

\section*{References}
[1]

\section*{Examples}

Isooctane at 350 K from [1]:
```

>>> Watson_sigma(T=350.0, Tc=543.836, a1=-3.02417, a2=1.21792, a3=-5.26877e-9, a4=5.
๑62659e-9, a5=-2.27553e-9)
0.0138340926605649

```
chemicals.interface.ISTExpansion ( \(T, T c, a 1, a 2, a 3=0.0, a 4=0.0, a 5=0.0\) )
Calculates air-liquid surface tension using the IST expansion [1] emperical (parameter-regressed) method developed by NIST.
\[
\sigma=\sum_{i} a_{i}\left(1-\frac{T}{T_{c}}\right)^{i}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
a1 [float] Regression parameter, [-]
\(\mathbf{a} 2\) [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]
a5 [float] Regression parameter, [-]

\section*{Returns}
sigma [float] Liquid surface tension, [ \(\mathrm{N} / \mathrm{m}\) ]

\section*{Notes}

This equation hsa a term term forcing it to become zero at the critical point, but it can easily be fit so as to produce negative values at any reduced temperature.

\section*{References}
[1]

\section*{Examples}

Diethyl phthalate at 400 K from [1]:
```

>> ISTExpansion(T=400.0, Tc=776.0, a1=0.037545, a2=0.0363288)
0.02672100905515996

```

\subsection*{1.15.7 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.interface.sigma_data_Mulero_Cachadina
Data from [5] with REFPROP_sigma coefficients.
chemicals.interface.sigma_data_Jasper_Lange
Data as shown in [4] but originally in [3] with Jasper coefficients.
chemicals.interface.sigma_data_Somayajulu
Data from [1] with Somayajulu coefficients.
chemicals.interface.sigma_data_Somayajulu2
Data from [2] with Somayajulu coefficients. These should be preferred over the original coefficients.
chemicals.interface.sigma_data_VDI_PPDS_11
Data from [6] with chemicals.dippr.EQ106 coefficients.
The structure of each dataframe is shown below:
```

In [1]: import chemicals
In [2]: chemicals.interface.sigma_data_Mulero_Cachadina
Out[2]:
CAS
Fluid ... Tmax
60-29-7
64-17-5
67-56-1
67-64-1
71-43-2 Benzene ... 553.15
7783-54, %...............
7783-54-2 Nitrogen trifluoride ... 206.36
7789-20-0 D20 ... 642.02
10024-97-2 Nitrous oxide ... 293.15
22410-44-2 RE245cb2 (Methyl-pentafluoroethyl ether) ... 353.41
29118-24-9 R1234ze(E) (trans-1,3,3,3-tetrafluoropropene) ... 373.14

```
[115 rows x 10 columns]
In [3]: chemicals.interface.sigma_data_Jasper_Lange
Out[3]:
\begin{tabular}{lrrrrr} 
& Name & a & b & Tmin & Tmax \\
CAS & & & & & \\
\(55-21-0\) & Benzamide & 47.26 & 0.0705 & 402.15 & 563.15 \\
\(55-63-0\) & Glycerol tris(nitrate) & 55.74 & 0.2504 & 286.15 & 433.15 \\
\(56-23-5\) & Carbon tetrachloride & 29.49 & 0.1224 & 250.15 & 349.85 \\
\(57-06-7\) & Allyl isothiocyanate & 36.76 & 0.1074 & 193.15 & 425.15 \\
\(60-29-7\) & Diethyl ether & 18.92 & 0.0908 & 157.15 & 307.75 \\
\(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) \\
\(13952-84-6\) & sec-Butylamine & 23.75 & 0.1057 & 169.15 & 336.15 \\
\(14901-07-6\) & -Ionone & 35.36 & 0.0950 & 401.15 & 401.15 \\
\(18854-56-3\) & 1,2-Dipropoxyethane & 25.03 & 0.0972 & NaN & NaN \\
\(19550-30-2\) & 2,3-Dimethyl-1-butanol & 26.22 & 0.0992 & 259.15 & 391.15 \\
\(40626-78-6\) & 2-Methylhexane & 21.22 & 0.0966 & 155.15 & 363.15
\end{tabular}
[522 rows x 5 columns]
In [4]: chemicals.interface.sigma_data_Somayajulu
Out[4]:
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline & Chemical & Tt & Tc & A & B & C \\
\hline \multicolumn{7}{|l|}{CAS} \\
\hline 60-29-7 & Ethyl ether & 157.00 & 466.74 & 61.0417 & -6.7908 & 0.14046 \\
\hline 64-17-5 & Ethanol & 159.00 & 513.92 & 111.4452 & -146.0229 & 89.57030 \\
\hline 64-19-7 & Acetic acid & 290.00 & 592.70 & 91.9020 & -91.7035 & 77.50720 \\
\hline 67-56-1 & Methanol & 175.59 & 512.64 & 122.6257 & -199.4044 & 153.37440 \\
\hline 71-23-8 & Propanaol & 147.00 & 536.78 & 107.1238 & -133.8128 & 84.43570 \\
\hline & & & & & & \\
\hline 10035-10-6 & Hydrogen bromide & 187.15 & 363.20 & 74.0521 & 20.1043 & -30.25710 \\
\hline 10102-43-9 & Nitric oxide & 112.15 & 180.00 & 58.6304 & 97.8722 & -33.67390 \\
\hline 13465-07-1 & Hydrogen disulfide & 185.15 & 572.00 & 130.1176 & -40.6216 & 4.77160 \\
\hline 17778-80-2 & Oxygen & 54.35 & 154.58 & 38.2261 & 5.6316 & -7.74050 \\
\hline 19287-45-7 & Diborane & 104.15 & 289.80 & 38.0417 & 29.7743 & -24.26050 \\
\hline \multicolumn{7}{|l|}{[64 rows x 6 columns]} \\
\hline \multicolumn{7}{|l|}{In [5]: chemicals.interface.sigma_data_Somayajulu2} \\
\hline \multicolumn{7}{|l|}{Out[5]:} \\
\hline & Chemical & Tt & Tc & A & B & C \\
\hline \multicolumn{7}{|l|}{CAS} \\
\hline 60-29-7 & Ethyl ether & 157.00 & 466.74 & 61.0417 & -6.7908 & 0.14046 \\
\hline 64-17-5 & Ethanol & 159.00 & 513.92 & 111.4452 & -146.0229 & 89.57030 \\
\hline 64-19-7 & Acetic acid & 290.00 & 592.70 & 91.9020 & -91.7035 & 77.50720 \\
\hline 67-56-1 & Methanol & 175.59 & 512.64 & 122.6257 & -199.4044 & 153.37440 \\
\hline 71-23-8 & Propanaol & 147.00 & 536.78 & 107.1238 & -133.8128 & 84.43570 \\
\hline & & & & & & \\
\hline 10035-10-6 & Hydrogen bromide & 187.15 & 363.20 & 74.0521 & 20.1043 & -30.25710 \\
\hline 10102-43-9 & Nitric oxide & 112.15 & 180.00 & 58.6304 & 97.8722 & -33.67390 \\
\hline 13465-07-1 & Hydrogen disulfide & 185.15 & 572.00 & 150.6970 & -102.9100 & 56.72580 \\
\hline
\end{tabular}


\subsection*{1.16 Lennard-Jones Models (chemicals.lennard_jones)}

This module contains lookup functions and estimation methods for the parameters molecular diameter sigma and the Stockmayer parameter epsilon. These are used for diffusivity calculations. It also contains several methods for computing the collision integral, another parameter used in the Lennard-Jones model.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Stockmayer Parameter
- Stockmayer Parameter Correlations
- Molecular Diameter
- Molecular Diameter Correlations
- Utility Functions

\subsection*{1.16.1 Stockmayer Parameter}
chemicals.lennard_jones.Stockmayer (CASRN=", Tm=None, \(T b=N o n e, T c=N o n e, Z c=N o n e\), omega=None, method=None)
This function handles the retrieval or calculation a chemical's Stockmayer parameter. Values are available from one source with lookup based on CASRNs, or can be estimated from 7 CSP methods. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Preferred sources are 'Magalhães, Lito, Da Silva, and Silva (2013)' for common chemicals which had valies listed in that source, and the CSP method Tee, Gotoh, and Stewart CSP with Tc, omega (1966) for chemicals
which don't.

\section*{Parameters}

CASRN [str, optional] CASRN [-]
Tm [float, optional] Melting temperature of compound [K]
Tb [float, optional] Boiling temperature of compound [K]
Tc [float, optional] Critical temperature of compound, [K]
Zc [float, optional] Critical compressibility of compound, [-]
omega [float, optional] Acentric factor of compound, [-]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over k, [K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in Stockmayer_all_methods

\section*{Notes}

These values are somewhat rough, as they attempt to pigeonhole a chemical into L-J behavior.
The tabulated data is from [2], for 322 chemicals.

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Stockmayer(CASRN='64-17-5')
1291.41
>>> Stockmayer('7727-37-9')
71.4

```
chemicals.lennard_jones.Stockmayer_methods(CASRN=None, \(T m=N o n e, T b=N o n e, T c=N o n e, Z c=N o n e\), omega=None)
Return all methods available to obtain the Stockmayer parameter for the desired chemical.

\section*{Parameters}

CASRN [str, optional] CASRN [-]
Tm [float, optional] Melting temperature of compound [K]
Tb [float, optional] Boiling temperature of compound [K]
Tc [float, optional] Critical temperature of compound, [K]
Zc [float, optional] Critical compressibility of compound, [-]
omega [float, optional] Acentric factor of compound, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain Stockmayer with the given inputs.
See also:

\section*{Stockmayer}
chemicals.lennard_jones.Stockmayer_all_methods = ('Magalhães, Lito, Da Silva, and Silva (2013)', 'Poling et al. (2001)', 'Tee, Gotoh, and Stewart CSP with Tc, omega (1966)', 'Stiel and Thodos Tc, Zc (1962)', 'Flynn (1960)', 'Bird, Stewart, and Light (2002) critical relation', 'Tee, Gotoh, and Stewart CSP with Tc (1966)', 'Bird, Stewart, and Light (2002) boiling relation', 'Bird, Stewart, and Light (2002) melting relation')

Tuple of method name keys. See the Stockmayer for the actual references

\subsection*{1.16.2 Stockmayer Parameter Correlations}
chemicals.lennard_jones.epsilon_Flynn(Tc)
Calculates Lennard-Jones depth of potential-energy minimum. Uses critical temperature. CSP method by [1] as reported in [2].
\[
\epsilon / k=1.77 T_{c}^{5 / 6}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over \(k,[K]\)

\section*{References}
[1], [2]

\section*{Examples}
```

>>> epsilon_Flynn(560.1)

```
345.2984087011443
chemicals.lennard_jones.epsilon_Bird_Stewart_Lightfoot_critical(Tc)
Calculates Lennard-Jones depth of potential-energy minimum. Uses critical temperature. CSP method by [1].
\[
\epsilon / k=0.77 T_{c}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over k, [K]

\section*{References}
[1]

\section*{Examples}
>>> epsilon_Bird_Stewart_Lightfoot_critical(560.1)
431.27700000000004
chemicals.lennard_jones.epsilon_Bird_Stewart_Lightfoot_boiling(Tb)
Calculates Lennard-Jones depth of potential-energy minimum. Uses boiling temperature. CSP method by [1].
\[
\epsilon / k=1.15 T_{b}
\]

\section*{Parameters}

Tb [float] Boiling temperature [K]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over k, [K]

\section*{References}
[1]

\section*{Examples}
>>> epsilon_Bird_Stewart_Lightfoot_boiling(357.85)
411.5275
chemicals.lennard_jones.epsilon_Bird_Stewart_Lightfoot_melting(Tm)
Calculates Lennard-Jones depth of potential-energy minimum. Uses melting temperature. CSP method by [1].
\[
\epsilon / k=1.92 T_{m}
\]

\section*{Parameters}

Tm [float] Melting temperature [K]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over \(k\), [K]

\section*{References}
[1]

\section*{Examples}
>>> epsilon_Bird_Stewart_Lightfoot_melting(231.15)
443.808
chemicals.lennard_jones.epsilon_Stiel_Thodos( \(T c, Z c\) )
Calculates Lennard-Jones depth of potential-energy minimum. Uses Critical temperature and critical compressibility. CSP method by [1].
\[
\epsilon / k=65.3 T_{c} Z_{c}^{3.6}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]
Zc [float] Critical compressibility of fluid, [-]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over k, [K]

\section*{References}
[1]

\section*{Examples}

Fluorobenzene
>>> epsilon_Stiel_Thodos(358.5, Q.265)
196.3755830305783
chemicals.lennard_jones.epsilon_Tee_Gotoh_Steward_1 (Tc)
Calculates Lennard-Jones depth of potential-energy minimum. Uses Critical temperature. CSP method by [1].
\[
\epsilon / k=0.7740 T_{c}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over k, [K]

\section*{Notes}

Further regressions with other parameters were performed in [1] but are not included here, except for epsilon_Tee_Gotoh_Steward_2.

\section*{References}
[1]

\section*{Examples}
>>> epsilon_Tee_Gotoh_Steward_1(560.1)
433.5174

\section*{chemicals.lennard_jones.epsilon_Tee_Gotoh_Steward_2(Tc, omega)}

Calculates Lennard-Jones depth of potential-energy minimum. Uses critical temperature and acentric factor. CSP method by [1].
\[
\epsilon / k=(0.7915+0.1693 \omega) T_{c}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
epsilon_k [float] Lennard-Jones depth of potential-energy minimum over \(\mathrm{k},[\mathrm{K}\) ]

\section*{Notes}

Further regressions with other parameters were performed in [1] but are not included here, except for epsilon_Tee_Gotoh_Steward_1.

\section*{References}
[1]

\section*{Examples}
>>> epsilon_Tee_Gotoh_Steward_2(560.1, 0.245)
466.55125785

\subsection*{1.16.3 Molecular Diameter}
chemicals.lennard_jones.molecular_diameter (CASRN=None, \(T c=N o n e, P c=N o n e, V c=N o n e, Z c=N o n e\), omega=None, \(V m=\) None, \(V b=\) None, method \(=\) None)
This function handles the retrieval or calculation a chemical's L-J molecular diameter. Values are available from one source with lookup based on CASRNs, or can be estimated from 9 CSP methods. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Preferred sources are 'Magalhães, Lito, Da Silva, and Silva (2013)' for common chemicals which had valies listed in that source, and the CSP method Tee, Gotoh, and Stewart CSP with Tc, Pc, omega (1966) for chemicals which don't.

\section*{Parameters}

CASRN [str, optional] CASRN [-]
Tc [float, optional] Critical temperature, [K]
Pc [float, optional] Critical pressure, [Pa]
Vc [float, optional] Critical volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
Zc [float, optional] Critical compressibility, [-]
omega [float, optional] Acentric factor of compound, [-]
Vm [float, optional] Molar volume of liquid at the melting point of the fluid [K]
\(\mathbf{V b}\) [float, optional] Molar volume of liquid at the boiling point of the fluid [K]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in molecular_diameter_all_methods

\section*{Notes}

These values are somewhat rough, as they attempt to pigeonhole a chemical into L-J behavior.
The tabulated data is from [2], for 322 chemicals.

\section*{References}
[1], [2]

\section*{Examples}
```

>>> molecular_diameter(CASRN='64-17-5')
4.23738
>>> molecular_diameter('7727-37-9')
3.798

```
chemicals.lennard_jones.molecular_diameter_methods (CASRN=None, \(T c=N o n e, P c=N o n e, V c=N o n e\), \(Z c=\) None, omega \(=\) None, \(V m=\) None, \(V b=\) None)
Return all methods available to obtain the molecular diameter for the desired chemical.

\section*{Parameters}

CASRN [str, optional] CASRN [-]
Tc [float, optional] Critical temperature, [K]
Pc [float, optional] Critical pressure, [Pa]
Vc [float, optional] Critical volume, [m^3/mol]
Zc [float, optional] Critical compressibility, [-]
omega [float, optional] Acentric factor of compound, [-]
Vm [float, optional] Molar volume of liquid at the melting point of the fluid [K]
\(\mathbf{V b}\) [float, optional] Molar volume of liquid at the boiling point of the fluid [K]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain molecular_diameter with the given inputs.

See also:
molecular_diameter
chemicals.lennard_jones.molecular_diameter_all_methods = ('Magalhães, Lito, Da Silva, and Silva (2013)', 'Poling et al. (2001)', 'Tee, Gotoh, and Stewart CSP with Tc, Pc, omega (1966)', 'Silva, Liu, and Macedo (1998) critical relation with Tc, Pc', 'Bird, Stewart, and Light (2002) critical relation with Tc, Pc', 'Tee, Gotoh, and Stewart CSP with Tc, Pc (1966)', 'Stiel and Thodos Vc, Zc (1962)', 'Flynn (1960)', 'Bird, Stewart, and Light
(2002) critical relation with Vc', 'Bird, Stewart, and Light (2002) boiling relation', 'Bird, Stewart, and Light (2002) melting relation')

Tuple of method name keys. See the molecular_diameter for the actual references

\subsection*{1.16.4 Molecular Diameter Correlations}
chemicals.lennard_jones.sigma_Flynn(Vc)
Calculates Lennard-Jones molecular diameter. Uses critical volume. CSP method by [1] as reported in [2].
\[
\sigma=0.561\left(V_{c}^{1 / 3}\right)^{5 / 4}
\]

\section*{Parameters}

Vc [float] Critical volume of fluid [m^3/mol]
Returns
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

Notes

Vc is originally in units of \(\mathrm{mL} / \mathrm{mol}\).

\section*{References}
[1], [2]

\section*{Examples}
```

>>> sigma_Flynn(0.000268)
5.2506948422196285

```
chemicals.lennard_jones.sigma_Bird_Stewart_Lightfoot_critical_2 (Tc, Pc)
Calculates Lennard-Jones molecular diameter. Uses critical temperature and pressure. CSP method by [1].
\[
\sigma=2.44\left(T_{c} / P_{c}\right)^{1 / 3}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

\section*{Notes}

Original units of critical pressure are atmospheres.

\section*{References}
[1]

\section*{Examples}
```

>>> sigma_Bird_Stewart_Lightfoot_critical_2(560.1, 4550000)

```
5.658657684653222
chemicals.lennard_jones.sigma_Bird_Stewart_Lightfoot_critical_1(Vc)
Calculates Lennard-Jones molecular diameter. Uses critical volume. CSP method by [1].
\[
\sigma=0.841 V_{c}^{1 / 3}
\]

\section*{Parameters}

Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

Notes
Original units of Vc are \(\mathrm{mL} / \mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}
>>> sigma_Bird_Stewart_Lightfoot_critical_1(0.000268)
5.422184116631474
chemicals.lennard_jones.sigma_Bird_Stewart_Lightfoot_boiling(Vb)
Calculates Lennard-Jones molecular diameter. Uses molar volume of liquid at boiling. CSP method by [1].
\[
\sigma=1.166 V_{b, l i q}^{1 / 3}
\]

\section*{Parameters}
\(\mathbf{V b}\) [float] Boiling molar volume of liquid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
sigma [float] Lennard-Jones collision integral, [Angstrom]

\section*{Notes}

Original units of Vb are \(\mathrm{mL} / \mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}
>>> sigma_Bird_Stewart_Lightfoot_boiling(0.0001015)
5.439018856944655
chemicals.lennard_jones.sigma_Bird_Stewart_Lightfoot_melting(Vm)
Calculates Lennard-Jones molecular diameter. Uses molar volume of a liquid at its melting point. CSP method by [1].
\[
\sigma=1.222 V_{m, s o l}^{1 / 3}
\]

\section*{Parameters}

Vm [float] Melting molar volume of a liquid at its melting point [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

\section*{Notes}

Original units of Vm are \(\mathrm{mL} / \mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}
```

>>> sigma_Bird_Stewart_Lightfoot_melting(8.8e-05)
5.435407341351406

```
chemicals.lennard_jones.sigma_Stiel_Thodos \((V c, Z c)\)
Calculates Lennard-Jones molecular diameter. Uses critical volume and compressibility. CSP method by [1].
\[
\sigma=0.1866 V_{c}^{1 / 3} Z_{c}^{-6 / 5}
\]

\section*{Parameters}

Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
Zc [float] Critical compressibility of fluid, [-]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

Notes
Vc is originally in units of \(\mathrm{mL} / \mathrm{mol}\).

\section*{References}

\section*{[1]}

\section*{Examples}

Monofluorobenzene
```

>>> sigma_Stiel_Thodos(0.000271, 0.265)

```
5.94300853971033
chemicals.lennard_jones.sigma_Tee_Gotoh_Steward_1 (Tc, Pc)
Calculates Lennard-Jones molecular diameter. Uses critical temperature and pressure. CSP method by [1].
\[
\sigma=2.3647\left(\frac{T_{c}}{P_{c}}\right)^{1 / 3}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

\section*{Notes}

Original units of Pc are atm. Further regressions with other parameters were performed in [1] but are not included here, except for sigma_Tee_Gotoh_Steward_2.

\section*{References}
[1]

\section*{Examples}
>>> sigma_Tee_Gotoh_Steward_1(560.1, 4550000)
5.48402779790962
chemicals.lennard_jones.sigma_Tee_Gotoh_Steward_2 (Tc, Pc, omega)
Calculates Lennard-Jones molecular diameter. Uses critical temperature, pressure, and acentric factor. CSP method by [1].
\[
\sigma=(2.3551-0.0874 \omega)\left(\frac{T_{c}}{P_{c}}\right)^{1 / 3}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

\section*{Notes}

Original units of Pc are atm. Further regressions with other parameters were performed in [1] but are not included here, except for sigma_Tee_Gotoh_Steward_1.

\section*{References}
[1]

\section*{Examples}
>>> sigma_Tee_Gotoh_Steward_2(560.1, 4550000, 0.245)
5.412104867264477
chemicals.lennard_jones.sigma_Silva_Liu_Macedo( \(T c, P c\) )
Calculates Lennard-Jones molecular diameter. Uses critical temperature and pressure. CSP method by [1].
\[
\sigma_{L J}^{3}=0.17791+11.779\left(\frac{T_{c}}{P_{c}}\right)-0.049029\left(\frac{T_{c}}{P_{c}}\right)^{2}
\]

\section*{Parameters}

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}
sigma [float] Lennard-Jones molecular diameter, [Angstrom]

\section*{Notes}

Pc is originally in bar. An excellent paper. None is returned if the polynomial returns a negative number, as in the case of 1029.13 K and 3.83 bar.

\section*{References}
[1]

\section*{Examples}
>>> sigma_Silva_Liu_Macedo(560.1, 4550000)
5.164483998730177

\subsection*{1.16.5 Utility Functions}
chemicals.lennard_jones.T_star ( \(T\), epsilon_k=None, epsilon=None)
This function calculates the parameter \(T_{-}\)star as needed in performing collision integral calculations.
\[
T^{*}=\frac{k T}{\epsilon}
\]

\section*{Parameters}
epsilon_k [float, optional] Lennard-Jones depth of potential-energy minimum over \(k,[\mathrm{~K}]\)
epsilon [float, optional] Lennard-Jones depth of potential-energy minimum [J]

\section*{Returns}

T_star [float] Dimentionless temperature for calculating collision integral, [-]

\section*{Notes}

Tabulated values are normally listed as epsilon/k. k is the Boltzman constant, with units of \(\mathrm{J} / \mathrm{K}\).

\section*{References}
[1]

\section*{Examples}
```

>>> T_star(T=318.2, epsilon_k=308.43)

```
1.0316765554582887

\subsection*{1.17 Miscellaneous Data (chemicals.miscdata)}

This module contains several tables which are common to different lookup functions.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Temperature Dependent data

\subsection*{1.17.1 Temperature Dependent data}

\section*{chemicals.miscdata.lookup_VDI_tabular_data (CASRN, prop)}

This function retrieves the tabular data available for a given chemical and a given property. Lookup is based on CASRNs. Length of data returned varies between chemicals. All data is at saturation condition from [1].
Function has data for 58 chemicals.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}
prop [string] Property [-]

\section*{Returns}

Ts [list] Temperatures where property data is available, \([\mathrm{K}]\) props [list] Properties at each temperature, [various]

\section*{Notes}

The available properties are 'P', 'Density (l)', 'Density (g)', ‘Hvap', ‘Cp (l)', ‘Cp (g)', 'Mu (l)', 'Mu (g)', ‘K (l)', 'K (g)', 'Pr (l)', 'Pr (g)', ‘sigma', 'Beta', 'Volume (l)', and 'Volume (g)'.
Data is available for all properties and all chemicals; surface tension data was missing for mercury, but added as estimated from the \(\mathrm{a} / \mathrm{b}\) coefficients listed in Jasper (1972) to simplify the function.

\section*{References}
[1]

\section*{Examples}
```

>>> lookup_VDI_tabular_data('67-56-1', 'Mu (g)')
([337.63, 360.0, 385.0, 410.0, 435.0, 460.0, 500.0], [1.11e-05, 1.18e-05, 1.27e-05,七
|1.36e-05, 1.46e-05, 1.59e-05, 2.04e-05])
>>> lookup_VDI_tabular_data('7782-41-4', 'sigma')
([53.49, 64.0, 74.0, 85.04, 92.0, 102.0, 112.0, 122.0, 132.0, 144.41], [0.0227, 0.
@2, 0.0166, 0.0136, 0.0117, 0.0092, 0.0068, 0.0045, 0.0024, 0.0])

```

\subsection*{1.18 Chemical Geometry (chemicals.molecular_geometry)}

This module contains various radius of gyration functions.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Lookup Functions

\subsection*{1.18.1 Lookup Functions}

\section*{chemicals.molecular_geometry.RG(CASRN, method=None)}

This function handles the retrieval of a chemical's radius of gyration. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 670 chemicals.

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}

RG [float] Radius of gyration, [m]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in RG_methods

\section*{Notes}

The available sources are as follows:
- 'PSI4_2022A', values computed using the Psi4 version 1.3.2 quantum chemistry software, with initialized positions from rdkit's EmbedMolecule method, the basis set 6-31G** and the method mp2 [1].
- 'CHEMSEP', from the databank included and distributed with the licence notice ChemSep v8.1 pure component data - Copyright (c) Harry Kooijman and Ross Taylor (2018) - http://www.perlfoundation.org/ artistic_license_2_0. A small portion of the data is used.

\section*{References}
[1], [2]

\section*{Examples}
>> RG(CASRN='64-17-5')
2.225e-10
chemicals.molecular_geometry.RG_methods(CASRN)
Return all methods available to obtain the radius of gyration for the desired chemical.

\section*{Parameters}

\section*{CASRN [str] CASRN, [-]}

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the RG with the given inputs.
See also:
RG
```

chemicals.molecular_geometry.RG_all_methods = ('PSI4_2022A', 'CHEMSEP')

```

Tuple of method name keys. See the \(R G\) for the actual references
chemicals.molecular_geometry.linear (CASRN, method=None)
This function handles the retrieval whether or not a chemical is linear. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.
Function has data for approximately 300 chemicals.

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}
linear [bool] Whether or not the chemical is linear, [-]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in linear_methods

\section*{Notes}

The available sources are as follows:
- 'PSI4_2022A', values computed using the Psi4 version 1.3.2 quantum chemistry software, with initialized positions from rdkit's EmbedMolecule method, the basis set \(6-31 \mathrm{G}^{* *}\) and the method mp2 [1].

Warning: This function does not yet have a reliable data source.

\section*{References}
[1]

\section*{Examples}
>>> linear (CASRN='64-17-5')
False
chemicals.molecular_geometry.linear_methods(CASRN)
Return all methods available to obtain whether or not the desired chemical is linear.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the linear with the given inputs.

\section*{See also:}
linear
chemicals.molecular_geometry.linear_all_methods = ('PSI4_2022A',)
Tuple of method name keys. See the linear for the actual references

\subsection*{1.19 Support for Numba (chemicals.numba)}

Basic module which wraps most of chemicals functions and classes to be compatible with the Numba dynamic Python compiler. Numba is only supported on Python 3, and may require the latest version of Numba. Numba is rapidly evolving, and hopefully in the future it will support more of the functionality of fluids.

Using the numba-accelerated version of chemicals is easy; simply call functions and classes from the chemicals.numba namespace. The chemicals.numba module must be imported separately on Python < 3.7; it is not loaded automatically as part of chemicals.
```

>>> import chemicals
>>> import chemicals.numba
>>> chemicals.numba.Antoine(180, A=8.95894, B=510.595, C=-15.95)
702271.05185795

```

There is a delay while the code is compiled when using Numba; the speed is not quite free.
Some parts of chemicals are not supported in the Numba interface. Any data lookup function like Tc () and omega_methods () are not numba compatible. These functions could not be speed up anyway though as they are memory-bound and numba helps with things that are compute-bound.

Today, the list of things known not to work is as follows:
- Everything in chemicals.identifiers
- Everything in chemicals. combustion (uses dictionaries)
- Everything in chemicals.elements (uses dictionaries, periodic_table class, string parsing)
- Everything in chemicals.critical except the mixture critical point routines
- In chemicals.flash_basic, flash_Tb_Tc_Pc() and flash_ideal() have not been ported but can be made compatible.
- In chemicals.dippr, only EQ102() is unsupported as it uses a complex hyp2f1 call.
- In chemicals.reaction, stoichiometric_matrix() (dictionaries), balance_stoichiometry() (scipy functions, fractional numbers).
- In chemicals.safety, LFL_ISO_10156_2017() (dictionaries)
- The assorted functions collision_integral_Kim_Monroe(), Henry_pressure_mixture(), T_converter(), Wilke(), Wilke_prefactors(), Brokaw() viscosity_converter(), CAS_to_int(), int_to_CAS(), sorted_CAS_key() may or may not be able to be ported but have not yet been.

All of the regular Numba-compiled functions are built with the nogil flag, which means you can use Python's threading mechanism effectively to get the speed of parallel processing.

\subsection*{1.20 Relative Permittivity/Dielectric Constant (chemicals.permittivity)}

This module contains various permittivity calculation routines and dataframes of coefficients for correlations.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Correlations for Specific Substances
- Fit Coefficients

\subsection*{1.20.1 Correlations for Specific Substances}

\section*{chemicals.permittivity.permittivity_IAPWS ( \(T, r h o\) )}

Calculate the relative permittivity of pure water as a function of. temperature and density. Assumes the 1997 IAPWS [1] formulation.
\[
\begin{gathered}
\epsilon(\rho, T)=\frac{1+A+5 B+\left(9+2 A+18 B+A^{2}+10 A B+9 B^{2}\right)^{0.5}}{4(1-B)} \\
A(\rho, T)=\frac{N_{A} \mu^{2} \rho g}{M \epsilon_{0} k T} \\
B(\rho)=\frac{N_{A} \alpha \rho}{3 M \epsilon_{0}} \\
g(\delta, \tau)=1+\sum_{i=1}^{11} n_{i} \delta^{I_{i}} \tau^{J_{i}}+n_{12} \delta\left(\frac{647.096}{228} \tau^{-1}-1\right)^{-1.2} \\
\delta=\rho /\left(322 \mathrm{~kg} / \mathrm{m}^{3}\right) \\
\tau=T / 647.096 \mathrm{~K}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of water [K]
rho [float] Mass density of water at \(T\) and \(P\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]\)

\section*{Returns}
epsilon [float] Relative permittivity of water at T and rho, [-]

\section*{Notes}

Validity:
\(273.15<\mathrm{T}<323.15 \mathrm{~K}\) for \(0<\mathrm{P}<\) iceVI melting pressure at T or 1000 MPa , whichever is smaller.
\(323.15<\mathrm{T}<873.15 \mathrm{~K} 0<\mathrm{p}<600 \mathrm{MPa}\).
Coefficients and constants (they are optimized away in the function itself):
\(\mathrm{ih}=[1,1,1,2,3,3,4,5,6,7,10]\)
\(\mathrm{jh}=[0.25,1,2.5,1.5,1.5,2.5,2,2,5,0.5,10]\)
\(\mathrm{Nh}=[\mathbf{0 . 9 7 8 2 2 4 4 8 6 8 2 6},-\mathbf{0 . 9 5 7 7 7 1 3 7 9 3 7 5}, \mathbf{0 . 2 3 7 5 1 1 7 9 4 1 4 8}, \mathbf{0 . 7 1 4 6 9 2 2 4 4 3 9 6},-0.298217036956\), \(0.108863472196,0.949327488264 \mathrm{E}-1,-.980469816509 \mathrm{E}-2,0.165167634970 \mathrm{E}-4,0.937359795772 \mathrm{E}-4\), -0.12317921872E-9]
polarizability \(=1.636 \mathrm{E}-40\)
dipole \(=6.138 \mathrm{E}-30\)

\section*{References}
[1]

\section*{Examples}
```

>>> permittivity_IAPWS(373., 958.46)
55.565841872697234
>>> permittivity_IAPWS(650., 40.31090)
1.2659205723606064

```
chemicals.permittivity.permittivity_CRC \((T, a, b, c, d)\)

Return the relative permittivity (epsilon) of a chemical using a polynomical equation as in [1].

\section*{Parameters}
\(\mathbf{a , b , c , d}\) [float] Regressed coefficients.

\section*{Notes}

The permittivity is given by \(\epsilon_{r}=A+B T+C T^{2}+D T^{3}\)

\section*{References}
[1]

\section*{Examples}

Calculate the permittivity of 4-Nitroaniline:
>>> permittivity_CRC(450., 487, -1.5, 0.00129, 0.)
73.225

\subsection*{1.20.2 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.permittivity.permittivity_data_CRC
Data from [1] with coefficients fit to a polynomial in terms of temperature in K. \(\epsilon_{r}=A+B T+C T^{2}+D T^{3}\) is the equation, although some chemcials only have a constant value.
```

In [1]: import chemicals
In [2]: chemicals.permittivity.permittivity_data_CRC
Out[2]:

```
(continued from previous page)
\begin{tabular}{|c|c|c|}
\hline & Chemical & Tmax \\
\hline CAS & & \\
\hline 50-70-4 & D-Glucitol & NaN \\
\hline 50-78-2 & 2-(Acetyloxy)benzoic acid & 416.0 \\
\hline 51-79-6 & Ethyl carbamate & 368.0 \\
\hline 54-11-5 & L-Nicotine & 363.0 \\
\hline 55-63-0 & Trinitroglycerol & NaN \\
\hline \(\ldots\) & & \(\ldots\) \\
\hline 100295-85-0 & 6-Methyl-3-heptanol, ()- & 383.0 \\
\hline 100296-26-2 & 2-Methyl-3-heptanol, ()- & 403.0 \\
\hline 111675-77-5 & 2-Methyl-1-heptanol, ()- & 328.0 \\
\hline 111767-95-4 & 5-Methyl-1-heptanol, ()- & 328.0 \\
\hline 123434-07-1 & 2,4,6-Trimethyl-3-heptene (unspecified isomer) & NaN \\
\hline
\end{tabular}

\subsection*{1.21 Phase Change Properties (chemicals.phase_change)}

This module contains lookup functions for melting and boiling point, heat of fusion, various enthalpy of vaporization estimation routines, and dataframes of fit coefficients.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Boiling Point
- Melting Point
- Heat of Fusion
- Heat of Vaporization at Tb Correlations
- Heat of Vaporization at T Correlations
- Heat of Vaporization at T Model Equations
- Heat of Sublimation
- Fit Coefficients

\subsection*{1.21.1 Boiling Point}

\section*{chemicals.phase_change.Tb (CASRN, method=None)}

This function handles the retrieval of a chemical's normal boiling point. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available. Function has data for approximately 34000 chemicals.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Tb [float] Boiling temperature, [K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, Tb_all_methods.

\section*{See also:}

Tb_methods

\section*{Notes}

The available sources are as follows:
- 'CRC_ORG', a compillation of data on organics as published in [1].
- 'CRC_INORG', a compillation of data on inorganic as published in [1].
- 'WEBBOOK', a NIST resource [6] containing mostly experimental and averaged values
- 'WIKIDATA', data from the Wikidata project [3]
- 'COMMON_CHEMISTRY', a project from the CAS [4]
- 'JOBACK', an estimation method for organic substances in [5]
- 'YAWS', a large compillation of data from a variety of sources both experimental and predicted; no data points are sourced in the work of [2].
- 'HEOS', a series of values from the NIST REFPROP Database for Highly Accurate Properties of Industrially Important Fluids (and other high-precision fundamental equations of state)

\section*{References}
[1], [2], [3], [4], [5], [6], [7]

\section*{Examples}
```

>>> Tb('7732-18-5')

```
373.124
chemicals.phase_change.Tb_methods (CASRN)
Return all methods available to obtain the normal boiling point for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Tb with the given inputs.

\section*{See also:}

Tb
chemicals.phase_change.Tb_all_methods = ('HEOS', 'CRC_INORG', 'CRC_ORG', 'COMMON_CHEMISTRY', 'WEBBOOK', 'YAWS', 'WIKIDATA', 'JOBACK')

Tuple of method name keys. See the Tbg for the actual references

\subsection*{1.21.2 Melting Point}

\section*{chemicals.phase_change. \(\operatorname{Tm}(C A S R N\), method \(=\) None \()\)}

This function handles the retrieval of a chemical's melting point. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available. Function has data for approximately 83000 chemicals.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Tm [float] Melting temperature, [K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by the vairable Tm_all_methods.

\section*{See also:}

Tm_methods

\section*{Notes}

The available sources are as follows:
- 'OPEN_NTBKM, a compillation of data on organics as published in [1] as Open Notebook Melting Points; Averaged (median) values were used when multiple points were available. For more information on this invaluable and excellent collection, see http://onswebservices.wikispaces.com/meltingpoint.
- 'CRC_ORG', a compillation of data on organics as published in [2].
- 'CRC_INORG', a compillation of data on inorganic as published in [2].
- 'WEBBOOK', a NIST resource [6] containing mostly experimental and averaged values
- 'WIKIDATA', data from the Wikidata project [3]
- 'COMMON_CHEMISTRY', a project from the CAS [4]
- 'JOBACK', an estimation method for organic substances in [5]

\section*{References}
[1], [2], [3], [4], [5], [6]

\section*{Examples}
>>> Tm(CASRN='7732-18-5')
273.15
chemicals.phase_change.Tm_methods(CASRN)
Return all methods available to obtain the melting point for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Tm with the given inputs.

\section*{See also:}

Tm
```

chemicals.phase_change.Tm_all_methods = ('OPEN_NTBKM', 'CRC_INORG', 'CRC_ORG',
'COMMON_CHEMISTRY', 'WEBBOOK', 'WIKIDATA', 'JOBACK')
Tuple of method name keys. See the Tm for the actual references

```

\subsection*{1.21.3 Heat of Fusion}

Heat of fusion does not strongly depend on temperature or pressure. This is the standard value, at 1 atm and the normal melting point.

\section*{chemicals.phase_change.Hfus(CASRN, method=None)}

This function handles the retrieval of a chemical's heat of fusion. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 22000 chemicals.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Hfus [float] Molar enthalpy of fusion at normal melting point, [J/mol]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by the variable, Hfus_all_methods.

\section*{See also:}

Hfus_methods

\section*{Notes}

The available sources are as follows:
- 'CRC', a compillation of data on organics and inorganics as published in [1].
- 'WEBBOOK', a NIST resource [4] containing mostly experimental and averaged values
- 'WIKIDATA', data from the Wikidata project [2]
- 'JOBACK', an estimation method for organic substances in [3]

\section*{References}
[1], [2], [3], [4]

Examples
>>> Hfus('7732-18-5')
6010.0
chemicals.phase_change.Hfus_methods(CASRN)
Return all methods available to obtain the heat of fusion for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Hfus with the given inputs.
See also:

Hfus
chemicals.phase_change.Hfus_all_methods = ('CRC', 'WEBBOOK', 'WIKIDATA', 'JOBACK')
Tuple of method name keys. See the Hfus for the actual references

\subsection*{1.21.4 Heat of Vaporization at Tb Correlations}
chemicals.phase_change. Riedel \((T b, T c, P c)\)
Calculates enthalpy of vaporization at the boiling point, using the Ridel [1] CSP method. Required information are critical temperature and pressure, and boiling point. Equation taken from [2] and [3].

The enthalpy of vaporization is given by:
\[
\Delta_{v a p} H=1.093 T_{b} R \frac{\ln P_{c}-1.013}{0.930-T_{b r}}
\]

\section*{Parameters}

Tb [float] Boiling temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}

Hvap [float] Enthalpy of vaporization at the normal boiling point, [J/mol]

\section*{Notes}

This equation has no example calculation in any source. The source has not been verified. It is equation 4-144 in Perry's. Perry's also claims that errors seldom surpass 5\%.
[2] is the source of example work here, showing a calculation at \(0.0 \%\) error.
Internal units of pressure are bar.

\section*{References}
[1], [2], [3]

\section*{Examples}

Pyridine, \(0.0 \%\) err vs. exp: \(35090 \mathrm{~J} / \mathrm{mol}\); from Poling [2].
```

>>> Riedel(388.4, 620.0, 56.3E5)

```
35089.80179000598
chemicals.phase_change. Chen \((T b, T c, P c)\)
Calculates enthalpy of vaporization using the Chen [1] correlation and a chemical's critical temperature, pressure and boiling point.

The enthalpy of vaporization is given by:
\[
\Delta H_{v b}=R T_{b} \frac{3.978 T_{r}-3.958+1.555 \ln P_{c}}{1.07-T_{r}}
\]

\section*{Parameters}

Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

The formulation presented in the original article is similar, but uses units of atm and calorie instead. The form in [2] has adjusted for this. A method for estimating enthalpy of vaporization at other conditions has also been developed, but the article is unclear on its implementation. Based on the Pitzer correlation.

Internal units: bar and K

\section*{References}
[1], [2]

\section*{Examples}

Same problem as in Perry's examples.
>>> Chen(294.0, 466.0, 5.55E6)
26705.902558030946

\section*{chemicals.phase_change.Liu( \(T b, T c, P c\) )}

Calculates enthalpy of vaporization at the normal boiling point using the Liu [1] correlation, and a chemical's critical temperature, pressure and boiling point.
The enthalpy of vaporization is given by:
\[
\Delta H_{v a p}=R T_{b}\left[\frac{T_{b}}{220}\right]^{0.0627} \frac{\left(1-T_{b r}\right)^{0.38} \ln \left(P_{c} / P_{A}\right)}{1-T_{b r}+0.38 T_{b r} \ln T_{b r}}
\]

\section*{Parameters}

Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

This formulation can be adjusted for lower boiling points, due to the use of a rationalized pressure relationship. The formulation is taken from the original article.

A correction for alcohols and organic acids based on carbon number, which only modifies the boiling point, is available but not implemented.
No sample calculations are available in the article.
Internal units: Pa and K

\section*{References}
[1]

\section*{Examples}

Same problem as in Perry's examples
>>> Liu(294.0, 466.0, 5.55E6)
26378.575260517395
chemicals.phase_change. Vetere ( \(T b, T c, P c, F=1.0\) )
Calculates enthalpy of vaporization at the boiling point, using the Vetere [1] CSP method. Required information are critical temperature and pressure, and boiling point. Equation taken from [2].

The enthalpy of vaporization is given by:
\[
\frac{\Delta H_{v a p}}{R T_{b}}=\frac{\tau_{b}^{0.38}\left[\ln P_{c}-0.513+\frac{0.5066}{P_{c} T_{b r}^{2}}\right]}{\tau_{b}+F\left(1-\tau_{b}^{0.38}\right) \ln T_{b r}}
\]

\section*{Parameters}

Tb [float] Boiling temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
F [float, optional] Constant for a fluid, [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization at the boiling point, [J/mol]

\section*{Notes}

The equation cannot be found in the original source. It is believed that a second article is its source, or that DIPPR staff have altered the formulation.

Internal units of pressure are bar.

\section*{References}
[1], [2]

\section*{Examples}

Example as in [2], p2-487; exp: 25.73
```

>>> Vetere(294.0, 466.0, 5.55E6)

```
26363.43895706672

\subsection*{1.21.5 Heat of Vaporization at T Correlations}

\section*{chemicals.phase_change. Pitzer ( \(T, T c\), omega)}

Calculates enthalpy of vaporization at arbitrary temperatures using a fit by [2] to the work of Pitzer [1]; requires a chemical's critical temperature and acentric factor.

The enthalpy of vaporization is given by:
\[
\frac{\Delta_{v a p} H}{R T_{c}}=7.08\left(1-T_{r}\right)^{0.354}+10.95 \omega\left(1-T_{r}\right)^{0.456}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

This equation is listed in [3], page 2-487 as method \#2 for estimating Hvap. This cites [2].
The recommended range is 0.6 to 1 Tr . Users should expect up to \(5 \%\) error. This function converges to zero at \(T c\). If Tc is larger than T, 0 is returned as the model would return complex numbers.
The original article has been reviewed and found to have a set of tabulated values which could be used instead of the fit function to provide additional accuracy.

\section*{References}
[1], [2], [3]

\section*{Examples}

Example as in [3], p2-487; exp: \(37.51 \mathrm{~kJ} / \mathrm{mol}\)
```

>>> Pitzer(452, 645.6, 0.35017)
36696.749078320056

```
chemicals.phase_change.SMK (T, Tc, omega)
Calculates enthalpy of vaporization at arbitrary temperatures using a the work of [1]; requires a chemical's critical temperature and acentric factor.

The enthalpy of vaporization is given by:
\[
\begin{gathered}
\frac{\Delta H_{v a p}}{R T_{c}}=\left(\frac{\Delta H_{v a p}}{R T_{c}}\right)^{(R 1)}+\left(\frac{\omega-\omega^{(R 1)}}{\omega^{(R 2)}-\omega^{(R 1)}}\right)\left[\left(\frac{\Delta H_{v a p}}{R T_{c}}\right)^{(R 2)}-\left(\frac{\Delta H_{v a p}}{R T_{c}}\right)^{(R 1)}\right] \\
\left(\frac{\Delta H_{v a p}}{R T_{c}}\right)^{(R 1)}=6.537 \tau^{1 / 3}-2.467 \tau^{5 / 6}-77.251 \tau^{1.208}+59.634 \tau+36.009 \tau^{2}-14.606 \tau^{3} \\
\left(\frac{\Delta H_{v a p}}{R T_{c}}\right)^{(R 2)}-\left(\frac{\Delta H_{v a p}}{R T_{c}}\right)^{(R 1)}=-0.133 \tau^{1 / 3}-28.215 \tau^{5 / 6}-82.958 \tau^{1.208}+99.00 \tau+19.105 \tau^{2}-2.796 \tau^{3}
\end{gathered}
\]
\[
\tau=1-T / T_{c}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

The original article has been reviewed and found to have coefficients with slightly more precision. Additionally, the form of the equation is slightly different, but numerically equivalent.

The refence fluids are:
\(\omega_{0}=\) benzene \(=0.212\)
\(\omega_{1}=\) carbazole \(=0.461\)
A sample problem in the article has been verified. The numerical result presented by the author requires high numerical accuracy to obtain.

This function converges to zero at \(T c\). If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

Problem in [1]:
```

>>> SMK(553.15, 751.35, 0.302)
39866.189990446229

```
chemicals.phase_change.MK \((T, T c\), omega)
Calculates enthalpy of vaporization at arbitrary temperatures using a the work of [1]; requires a chemical's critical temperature and acentric factor.

The enthalpy of vaporization is given by:
\[
\begin{gathered}
\Delta H_{v a p}=\Delta H_{v a p}^{(0)}+\omega \Delta H_{v a p}^{(1)}+\omega^{2} \Delta H_{v a p}^{(2)} \\
\frac{\Delta H_{v a p}^{(i)}}{R T_{c}}=b^{(j)} \tau^{1 / 3}+b_{2}^{(j)} \tau^{5 / 6}+b_{3}^{(j)} \tau^{1.2083}+b_{4}^{(j)} \tau+b_{5}^{(j)} \tau^{2}+b_{6}^{(j)} \tau^{3} \\
\tau=1-T / T_{c}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

The original article has been reviewed. A total of 18 coefficients are used:
WARNING: The correlation has been implemented as described in the article, but its results seem different and with some error. Its results match with other functions however.

Has poor behavior for low-temperature use. This function converges to zero at \(T c\). If Tc is larger than \(\mathrm{T}, 0\) is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

Problem in article for SMK function.
>>> MK(553.15, 751.35, 0.302)
38728.00667307733
chemicals.phase_change. Velasco ( \(T, T c\), omega)
Calculates enthalpy of vaporization at arbitrary temperatures using a the work of [1]; requires a chemical's critical temperature and acentric factor.

The enthalpy of vaporization is given by:
\[
\Delta_{v a p} H=R T_{c}\left(7.2729+10.4962 \omega+0.6061 \omega^{2}\right)\left(1-T_{r}\right)^{0.38}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
omega [float] Acentric factor [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

The original article has been reviewed. It is regressed from enthalpy of vaporization values at 0.7 Tr , from 121 fluids in REFPROP 9.1. A value in the article was read to be similar, but slightly too low from that calculated here. This function converges to zero at \(T c\). If Tc is larger than T, 0 is returned as the model would return complex numbers.

\section*{References}
[1]

\section*{Examples}

From graph, in [1] for perfluoro-n-heptane.
>>> Velasco(333.2, 476.0, 0.5559)
33299.428636069264
chemicals.phase_change. Clapeyron ( \(T, T c, P c, d Z=1\), Psat=101325)
Calculates enthalpy of vaporization at arbitrary temperatures using the Clapeyron equation.
The enthalpy of vaporization is given by:
\[
\Delta H_{v a p}=R T \Delta Z \frac{\ln \left(P_{c} / P s a t\right)}{\left(1-T_{r}\right)}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
\(\mathbf{d Z}\) [float] Change in compressibility factor between liquid and gas, []
Psat [float] Saturation pressure of fluid [Pa], optional

\section*{Returns}

Hvap [float] Enthalpy of vaporization, [J/mol]

\section*{Notes}

No original source is available for this equation. [1] claims this equation overpredicts enthalpy by several percent. Under \(\operatorname{Tr}=0.8, \mathrm{dZ}=1\) is a reasonable assumption. This equation is most accurate at the normal boiling point.
Internal units are bar.
WARNING: I believe it possible that the adjustment for pressure may be incorrect

\section*{References}
[1]

\section*{Examples}

Problem from Perry's examples.
```

>>> Clapeyron(T=294.0, Tc=466.0, Pc=5.55E6)

```
26512. 36357131963
chemicals.phase_change.Watson(T,Hvap_ref, T_ref, Tc, exponent=0.38)
Calculates enthalpy of vaporization of a chemical at a temperature using the known heat of vaporization at another temperature according to the Watson [1] [2] correlation. This is an application of the correspondingstates principle, with an emperical temperature dependence.
\[
\frac{\Delta H_{v a p}^{T 1}}{\Delta H_{v a p}^{T 2}}=\left(\frac{1-T_{r, 1}}{1-T_{r, 2}}\right)^{0.38}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature for which to calculate heat of vaporization, [K]
Hvap_ref [float] Enthalpy of vaporization at the known temperature point, [J/mol]
T_ref [float] Reference temperature; ideally as close to \(T\) as posible, [K]
Tc [float] Critical temperature of fluid [K]
exponent [float, optional] A fit exponent can optionally be used instead of the Watson 0.38 exponent, [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization at \(T,[\mathrm{~J} / \mathrm{mol}]\)

\section*{References}
[1], [2]

\section*{Examples}

Predict the enthalpy of vaporization of water at 320 K from a point at 300 K :
```

>>> Watson(T=320, Hvap_ref=43908, T_ref=300.0, Tc=647.14)

```
42928.990094915454

The error is \(0.38 \%\) compared to the correct value of \(43048 \mathrm{~J} / \mathrm{mol}\).
If the provided temperature is above the critical point, zero is returned.
chemicals.phase_change.Watson_n(T1, T2, Hvap1, Hvap2, Tc)
Calculates the Watson heat of vaporizaton extrapolation exponent given two known heats of vaporization.
\[
n=\left[\frac{\ln \left(\frac{\text { Hop }_{1}}{H \text { vap }_{2}}\right)}{\ln \left(\frac{T_{1}-T_{c}}{T_{2}-T_{c}}\right)}\right]
\]

\section*{Parameters}
\(\mathbf{T 1}\) [float] Temperature of first heat of vaporization point, [K]
\(\mathbf{T} 2\) [float] Temperature of second heat of vaporization point, [K]

Hvap1 [float] Enthalpy of vaporization at the first known temperature point, [J/mol]
Hvap2 [float] Enthalpy of vaporization at the second known temperature point, [J/mol]
Tc [float] Critical temperature of fluid [K]

\section*{Returns}
exponent [float] A fit exponent that can be used instead of the Watson 0.38 exponent, [-]

\section*{Notes}

This can be useful for extrapolating when a correlation does not reach the critical point.

\section*{Examples}
```

>>> Watson_n(T1=320, T2=300, Hvap1=42928.990094915454, Hvap2=43908, Tc=647.14)
0.380000000000

```

\subsection*{1.21.6 Heat of Vaporization at T Model Equations}
chemicals.phase_change.Alibakhshi ( \(T, T c, C\) )
Calculates enthalpy of vaporization of a chemical at a temperature using a theoretically-derived single-coefficient fit equation developed in [1]. This model falls apart at \(\sim 0.8 \mathrm{Tc}\).
\[
\Delta H_{v a p}=\left(4.5 \pi N_{A}\right)^{1 / 3 .} 4.2 \times 10^{-7}\left(T_{c}-6\right)-0.5 R T \ln (T)+C T
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature for which to calculate heat of vaporization, [K]
Tc [float] Critical temperature of fluid [K]
C [float] Alibakhshi fit coefficient, [J/mol/K]

\section*{Returns}

Hvap [float] Enthalpy of vaporization at \(T,[\mathrm{~J} / \mathrm{mol}]\)

\section*{Notes}

The authors of [1] evaluated their model on 1890 compounds for a temperature range of 50 K under Tb to 100 K below \(T c\), and obtained an average absolute relative error of \(4.5 \%\).

\section*{References}
[1]

\section*{Examples}

Predict the enthalpy of vaporization of water at 320 K :
>>> Alibakhshi(T=320.0, Tc=647.14, C=-16.7171)
41961.30490225752

The error is \(2.5 \%\) compared to the correct value of \(43048 \mathrm{~J} / \mathrm{mol}\).
chemicals.phase_change. \(\operatorname{PPDS} 12(T, T c, A, B, C, D, E)\)
Calculate the enthalpy of vaporization of a fluid using the 5 -term power fit developed by the PPDS and named PPDS equation 12.
\[
\begin{gathered}
H_{v a p}=R T_{c}\left(A \tau^{1 / 3}+B \tau^{2 / 3}+C \tau+D \tau^{2}+E \tau^{6}\right) \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid \([\mathrm{K}\) ]
A [float] Coefficient, [-]
B [float] Coefficient, [-]
C [float] Coefficient, [-]
D [float] Coefficient, [-]
E [float] Coefficient, [-]

\section*{Returns}

Hvap [float] Enthalpy of vaporization at \(T\), [ \(\mathrm{J} / \mathrm{mol}\) ]

\section*{Notes}

Coefficients can be found in [1], but no other source for these coefficients has been found.

\section*{References}
[1], [2]

\section*{Examples}

Example from [1]:
```

>>> PPDS12(300.0, 591.75, 4.60584, 13.97224, -10.592315, 2.120205, 4.277128)

```
37948.76862035925

Example from [2] for benzene; note the coefficients from [2] predict enthalpy of vaporization in \(\mathrm{kJ} / \mathrm{mol}\), so the output must be adjusted. The same effect can be obtained by multiplying each of the coefficients by 1000 .
```

>>> 1000.0*PPDS12(300.0, 562.05, 0.00171484, 0.0258604, -0.0243564, 0.00740881,0.
->00680068)
33662.4258030

```

\subsection*{1.21.7 Heat of Sublimation}

No specific correlation is provided. This value is fairly strongly temperature dependent; the dependency comes almost entirely from the vaporization enthalpy's dependence. To calculate heat of sublimation at any temperature, use the equation \(H_{\text {sub }}=H_{\text {fus }}+H_{\text {vap }}\).

\subsection*{1.21.8 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.phase_change.phase_change_data_Perrys2_150
A collection of 344 coefficient sets from the DIPPR database published openly in [1]. Provides temperature limits for all its fluids. See chemicals.dippr.EQ106 for the model equation.
chemicals.phase_change.phase_change_data_VDI_PPDS_4
Coefficients for a equation form developed by the PPDS, published openly in [2]. Extrapolates poorly at low temperatures. See PPDS12 for the model equation.
chemicals.phase_change.phase_change_data_Alibakhshi_Cs
One-constant limited temperature range regression coefficients presented in [3], with constants for \(\sim 2000\) chemicals from the DIPPR database. Valid up to 100 K below the critical point, and 50 K under the boiling point. See Alibakhshi for the model equation.

The structure of each dataframe is shown below:
```

In [1]: import chemicals
In [2]: chemicals.phase_change.phase_change_data_Perrys2_150
Out[2]:
CAS
50-00-0
55-21-0
56-23-5
Carbon tetrachlorid
60-29-7
...
10028-15-
10035-10-6 Hydrogen bromid
10102-43-9 Nitric oxid
13511-13-2 Propenylcyclohexen
132259-10-0
[344 rows x 8 columns]
In [3]: chemicals.phase_change.phase_change_data_VDI_PPDS_4
Out[3]:
Chemical MW ...
E
CAS
50-00-0
56-23-5
56-81-5
60-29-7
62-53-3

| Chemical | MW | $\ldots$ | D | E |
| ---: | ---: | :--- | ---: | ---: |
|  |  | $\ldots$ |  |  |
| Formaldehyde | 30.03 | $\ldots$ | -4.856937 | 11.036836 |
| Carbon tetrachloride | 153.82 | $\ldots$ | -0.172679 | 3.053272 |
| Glycerol | 92.09 | $\ldots$ | 2.052518 | -13.771300 |
| Diethyl ether | 74.12 | $\ldots$ | -0.175016 | 3.557340 |
| Aniline | 93.13 | $\ldots$ | -1.656520 | 3.263408 |

```
\begin{tabular}{lrrlrr}
\(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) \\
\(10097-32-2\) & Bromine & 159.82 & \(\ldots\) & -0.025698 & -0.197360 \\
\(10102-43-9\) & Nitric oxide & 30.01 & \(\ldots\) & -5.159373 & 97.203137 \\
\(10102-44-0\) & Nitrogen dioxide & 46.01 & \(\ldots\) & 10.653997 & 68.680656 \\
\(10544-72-6\) & Dinitrogentetroxide & 92.01 & \(\ldots\) & -1.535179 & 102.679020 \\
\(132259-10-0\) & Air & 28.96 & \(\ldots\) & -8.064787 & 14.645081
\end{tabular}
[272 rows x 8 columns]
In [4]: chemicals.phase_change.phase_change_data_Alibakhshi_Cs Out[4]:

Chemical C
CAS
\begin{tabular}{lrr}
\(50-00-0\) & formaldehyde & -26.7916 \\
\(50-21-5\) & lactic acid & 30.5238 \\
\(50-70-4\) & sorbitol & 89.1371 \\
\(50-78-2\) & acetylsalicylic acid & 15.9121 \\
\(50-81-7\) & ascorbic acid & 102.2858 \\
\(\ldots\) & \(\ldots\) & \(\ldots\) \\
\(7642-10-6\) & cis-3-heptene & -17.8032 \\
\(7719-09-7\) & thionyl chloride & -31.2745 \\
\(7719-12-2\) & phosphorus trichloride & -27.0024 \\
\(7783-06-4\) & hydrogen sulfide & -37.3259 \\
\(7783-07-5\) & hydrogen selenide & -38.5320
\end{tabular}
[1890 rows x 2 columns]

\subsection*{1.22 Rachford-Rice Equation Solvers (chemicals.rachford_rice)}

This module contains functions for solving the Rachford-Rice Equation. This is used to solve ideal flashes, and is the inner loop of the sequential-substitution flash algorithm. It is not used by full newton-algorithms. The sequentialsubstitution is normally recommended because it does not suffer from the \(\sim \mathrm{N}^{\wedge} 3\) behavior of solving a matrix.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

\footnotetext{
- Two Phase - Interface
- Two Phase - Implementations
- Two Phase - High-Precision Implementations
- Three Phase
- N Phase
- Two Phase Utility Functions
- Numerical Notes
}

\subsection*{1.22.1 Two Phase - Interface}

\section*{chemicals.rachford_rice.flash_inner_loop (zs, Ks, method=None, guess=None, check=False)}

This function handles the solution of the inner loop of a flash calculation, solving for liquid and gas mole fractions and vapor fraction based on specified overall mole fractions and K values. As K values are weak functions of composition, this should be called repeatedly by an outer loop. Will automatically select an algorithm to use if no method is provided. Should always provide a solution.
The automatic algorithm selection will try an analytical solution, and use the Rachford-Rice method if there are 6 or more components in the mixture.

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float] Equilibrium K-values, [-]
guess [float, optional] Optional initial guess for vapor fraction, [-]
check [bool, optional] Whether or not to check the K values to ensure a positive-composition solution exists, [-]

\section*{Returns}

V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Other Parameters}
method [string, optional] The method name to use. Accepted methods are 'Analytical', 'Rachford-Rice (Secant)', 'Rachford-Rice (Newton-Raphson)', 'Rachford-Rice (Halley)', 'Rachford-Rice (NumPy)', 'Leibovici and Nichita 2', 'Rachford-Rice (polynomial)', and 'Li-Johns-Ahmadi'. All valid values are also held in the list flash_inner_loop_methods.

\section*{Notes}

A total of eight methods are available for this function. They are:
- 'Analytical', an exact solution derived with SymPy, applicable only only to mixtures of two, three, or four components
- 'Rachford-Rice (Secant)', 'Rachford-Rice (Newton-Raphson)', 'Rachford-Rice (Halley)', or 'RachfordRice (NumPy)', which numerically solves an objective function described in Rachford_Rice_solution.
- 'Leibovici and Nichita 2', a transformation of the RR equation described in Rachford_Rice_solution_LN2.
- 'Li-Johns-Ahmadi', which numerically solves an objective function described in Li_Johns_Ahmadi_solution.
- 'Leibovici and Neoschil', which numerically solves an objective function described in Rachford_Rice_solution_Leibovici_Neoschil.

\section*{Examples}
>>> flash_inner_loop(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
(0.6907302627738, [0.3394086969663, 0.3650560590371, 0.29553524399648], [0. \(\rightarrow 571903654388,0.27087159580558,0.1572247498061])\)

\section*{chemicals.rachford_rice.flash_inner_loop_methods( \(N\) )}

Return all methods able to solve the Rachford-Rice equation for the specified number of components.

\section*{Parameters}
\(\mathbf{N}\) [int] Number of components, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to solve the Rachford-rice equation
See also:
flash_inner_loop
chemicals.rachford_rice.flash_inner_loop_all_methods = ('Analytical', 'Rachford-Rice (Secant)', 'Rachford-Rice (Newton-Raphson)', 'Rachford-Rice (Halley)', 'Rachford-Rice (NumPy)', 'Li-Johns-Ahmadi', 'Rachford-Rice (polynomial)', 'Leibovici and Nichita 2', 'Leibovici and Neoschil')

Tuple of method name keys. See the flash_inner_loop for the actual references

\subsection*{1.22.2 Two Phase - Implementations}
chemicals.rachford_rice.Rachford_Rice_solution(zs, Ks, fprime=False, fprime \(2=\) False, guess=None)
Solves the objective function of the Rachford-Rice flash equation [1]. Uses the method proposed in [2] to obtain an initial guess.
\[
\sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0
\]

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float]] Equilibrium K-values, [-]
fprime [bool, optional] Whether or not to use the first derivative of the objective function in the solver (Newton-Raphson is used) or not (secant is used), [-]
fprime 2 [bool, optional] Whether or not to use the second derivative of the objective function in the solver (parabolic Halley`s method is used if True) or not, [-]
guess [float, optional] Optional initial guess for vapor fraction, [-]

\section*{Returns}

V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

The initial guess is the average of the following, as described in [2].
\[
\begin{gathered}
\left(\frac{V}{F}\right)_{\min }=\frac{\left(K_{\max }-K_{\min }\right) z_{o f} K_{\max }-\left(1-K_{\min }\right)}{\left(1-K_{\min }\right)\left(K_{\max }-1\right)} \\
\left(\frac{V}{F}\right)_{\max }=\frac{1}{1-K_{\min }}
\end{gathered}
\]

Another algorithm for determining the range of the correct solution is given in [3]; [2] provides a narrower range however. For both cases, each guess should be limited to be between 0 and 1 as they are often negative or larger than 1.
\[
\begin{aligned}
& \left(\frac{V}{F}\right)_{\min }=\frac{1}{1-K_{\max }} \\
& \left(\frac{V}{F}\right)_{\max }=\frac{1}{1-K_{\min }}
\end{aligned}
\]

If the newton method does not converge, a bisection method (brenth) is used instead. However, it is somewhat slower, especially as newton will attempt 50 iterations before giving up.

In all benchmarks attempted, secant method provides better performance than Newton-Raphson or parabolic Halley`s method. This may not be generally true; but it is for Python and SciPy's implementation. They are implemented for benchmarking purposes.

The first and second derivatives are:
\[
\begin{aligned}
\frac{d \text { obj }}{d \frac{V}{F}} & =\sum_{i} \frac{-z_{i}\left(K_{i}-1\right)^{2}}{\left(1+\frac{V}{F}\left(K_{i}-1\right)\right)^{2}} \\
\frac{d^{2} \mathrm{obj}}{d\left(\frac{V}{F}\right)^{2}} & =\sum_{i} \frac{2 z_{i}\left(K_{i}-1\right)^{3}}{\left(1+\frac{V}{F}\left(K_{i}-1\right)\right)^{3}}
\end{aligned}
\]

\section*{References}
[1], [2], [3]

\section*{Examples}
>>> Rachford_Rice_solution(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
(0.6907302627738544, [0.33940869696634357, 0.3650560590371706, 0.2955352439964858], ь \(\hookrightarrow[0.5719036543882889,0.27087159580558057,0.15722474980613044])\)
chemicals.rachford_rice.Rachford_Rice_solution_LN2 ( \(z s\), Ks, guess=None)
Solves the a objective function for the Rachford-Rice flash equation according to the Leibovici and Nichita (2010) transformation (method 2). This transformation makes the only zero of the function be the desired one. Consequently, higher-order methods may be used to solve this equation. Halley's (second derivative) method is found to be the best; typically needing \(\sim 50 \%\) fewer iterations than the RR formulation with Secant method.
\[
\begin{gathered}
H(y)=\sum_{i}^{n} \frac{z_{i}}{\lambda-c_{i}}=0 \\
\lambda=c_{k}+\frac{c_{k+1}-c_{k}}{1+e^{-y}}
\end{gathered}
\]
\[
\begin{aligned}
c_{i} & =\frac{1}{1-K_{i}} \\
c_{k} & =\left(\frac{V}{F}\right)_{\min } \\
c_{k+1} & =\left(\frac{V}{F}\right)_{\max }
\end{aligned}
\]

Note the two different uses of \(c\) in the above equation, confusingly given in [1]. lambda is the vapor fraction.
Once the equation has been solved for \(y\), the vapor fraction can be calculated outside the solver.

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float]] Equilibrium K-values, [-]
guess [float, optional] Optional initial guess for vapor fraction, [-]

\section*{Returns}

V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

The initial guess is the average of the following, as described in [2].
\[
\begin{gathered}
\left(\frac{V}{F}\right)_{\min }=\frac{\left(K_{\max }-K_{\min }\right) z_{o f} K_{\max }-\left(1-K_{\min }\right)}{\left(1-K_{\min }\right)\left(K_{\max }-1\right)} \\
\left(\frac{V}{F}\right)_{\max }=\frac{1}{1-K_{\min }}
\end{gathered}
\]

The first and second derivatives are derived with sympy as follows:
```

>>> from sympy import *
>>> VF_min, VF_max, ai, ci, y = symbols('VF_min, VF_max, ai, ci, y')
>>> V_over_F = (VF_min + (VF_max - VF_min)/(1 + exp(-y)))
>>> F = ai/(V_over_F - ci)
>>> terms = [F, diff(F, y), diff(F, y, 2)]
>>> cse(terms, optimizations='basic')

```

Some helpful information about this transformation can also be found in [3].

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> Rachford_Rice_solution_LN2(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
(0.6907302627738, [0.3394086969663, 0.3650560590371, 0.29553524399648], [0.
\hookrightarrow71903654388, 0.27087159580558, 0.1572247498061])

```

\section*{chemicals.rachford_rice.Li_Johns_Ahmadi_solution(zs, Ks, guess=None)}

Solves the objective function of the Li-Johns-Ahmadi flash equation. Uses the method proposed in [1] to obtain an initial guess.
\[
0=1+\left(\frac{K_{\max }-K_{\min }}{K_{\min }-1}\right) x_{\max }+\sum_{i=2}^{n-1} \frac{K_{i}-K_{\min }}{K_{\min }-1}\left[\frac{z_{i}\left(K_{\max }-1\right) x_{\max }}{\left(K_{i}-1\right) z_{\max }+\left(K_{\max }-K_{i}\right) x_{\max }}\right]
\]

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float]] Equilibrium K-values, [-]

\section*{Returns}

V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

The initial guess is the average of the following, as described in [1]. Each guess should be limited to be between 0 and 1 as they are often negative or larger than 1. max refers to the corresponding mole fractions for the species with the largest K value.
\[
\left(\frac{1-K_{\min }}{K_{\max }-K_{\min }}\right) z_{\max } \leq x_{\max } \leq\left(\frac{1-K_{\min }}{K_{\max }-K_{\min }}\right)
\]

If the newton method does not converge, a bisection method (brenth) is used instead. However, it is somewhat slower, especially as newton will attempt 50 iterations before giving up.

This method does not work for problems of only two components. K values are sorted internally. Has not been found to be quicker than the Rachford-Rice equation.

\section*{References}
[1]

\section*{Examples}
```

>>> Li_Johns_Ahmadi_solution(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
(0.6907302627738544, [0.33940869696634357, 0.3650560590371706, 0.2955352439964858],,
\rightarrow [ 0 . 5 7 1 9 0 3 6 5 4 3 8 8 2 8 8 9 , ~ 0 . 2 7 0 8 7 1 5 9 5 8 0 5 5 8 0 5 7 , ~ 0 . 1 5 7 2 2 4 7 4 9 8 0 6 1 3 0 4 4 ] ) ~

```
chemicals.rachford_rice.Rachford_Rice_solution_Leibovici_Neoschil(zs, Ks, guess=None)
Solves the objective function of the Rachford-Rice flash equation as modified by Leibovici and Neoschil. This modification helps convergence near the vapor fraction boundaries only; it slows convergence in other regions.
\[
\begin{gathered}
\left(\frac{V}{F}-\alpha_{L}\right)\left(\alpha_{R}-\frac{V}{F}\right) \sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0 \\
\alpha_{L}=-\frac{1}{K_{\max }-1} \\
\alpha_{R}=\frac{1}{1-K_{\min }}
\end{gathered}
\]

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float] Equilibrium K-values, [-]
guess [float, optional] Optional initial guess for vapor fraction, [-]

\section*{Returns}

L_over_F [float] Liquid fraction solution [-]
V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

The initial guess is the average of the following.
\[
\begin{gathered}
\left(\frac{V}{F}\right)_{\min }=\frac{\left(K_{\max }-K_{\min }\right) z_{o f} K_{\max }-\left(1-K_{\min }\right)}{\left(1-K_{\min }\right)\left(K_{\max }-1\right)} \\
\left(\frac{V}{F}\right)_{\max }=\frac{1}{1-K_{\min }}
\end{gathered}
\]

\section*{References}
[1]

\section*{Examples}
```

>>> Rachford_Rice_solution_Leibovici_Neoschil(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742,ь
@0.532])
(0.3092697372261, 0.69073026277385, [0.339408696966343, 0.36505605903717, 0.
\rightarrow 2 9 5 5 3 5 2 4 3 9 9 6 4 8 ] , ~ [ 0 . 5 7 1 9 0 3 6 5 4 3 8 8 2 8 , ~ 0 . 2 7 0 8 7 1 5 9 5 8 0 5 5 8 0 , ~ 0 . 1 5 7 2 2 4 7 4 9 8 0 6 1 3 0 ] ) ~ ( \% )

```
chemicals.rachford_rice.Rachford_Rice_solution_polynomial( \(z s, K s\) )
Solves the Rachford-Rice equation by transforming it into a polynomial, and then either analytically calculating the roots, or, using the known range the correct root is in, numerically solving for the correct polynomial root. The analytical solutions are used for N from 2 to 4.

Uses the method proposed in [2] to obtain an initial guess when solving the polynomial for the root numerically.
\[
\sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0
\]

Warning: : Using this function with more than 20 components is likely to crash Python! This model does not work well with many components!

This method, developed first in [3] and expanded in [1], is clever but of little use for large numbers of components.

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float] Equilibrium K-values, [-]

\section*{Returns}

V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

This approach has mostly been ignored by academia, despite some of its advantages.
The initial guess is the average of the following, as described in [2].
\[
\begin{gathered}
\left(\frac{V}{F}\right)_{\min }=\frac{\left(K_{\max }-K_{\min }\right) z_{o f} K_{\max }-\left(1-K_{\min }\right)}{\left(1-K_{\min }\right)\left(K_{\max }-1\right)} \\
\left(\frac{V}{F}\right)_{\max }=\frac{1}{1-K_{\min }}
\end{gathered}
\]

If the newton method does not converge, a bisection method (brenth) is used instead. However, it is somewhat slower, especially as newton will attempt 50 iterations before giving up.

This method could be speed up somewhat for \(\mathrm{N}<=4\); the checks for the vapor fraction range are not really needed.

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> Rachford_Rice_solution_polynomial(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
(0.6907302627738543, [0.33940869696634357, 0.3650560590371706, 0.2955352439964858],的
\rightarrow [ 0 . 5 7 1 9 0 3 6 5 4 3 8 8 2 8 8 9 , ~ 0 . 2 7 0 8 7 1 5 9 5 8 0 5 5 8 0 5 7 , ~ 0 . 1 5 7 2 2 4 7 4 9 8 0 6 1 3 0 4 4 ] ) ~ ( )

```

\subsection*{1.22.3 Two Phase - High-Precision Implementations}
chemicals.rachford_rice.Rachford_Rice_solution_mpmath ( \(z s, K s, d p s=200\), tol=le-100)
Solves the the Rachford-Rice flash equation using numerical root-finding to a high precision using the mpmath library.
\[
\sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0
\]

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float] Equilibrium K-values, [-]
dps [int, optional] Number of decimal places to use in the intermediate values of the calculation, [-]
tol [float, optional] The tolerance of the solver used in mpmath, [-]

\section*{Returns}

L_over_F [float] Liquid fraction solution [-]
V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

This function is written solely for development purposes with the aim of returning bit-accurate solutions.
Note that the liquid fraction is also returned; it is insufficient to compute it as \(\frac{L}{F}=1-\frac{V}{F}\).

\section*{Examples}
```

>>> Rachford_Rice_solution_mpmath(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
(0.3092697372261456, 0.6907302627738544, [0.33940869696634357, 0.3650560590371706,0
\rightarrow 0 . 2 9 5 5 3 5 2 4 3 9 9 6 4 8 5 8 4 ] , ~ [ 0 . 5 7 1 9 0 3 6 5 4 3 8 8 2 8 8 9 , ~ 0 . 2 7 0 8 7 1 5 9 5 8 0 5 5 8 0 5 7 , ~ 0 .
415722474980613046])
>>> Rachford_Rice_solution_mpmath(zs=[0.9999999999999, 1e-12], Ks=[2.0, 1e-12])
(1e-12, 0.9999999999999, [0.49999999999975003, 0.50000000000025], [0.
\leftrightarrows9999999999995001, 5.0000000000025e-13])

```
chemicals.rachford_rice.Rachford_Rice_solution_binary_dd (zs, Ks)
Solves the the Rachford-Rice flash equation for a binary system using double-double math. This increases the range in which the calculation can be performed accurately but does not totally eliminate error.
\[
\sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0
\]

The analytical solution for a binary system is:
\[
\frac{V}{F}=\frac{-K_{0} z_{0}-K_{1} z_{1}+z_{0}+z_{1}}{K_{0} K_{1} z_{0}+K_{0} K_{1} z_{1}-K_{0} z_{0}-K_{0} z_{1}-K_{1} z_{0}-K_{1} z_{1}+z_{0}+z_{1}}
\]

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float]] Equilibrium K-values, [-]

\section*{Returns}

L_over_F [float] Liquid fraction solution [-]
V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Examples}

This system with large volatility difference and a trace of a component shows a correct calculation. Try it out with other solvers for bad results!
```

>>> Rachford_Rice_solution_binary_dd(zs=[1E-27, 1.0], Ks=[10000000000000,0.1])
(1.000000000001, -1.0000000000009988e-12, [9.0000000000009e-13, 0.9999999999991],,
\rightarrow [ 0 . 9 0 0 0 0 0 0 0 0 0 0 0 0 9 , ~ 0 . 0 9 9 9 9 9 9 9 9 9 9 9 9 1 0 0 1 ] ) ~ ( )

```

Note the limitations of this solver can be explored by comparing against Rachford_Rice_solution_mpmath. For example, with \(z 0\) of 1e-28 in the above example error creeps back in.
chemicals.rachford_rice.Rachford_Rice_solution_Leibovici_Neoschil_dd(zs,Ks, guess=None)
Solves the objective function of the Rachford-Rice flash equation as modified by Leibovici and Neoschil, using double-double precision math for maximum accuracy. For most cases, this function will return bit-for-bit accurate results; but there are pathological inputs where error still occurs.
\[
\begin{aligned}
&\left(\frac{V}{F}-\alpha_{L}\right)\left(\alpha_{R}-\frac{V}{F}\right) \sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0 \\
& \alpha_{L}=-\frac{1}{K_{\max }-1} \\
& \alpha_{R}=\frac{1}{1-K_{\min }}
\end{aligned}
\]

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float] Equilibrium K-values, [-]
guess [float, optional] Optional initial guess for vapor fraction, [-]

\section*{Returns}

L_over_F [float] Liquid fraction solution [-]
V_over_F [float] Vapor fraction solution [-]
xs [list[float]] Mole fractions of each species in the liquid phase, [-]
ys [list[float]] Mole fractions of each species in the vapor phase, [-]

\section*{Notes}

The initial guess is the average of the following.
\[
\begin{aligned}
\left(\frac{V}{F}\right)_{\min }= & \frac{\left(K_{\max }-K_{\min }\right) z_{o f} K_{\max }-\left(1-K_{\min }\right)}{\left(1-K_{\min }\right)\left(K_{\max }-1\right)} \\
& \left(\frac{V}{F}\right)_{\max }=\frac{1}{1-K_{\min }}
\end{aligned}
\]

\section*{References}
[1]

\section*{Examples}
```

>>> Rachford_Rice_solution_Leibovici_Neoschil_dd(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.
๑742, 0.532])
(0.3092697372261, 0.69073026277385, [0.339408696966343, 0.36505605903717, 0.
\hookrightarrow29553524399648], [0.57190365438828, 0.270871595805580, 0.157224749806130])

```

\subsection*{1.22.4 Three Phase}
chemicals.rachford_rice.Rachford_Rice_solution2 ( \(n s, K s s_{-} y, K s \_z, b e t a \_y=0.5\), beta_z=1e-06)
Solves the two objective functions of the Rachford-Rice flash equation for a three-phase system. Initial guesses are required for both phase fractions, beta_y and beta_z. The Newton method is used, with an analytical Jacobian.
\[
\begin{aligned}
& F_{0}=\sum_{i} \frac{z_{i}\left(K_{y}-1\right)}{1+\beta_{y}\left(K_{y}-1\right)+\beta_{z}\left(K_{z}-1\right)}=0 \\
& F_{1}=\sum_{i} \frac{z_{i}\left(K_{z}-1\right)}{1+\beta_{y}\left(K_{y}-1\right)+\beta_{z}\left(K_{z}-1\right)}=0
\end{aligned}
\]

\section*{Parameters}
ns [list[float]] Overall mole fractions of all species (would be \(z s\) except that is conventially used for one of the three phases), [-]
Ks_y [list[float]] Equilibrium K-values of \(y\) phase to \(x\) phase, [-]
Ks_z [list[float]] Equilibrium K-values of \(z\) phase to \(x\) phase, [-]
beta_y [float, optional] Initial guess for \(y\) phase (between 0 and 1), [-]
beta_z [float, optional] Initial guess for \(z\) phase (between 0 and 1 ), [-]

\section*{Returns}
beta_y [float] Phase fraction of \(y\) phase, [-]
beta_z [float] Phase fraction of \(z\) phase, [-]
\(\mathbf{x s}\) [list[float]] Mole fractions of each species in the \(x\) phase, [-]
ys [list[float]] Mole fractions of each species in the \(y\) phase, [-]
zs [list[float]] Mole fractions of each species in the \(z\) phase, [-]

\section*{Notes}

The elements of the Jacobian are calculated as follows:
\[
\begin{gathered}
\frac{\partial F_{0}}{\partial \beta_{y}}=\sum_{i} \frac{-z_{i}\left(K_{y}-1\right)^{2}}{\left(1+\beta_{y}\left(K_{y}-1\right)+\beta_{z}\left(K_{z}-1\right)\right)^{2}} \\
\frac{\partial F_{1}}{\partial \beta_{z}}=\sum_{i} \frac{-z_{i}\left(K_{z}-1\right)^{2}}{\left(1+\beta_{y}\left(K_{y}-1\right)+\beta_{z}\left(K_{z}-1\right)\right)^{2}} \\
\frac{\partial F_{1}}{\partial \beta_{y}}=\sum_{i} \frac{\partial F_{0}}{\partial \beta_{z}}=\frac{-z_{i}\left(K_{z}-1\right)\left(K_{y}-1\right)}{\left(1+\beta_{y}\left(K_{y}-1\right)+\beta_{z}\left(K_{z}-1\right)\right)^{2}}
\end{gathered}
\]

In general, the solution which Newton's method converges to may not be the desired one, so further constraints are required.
Okuno's method in [1] provides a polygonal region where the correct answer lies. It has not been implemented.
The Leibovici and Neoschil method [4] provides a method to compute/update the damping parameter, which is suposed to ensure convergence. It claims to be able to calculate the maximum damping factor for Newton's method, if it tries to go out of bounds.

A custom region which is believed to be the same as that of Okuno is implemented instead - the region which ensures positive compositions for all compounds in all phases, but does not restrict the phase fractions to be between 0 and 1 or even positive.

With the convergence restraint, it is believed if a solution lies within \((0,1)\) for both variables, the correct solution will be converged to so long as the initial guesses are within the correct region.
Some helpful information has also been found in [2] and [3].

\section*{References}
[1], [2], [3], [4]

\section*{Examples}
```

>>> ns = [0.204322076984, 0.070970999150, 0.267194323384, 0.296291964579, 0.
๑067046080882, 0.062489248292, 0.031685306730]
>>> Ks_y = [1.23466988745, 0.89727701141, 2.29525708098, 1.58954899888, 0.
43349348597, 0.02038108640, 1.40715641002]
>>> Ks_z = [1.52713341421, 0.02456487977, 1.46348240453, 1.16090546194, 0.
๑24166289908, 0.14815282572, 14.3128010831]
>>> Rachford_Rice_solution2(ns, Ks_y, Ks_z, beta_y=.1, beta_z=.6)
(0.6868328915094766, 0.06019424397668606, [0.1712804659711611, 0.08150738616425436, -
\rightarrow 0 . 1 3 9 3 4 3 3 9 4 9 1 9 3 1 8 8 , ~ 0 . 2 0 9 4 5 1 7 5 3 8 7 7 0 3 2 1 3 , ~ 0 . 1 5 6 6 8 9 7 7 7 8 4 0 2 7 8 9 3 , ~ 0 . 2 2 6 5 0 1 2 3 8 5 1 7 1 8 0 0 7 ,
@.015225982711774586], [0.21147483364299702, 0.07313470386530294, 0.
\hookrightarrow1982891387635903, 0.33293382568889657, 0.036586042443791586, 0.
\hookrightarrow004616341311925655, 0.02142533917172731], [0.26156812278601893, 0.
๑00200221914149187, 0.20392660665189805, 0.2431536850887592, 0.03786610596908295,稚
๑0.03355679851539993, 0.21792646184834918])

```

\subsection*{1.22.5 N Phase}

\section*{chemicals.rachford_rice.Rachford_Rice_solutionN(ns, Ks, betas)}

Solves the (phases -1) objectives functions of the Rachford-Rice flash equation for an N -phase system. Initial guesses are required for all phase fractions except the last. The Newton method is used, with an analytical Jacobian.

\section*{Parameters}
ns [list[float]] Overall mole fractions of all species, [-]
Ks [list[list[float]]] Equilibrium K-values of all phases with respect to the \(x\) (reference) phase, [-]
betas [list[float]] Phase fraction initial guesses only for the first N-1 phases; each value corresponds to the phase fraction of each set of the K values; if a phase fraction is specified for the last phase as well, it is ignored [-]

\section*{Returns}
betas [list[float]] Phase fractions of all of the phases; one each for each \(K\) value set given, plus the reference phase phase fraction [-]
compositions [list[list[float]]] Mole fractions of each species in each phase; order each phase in the same order as the K values were provided, and then the \(x\) phase last, which was the reference phase [-]

\section*{Notes}

This algorithm has been used without issue for 4 and 5 phase flashes.
Some helpful information was found in [1], although this method does not follow it exactly.

\section*{References}
[1]

\section*{Examples}
```

>>> ns = [0.204322076984, 0.070970999150, 0.267194323384, 0.296291964579,0.
@067046080882, 0.062489248292,0.031685306730]
>>> Ks_y = [1.23466988745, 0.89727701141, 2.29525708098, 1.58954899888, 0.
\rightarrow 2 3 3 4 9 3 4 8 5 9 7 , ~ 0 . 0 2 0 3 8 1 0 8 6 4 0 , ~ 1 . 4 0 7 1 5 6 4 1 0 0 2 ] ~
>>> Ks_z = [1.52713341421, 0.02456487977, 1.46348240453, 1.16090546194, 0.
\hookrightarrow4166289908, 0.14815282572, 14.3128010831]
>>> Rachford_Rice_solutionN(ns, [Ks_y, Ks_z], [.1, .6])
([0.6868328915094767, 0.06019424397668605, 0.25297286451383727], [[0.
\hookrightarrow21147483364299702, 0.07313470386530294, 0.3198289138763589, 0.332933825688889657,七
\rightarrow 0 . 0 3 6 5 8 6 0 4 2 4 4 3 7 9 1 5 9 , ~ 0 . 0 0 4 6 1 6 3 4 1 3 1 1 9 2 5 6 5 7 , ~ 0 . 0 2 1 4 2 5 3 3 9 1 7 1 7 2 7 3 1 ] , ~ [ 0 . ]
\hookrightarrow26156812278601893, 0.00200221914149187, 0.203926606651898, 0.2431536850887592,0.
->03786610596908296, 0.033556798515399944, 0.21792646184834918], [0.
๑1712804659711611, 0.08150738616425436, 0.13934339491931877, 0.20945175387703213,馆
๑0.15668977784027896, 0.22650123851718015, 0.015225982711774586]])

```

\subsection*{1.22.6 Two Phase Utility Functions}

\section*{chemicals.rachford_rice.Rachford_Rice_polynomial ( \(z s, K s\) )}

Transforms the Rachford-Rice equation into a polynomial and returns its coefficients. A spelled-out solution is used for N from 2 to 5, derived with SymPy and optimized with the common sub expression approach.

Warning: For large numbers of components ( \(>20\) ) this model performs terribly, though with future optimization it may be possible to have better performance.
\[
\begin{gathered}
\sum_{i=1}^{N} z_{i} C_{i}\left[\Pi_{j \neq i}^{N}\left(1+\frac{V}{F} C_{j}\right)\right]=0 \\
C_{i}=K_{i}-1.0
\end{gathered}
\]

Once the above calculation is performed, it must be rearranged into polynomial form.

\section*{Parameters}
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float]] Equilibrium K-values, [-]

\section*{Returns}
coeffs [float] Coefficients, with earlier coefficients corresponding to higher powers, [-]

\section*{Notes}

Explicit calculations for any degree can be obtained with SymPy, changing N as desired:
```

>>> from sympy import *
>>> N = 4
>>> Cs = symbols('CQ:' + str(N))
>>> zs = symbols('z0:' + str(N))
>>> alpha = symbols('alpha')
>>> tot = 0
>>> for i in range(N):
... mult_sum = 1
>>> for j in range(N):
.." if j != i:
\#." mult_sum *= (1 + alpha*Cs[j])
... tot += zs[i]*Cs[i]*mult_sum

```
poly_expr = poly(expand(tot), alpha) coeff_list = poly_expr.all_coeffs() cse(coeff_list, optimizations='basic')
[1] suggests a matrix-math based approach for solving the model, but that has not been performed here. [1] also has explicit equations for up to \(\mathrm{N}=7\) to derive the coefficients.
The general form was derived to be slightly different than that in [1], but is confirmed to also be correct as it matches other methods for solving the Rachford-Rice equation. [2] has similar information to [1].

The first coefficient is always 1 .
The approach is also discussed in [3], with one example.

\section*{References}
[1], [2], [3]

\section*{Examples}
>>> Rachford_Rice_polynomial(zs=[0.5, 0.3, 0.2], Ks=[1.685, 0.742, 0.532])
[1.0, -3.6926529966760824, 2.073518878815093]
chemicals.rachford_rice.Rachford_Rice_flash_error (V_over_F, \(z s, K s\) )
Calculates the objective function of the Rachford-Rice flash equation. This function should be called by a solver seeking a solution to a flash calculation. The unknown variable is \(V_{-}\)over_ \(F\), for which a solution must be between 0 and 1.
\[
\sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0
\]

\section*{Parameters}

V_over_F [float] Vapor fraction guess [-]
zs [list[float]] Overall mole fractions of all species, [-]
Ks [list[float]] Equilibrium K-values, [-]

\section*{Returns}
error [float] Deviation between the objective function at the correct V_over_F and the attempted V_over_F, [-]

\section*{Notes}

The derivation is as follows:
\[
\begin{gathered}
F z_{i}=L x_{i}+V y_{i} \\
x_{i}=\frac{z_{i}}{1+\frac{V}{F}\left(K_{i}-1\right)} \\
\sum_{i} y_{i}=\sum_{i} K_{i} x_{i}=1 \\
\sum_{i}\left(y_{i}-x_{i}\right)=0 \\
\sum_{i} \frac{z_{i}\left(K_{i}-1\right)}{1+\frac{V}{F}\left(K_{i}-1\right)}=0
\end{gathered}
\]

This objective function was proposed in [1].

\section*{References}
[1]

\section*{Examples}
```

>>> Rachford_Rice_flash_error(0.5, zs=[0.5, 0.3, 0.2],
\#Ks=[1.685, 0.742, 0.532])
0.04406445591174976

```

\subsection*{1.22.7 Numerical Notes}

For the two-phase problem, there are the following ways of computing the vapor and liquid mole fractions once the vapor fraction and liquid fraction has been computed:

The most commonly shown expression is:
\[
x_{i}=\frac{z_{i}}{1+\frac{V}{F}\left(K_{i}-1\right)}
\]

This can cause numerical issues when \(K_{i}\) is near 1 . It also shows issues near \(\frac{V}{F}\left(K_{i}-1\right)=-1\).
Another expression which avoids the second issue is
\[
x_{i}=\frac{z_{i}}{\frac{L}{F}+\left(1-\frac{L}{F}\right) K_{i}}
\]

Much like the other expression above this numerical issues but at different conditions: \(\frac{L}{F}=1\) and \(\frac{L}{F}=-\left(1-\frac{L}{F}\right) K_{i}\). One more expression using both liquid and vapor fraction is:
\[
x_{i}=\frac{z_{i}}{K_{i} \frac{V}{F}+\frac{L}{F}}
\]

This expression only has one problematic area: \(K_{i} \frac{V}{F}=\frac{L}{F}\). Preferably, this is computed with a fused-multiply-add operation.

Another expression which flips the K value into the liquid form and swaps the vapor fraction for the liquid fraction in-line is as follows
\[
x_{i}=\frac{\frac{z_{i}}{K_{i}}}{\frac{\frac{L}{F}}{K_{i}}+\frac{V}{F}}
\]

This also has numerical problems when \(-\frac{\frac{L}{F}}{K_{i}}=\frac{V}{F}\).
Even when computing a solution with high precision such as with mpmath, the resulting compositions and phase fractions may fail basic tests. In the following case, a nasty problem has a low-composition but relatively volatile last component. Mathematically, \(1=\frac{\frac{L}{F} x_{i}+\frac{V}{F} y_{i}}{z_{i}}\). This is true for all components except the last one in this case, where significant error exists.
```

>>> zs = [0.004632150100959984, 0.019748784459594933, 0.0037494212674659875, 0.
\hookrightarrow 0 0 5 0 4 9 2 8 1 5 0 3 3 6 4 9 8 3 5 , ~ 7 . 0 4 9 8 1 8 2 8 4 2 0 1 6 3 6 e - 0 5 , ~ 0 . 0 1 9 2 5 2 9 4 1 3 0 9 1 8 4 9 3 7 , 0 . 0 2 2 9 2 3 0 6 8 7 3 3 2 3 3 9 2 3 ,
\hookrightarrow.02751809363371991,0.044055273670258854, 0.026348159124199914,0.029384949788372902,
\hookrightarrow0.022368938441593926, 0.03876345111451487, 0.03440715821883388, 0.04220510198067186,0
\hookrightarrow.04109191458414686, 0.031180945124537895, 0.024703227642798916, 0.010618543295340965, ь
\leftrightarrow 0 . 0 4 3 2 6 2 4 4 2 1 6 1 0 0 3 8 5 4 , ~ 0 . 0 0 6 7 7 4 9 2 2 6 5 0 3 1 1 9 7 7 , ~ 0 . 0 2 4 1 8 0 9 0 7 8 8 2 6 2 3 9 2 , ~ 0 . 0 3 3 1 6 8 2 7 8 0 5 2 0 7 7 8 8 6 , ~ ᄂ , ~
\hookrightarrow.03325881573680989, 0.027794535589044905, 0.00302091746847699,0.013693571363003955, -
\hookrightarrow.043274465132840854, 0.02431371852108292, 0.004119055065872986,0.03314056562191489, - , 0
\hookrightarrow \mp@code { @ . 0 3 9 2 6 5 1 1 1 8 2 8 9 5 0 8 7 , ~ 0 . 0 3 0 5 0 6 8 0 4 8 0 4 6 1 5 9 , ~ 0 . 0 1 4 4 9 5 3 1 7 9 2 2 1 2 6 9 5 2 , ~ 0 . 0 3 6 0 3 7 3 7 7 0 7 4 0 9 9 8 8 , 0 . }
\hookrightarrow04346278949361786, 0.019715052322446934, 0.028565255195219907, 0.023343683279902924,0.
@026532427286078915, 2.0833722372767433e-06]
>> Ks = [0.000312001984979, 0.478348350355814, 0.057460349529956,0.142866526725442,0.
\hookrightarrow186076915390803, 1.67832923245552, 0.010784509466239, 0.037204384948088,0.
\hookrightarrow005359146955631, 2.41896552551221, 0.020514598049597, 0.104545054017411, 2.
\hookrightarrow7825397780443, 0.176463709057649, Q.000474240879865, Q.004738042026669, Q.
\hookrightarrow02556030236928, 0.00300089652604, 0.010614774675069, 1.75142303167203, 1.
\hookrightarrow7213647779132, 0.035773024794854, 4.15016401471676, 0.024475125100923, 0.
\hookrightarrow0206952065986, 2.09173484409107, 0.06290795470216, 0.001537212006245, 1.
\hookrightarrow16935817509767, Q.001830422812888, Q.058398776367331, 0.516860928072656, 1.
\hookrightarrow03039372722559, 0.460775800103578, 0.10980302936483, 0.009883724220094, 0.
\hookrightarrow21938589630783, 0.983011657214417, 0.01978995396409, 0.204144939961852, 14.
\hookrightarrow0521979447538]
>>> LF, VF, xs, ys = Rachford_Rice_solution_mpmath(zs=zs, Ks=Ks)
>> (LF*xs[-1] + VF*ys[-1])/zs[-1]
1.0000000000028162

```

\subsection*{1.23 Chemical Reactions (chemicals.reaction)}

This module contains lookup functions enthalpies and standard entropies of formation. Lookup functions are availa for the liquid, solid, and gas states. A compound may be in more than one lookup function.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Solid Heat of Formation
- Liquid Heat of Formation
- Gas Heat of Formation
- Solid Absolute Entropy
- Liquid Absolute Entropy
- Gas Absolute Entropy
- Utility Functions
- Chemical Reactions

\subsection*{1.23.1 Solid Heat of Formation}

\section*{chemicals.reaction.Hfs(CASRN, method=None)}

This function handles the retrieval of a chemical's solid/crystaline standard phase heat of formation. The lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Hfs [float] Solid standard-state heat of formation, [J/mol]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in Hfs_methods

\section*{See also:}

Hfs_methods

\section*{Notes}

Sources are:
- 'CRC', from the CRC handbook (1360 values) [1]
- 'WEBBOOK' (2000 values) [2]

\section*{References}
[1], [2]

\section*{Examples}
>>> Hfs('101-81-5') \# Diphenylmethane
71500.0
chemicals.reaction.Hfs_methods (CASRN)
Return all methods available to obtain the solid-phase heat of formation for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Hfs with the given inputs.
See also:

Hfs
chemicals.reaction.Hfs_all_methods = ('CRC', 'WEBBOOK')
Tuple of method name keys. See the \(H f s\) for the actual references

\subsection*{1.23.2 Liquid Heat of Formation}

\section*{chemicals.reaction. Hfl (CASRN, method=None)}

This function handles the retrieval of a chemical's liquid standard phase heat of formation. The lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Hfl [float] Liquid standard-state heat of formation, [J/mol]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, Hfl_all_methods.

\section*{See also:}

Hfl_methods

\section*{Notes}

Sources are:
- 'ATCT_L', the Active Thermochemical Tables version 1.112. [1]
- 'CRC', from the CRC handbook (1360 values) [2]
- 'WEBBOOK' (2000 values) [3]

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> Hfl('67-56-1')
-238400.0

```
chemicals.reaction.Hfl_methods (CASRN)
Return all methods available to obtain the standard liquid-state heat of formation for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Hfl with the given inputs.

\section*{See also:}

Hfl
```

chemicals.reaction.Hfl_all_methods = ('ATCT_L', 'CRC', 'WEBBOOK', 'JANAF')

```

Tuple of method name keys. See the \(H f\) for the actual references

\subsection*{1.23.3 Gas Heat of Formation}
chemicals.reaction. Hfg (CASRN, method=None)
This function handles the retrieval of a chemical's gas heat of formation. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}

Hfg [float] Ideal gas phase heat of formation, [J/mol]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in Hfg_methods

\section*{See also:}

Hfg_methods

\section*{Notes}

Function has data for approximately 8700 chemicals. Sources are:
- 'ATCT_G’, the Active Thermochemical Tables version 1.112 (600 values) [1]
- 'TRC', from a 1994 compilation (1750 values) [2]
- 'CRC', from the CRC handbook (1360 values) [3]
- 'WEBBOOK', a NIST resource [6] containing mostly experimental and averaged values
- 'JANAF', the 1998 JANAF values online
- 'JOBACK', an estimation method for organic substances in [5]
- 'YAWS', a large compillation of values, mostly estimated (5000 values) [4]
'TRC' data may have come from computational procedures, for example petane is off by \(30 \%\).

\section*{References}
[1], [2], [3], [4], [5], [6]

\section*{Examples}
```

>>> Hfg('67-56-1')
-200700.0
>>> Hfg('67-56-1', method='YAWS')
-200900.0
>>> Hfg('67-56-1', method='CRC')
-201000.0
>>> Hfg('67-56-1', method='TRC')
-190100.0

```
chemicals.reaction.Hfg_methods (CASRN)
Return all methods available to obtain the gas phase heat of formation for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Hfg with the given inputs.

\section*{See also:}
\(H f g\)
```

chemicals.reaction.Hfg_all_methods = ('ATCT_G', 'TRC', 'CRC', 'WEBBOOK', 'JANAF', 'YAWS',
'JOBACK')

```

Tuple of method name keys. See the Hfg for the actual references

\subsection*{1.23.4 Solid Absolute Entropy}

\section*{chemicals.reaction.SOs(CASRN, method=None)}

This function handles the retrieval of a chemical's absolute entropy at a reference temperature of 298.15 K and pressure of 1 bar, in the solid state. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

S0s [float] Ideal gas standard absolute entropy of compound, [J/mol/K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in SOs_all_methods.

\section*{See also:}
```

S0s_methods

```

\section*{Notes}

Sources are:
- 'CRC' [1] from the CRC handbook (1360 values)
- 'WEBBOOK', a NIST resource [2] containing mostly experimental and averaged values

\section*{References}
[1], [2]

\section*{Examples}
>>> S0s('7439-93-2') \# Lithium
29.1

\section*{chemicals.reaction.SOs_methods (CASRN)}

Return all methods available to obtain the absolute entropy of the compound in the solid phase for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the S0s with the given inputs.

\section*{See also:}

SOs
chemicals.reaction.SOs_all_methods = ('CRC', 'WEBBOOK')
Tuple of method name keys. See the \(S 0 s\) for the actual references

\subsection*{1.23.5 Liquid Absolute Entropy}
chemicals.reaction.SO1 (CASRN, method=None)
This function handles the retrieval of a chemical's absolute entropy at a reference temperature of 298.15 K and pressure of 1 bar, in the liquid state.

Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

S01 [float] Ideal gas standard absolute entropy of compound, [J/mol/K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, Sol_all_methods.
See also:

SO1_methods

\section*{Notes}

Sources are:
- 'CRC', from the CRC handbook

\section*{References}
[1]

\section*{Examples}
>>> SOl('7439-97-6') \# Mercury
75.9

\section*{chemicals.reaction.SOl_methods(CASRN)}

Return all methods available to obtain the absolute entropy for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the S 01 with the given inputs.
See also:

S01
chemicals.reaction.SOl_all_methods = ('CRC', 'WEBBOOK', 'JANAF')
Tuple of method name keys. See the \(S 0 l\) for the actual references

\subsection*{1.23.6 Gas Absolute Entropy}
chemicals.reaction. \(\mathbf{S O g}\) (CASRN, method=None)
This function handles the retrieval of a chemical's absolute entropy at a reference temperature of 298.15 K and pressure of 1 bar, in the ideal gas state.

Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}
\(\mathbf{S 0 g}\) [float] Ideal gas standard absolute entropy of compound, [J/mol/K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, SOg_all_methods

See also:

\section*{SOg_methods}

\section*{Notes}

Function has data for approximately 5400 chemicals. Sources are:
- 'CRC', from the CRC handbook (520 values)
- 'YAWS', a large compillation of values, mostly estimated (4890 values)
- 'WEBBOOK', a NIST resource [3] containing mostly experimental and averaged values

\section*{References}
[1], [2], [3]

\section*{Examples}
>>> SOg('67-56-1')
239.9
>>> SOg('67-56-1', method='YAWS')
239.88

\section*{chemicals.reaction.SOg_methods(CASRN)}

Return all methods available to obtain the S 0 g for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the SOg with the given inputs.
See also:

SOg
chemicals.reaction.SOg_all_methods = ('CRC', 'WEBBOOK', 'JANAF', 'YAWS')
Tuple of method name keys. See the \(S O g\) for the actual references

\subsection*{1.23.7 Utility Functions}
chemicals.reaction.Gibbs_formation (dHf, SO_abs, dHfs_std, SO_abs_elements, coeffs_elements, T_ref=298.15)
This function calculates the Gibbs free energy of formation of a compound, from its constituent elements.
The calculated value will be for a "standard-state" value if \(d H f\) and \(S O \_a b s\) are provided in the standard state; or it will be in an "ideal gas" basis if they are both for an ideal gas. For compounds which are gases at STP, the two values are the same.

\section*{Parameters}
dHf [float] Molar enthalpy of formation of the created compound, [J/mol]
S0_abs [float] Absolute molar entropy of the created compound at the reference temperature, [J/mol/K]
dHfs_std [list[float]] List of standard molar enthalpies of formation of all elements used in the formation of the created compound, [J/mol]
S0_abs_elements [list[float]] List of standard absolute molar entropies at the reference temperature of all elements used in the formation of the created compound, [ \(\mathrm{J} / \mathrm{mol} / \mathrm{K}\) ]
coeffs_elements [list[float]] List of coefficients for each compound (i.e. 1 for C, 2 for H 2 if the target is methane), in the same order as \(d H f s_{-} s t d\) and SO_abs_elements, [-]

T_ref [float, optional] The standard state temperature, default 298.15 K ; few values are tabulated at other temperatures, [-]

\section*{Returns}
dGf [float] Gibbs free energy of formation for the created compound, [J/mol]

\section*{Notes}

Be careful for elements like Bromine - is the tabulated value for Br 2 or Br ?

\section*{References}
[1]

\section*{Examples}

Calculate the standard-state Gibbs free energy of formation for water, using water's standard state heat of formation and absolute entropy at 298.15 K :
```

>>> Gibbs_formation(-285830, 69.91, [0, 0], [130.571, 205.147], [1, .5])
-237161.633825

```

Calculate the ideal-gas state Gibbs free energy of formation for water, using water's ideal-gas state heat of formation and absolute entropy at 298.15 K as a gas:
```

>>> Gibbs_formation(-241818, 188.825, [0, 0], [130.571, 205.147], [1, .5])
-228604.141075

```

Calculate the Gibbs free energy of formation for CBrF3 (it is a gas at STP, so its standard-state and ideal-gas state values are the same) at 298.15 K :
```

>>> Gibbs_formation(-648980, 297.713, [0, 0, 0], [5.74, 152.206, 202.789], [1, .5, -
->1.5])
-622649.329975

```

Note in the above calculation that the Bromine's \(S 0\) and \(H f\) are for Br 2 ; and that the value for Bromine as a liquid, which is its standard state, is used.

\section*{chemicals.reaction.entropy_formation( \(H f, G f, T_{-} r e f=298.15\) )}

This function calculates the entropy of formation of a compound, from its constituent elements.
The calculated value will be for a "standard-state" value if \(H f\) and \(G f\) are provided in the standard state; or it will be in an "ideal gas" basis if they are both for an ideal gas. For compounds which are gases at STP, the two values are the same.

\section*{Parameters}

Hf [float] Molar enthalpy of formation of the compound, [ \(\mathrm{J} / \mathrm{mol}\) ]
Gf [float] Molar Gibbs free energy of formation of the compound, [J/mol]
T_ref [float, optional] The standard state temperature, default 298.15 K ; few values are tabulated at other temperatures, [-]

\section*{Returns}

S0 [float] Entropy of formation of the compound, [J/mol/K]

\section*{Examples}

Entropy of formation of methane:
```

>>> entropy_formation(Hf=-74520, Gf=-50490)

```
-80. 59701492537314

Entropy of formation of water in ideal gas state:
```

>>> entropy_formation(Hf=-241818, Gf=-228572)

```
-44.427301693778304
chemicals.reaction.Hf_basis_converter(Hvapm, Hf_liq=None, Hf_gas=None)
This function converts a liquid or gas enthalpy of formation to the other. This is useful, as thermodynamic packages often work with ideal- gas as the reference state and require ideal-gas enthalpies of formation.

\section*{Parameters}

Hvapm [float] Molar enthalpy of vaporization of compound at 298.15 K or (unlikely) the reference temperature, [ \(\mathrm{J} / \mathrm{mol}\) ]

Hf_liq [float, optional] Enthalpy of formation of the compound in its liquid state, [J/mol]
Hf_gas [float, optional] Enthalpy of formation of the compound in its ideal-gas state, [J/mol]

\section*{Returns}

Hf_calc [float, optional] Enthalpy of formation of the compound in the other state to the one provided, [J/mol]

\section*{Examples}

Calculate the ideal-gas enthalpy of formation for water, from its standard- state (liquid) value:
```

>>> Hf_basis_converter(44018, Hf_liq=-285830)
-241812

```

Calculate the standard-state (liquid) enthalpy of formation for water, from its ideal-gas value:
```

>>> Hf_basis_converter(44018, Hf_gas=-241812)
-285830

```

\subsection*{1.23.8 Chemical Reactions}

\section*{chemicals.reaction.balance_stoichiometry (matrix, rounding \(=9\), allow_fractional=False)}

This function balances a chemical reaction.

\section*{Parameters}
matrix [list[list[float]]]
Chemical reaction matrix for further processing; rows contain element counts of each compound, and the columns represent each chemical, [-]

\section*{Returns}
coefficients [list[float]] Balanced coefficients; all numbers are positive, [-]

\section*{Notes}

Balance the reaction \(4 \mathrm{NH} 3+5 \mathrm{O} 2=4 \mathrm{NO}+6 \mathrm{H} 2 \mathrm{O}\), without knowing the coefficients:
```

>> matrix = stoichiometric_matrix([{'N': 1, 'H': 3}, {'0': 2}, {'N': 1, '0': 1}, {
↔'H': 2, '0': 1}], [True, True, False, False])
>>> matrix
[[3, 0, 0, -2], [1, 0, -1, 0], [0, 2, -1, -1]]
>>> balance_stoichiometry(matrix)
[4.0, 5.0, 4.0, 6.0]
>>> balance_stoichiometry(matrix, allow_fractional=True)
[1.0, 1.25, 1.0, 1.5]

```

This algorithm relies on scipy. The behavior of this function for inputs which do not have a unique solution is undefined.
This algorithm may suffer from floating point issues. If you believe there is an error in the result, please report your reaction to the developers.

\section*{References}
[1], [2]
chemicals.reaction.stoichiometric_matrix(atomss, reactants)
This function calculates a stoichiometric matrix of reactants and stoichiometric matrix, as required by a solver to compute the reation coefficients.

\section*{Parameters}
atomss [list[dict[(str, float)]]] A list of dictionaties of (element, element_count) pairs for each chemical, [-]
reactants [list[bool]] List of booleans indicating whether each chemical is a reactant (True) or a product (False), [-]

\section*{Returns}
matrix [list[list[float]]]
Chemical reaction matrix for further processing; rows contain element counts of each compound, and the columns represent each chemical, [-]

\section*{Notes}

The rows of the matrix contain the element counts of each compound, and the columns represent each chemical.

\section*{References}
[1], [2]

\section*{Examples}
```

MgO2 -> Mg + 1/2 O2 (k=1)
>>> stoichiometric_matrix([{'Mg': 1, '0': 1}, {'Mg': 1}, {'0': 2}], [True, False,七
False])
[[1, -1, 0], [1, 0, -2]]

```
\(\mathrm{Cl} 2+\) propylene \(->\) allyl chloride +HCl
>>> stoichiometric_matrix([\{'Cl': 2\}, \{'C': 3, 'H': 6\}, \{'C': 3, 'Cl': 1, 'H': 5\}, \{
\(\hookrightarrow\) 'Cl': 1, 'H': 1\}], [True, True, False, False, False])
\([[0,3,-3,0],[2,0,-1,-1],[0,6,-5,-1]]\)
\(\mathrm{Al}+4 \mathrm{HNO} 3->\mathrm{Al}(\mathrm{NO} 3) 3+\mathrm{NO}+2 \mathrm{H} 2 \mathrm{O}(\mathrm{k}=1)\)
\(\ggg\) stoichiometric_matrix([\{'Al': 1\}, \{'H': 1, 'N': 1, 'O': 3\}, \{'Al': 1, 'N': 3, '0

\([[1,0,-1,0,0],[0,1,0,0,-2],[0,1,-3,-1,0],[0,3,-9,-1,-1]]\)
\(4 \mathrm{Fe}+3 \mathrm{O} 2->2(\mathrm{Fe} 2 \mathrm{O} 3)(\mathrm{k}=2)\)
```

>>> stoichiometric_matrix([{'Fe': 1}, {'0': 2}, {'Fe':2, '0': 3}], [True, True,,
\leftrightarrow F a l s e ] )
[[1, 0, -2], [0, 2, -3]]
4NH3 + 5O2 -> 4NO + 6(H2O) (k=4)
>> stoichiometric_matrix([{'N': 1, 'H': 3}, {'0': 2}, {'N': 1, '0': 1}, {'H': 2, '0
\hookrightarrow': 1}], [True, True, False, False])
[[3, 0, 0, -2], [1, 0, -1, 0], [0, 2, -1, -1]]

```
No unique solution: \(\mathrm{C} 2 \mathrm{H} 5 \mathrm{NO} 2+\mathrm{C} 3 \mathrm{H} 7 \mathrm{NO} 3+2 \mathrm{C} 6 \mathrm{H} 14 \mathrm{~N} 4 \mathrm{O} 2+3 \mathrm{C} 5 \mathrm{H} 9 \mathrm{NO} 2+2 \mathrm{C} 9 \mathrm{H} 11 \mathrm{NO} 2->8 \mathrm{H} 2 \mathrm{O}+\)
C50H73N15O11
```

>>> stoichiometric_matrix([{'C': 2, 'H': 5, 'N': 1, 'O': 2}, {'C': 3, 'H': 7, 'N':ь
\leftrightarrow1, 'O': 3}, {'C': 6, 'H': 14, 'N': 4, 'O': 2}, {'C': 5, 'H': 9, 'N': 1, 'O': 2}, {
\hookrightarrow'C': 9, 'H': 11, 'N': 1, 'O': 2}, {'H': 2, 'O': 1}, {'C': 50, 'H': 73, 'N': 15, '0
\hookrightarrow': 11}], [True, True, True, True, True, False, False])
[[2, 3, 6, 5, 9, 0, -50], [5, 7, 14, 9, 11, -2, -73], [1, 1, 4, 1, 1, 0, -15], [2, ь
\hookrightarrow3, 2, 2, 2, -1, -11]]

```

\subsection*{1.24 Refractive Index (chemicals.refractivity)}

This module contains various refractive index lookup, calculation, and unit conversion routines and dataframes.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Lookup Functions
- Correlations for Specific Substances
- Unit Conversions
- Utility functions
- Pure Component Liquid Fit Correlations

\subsection*{1.24.1 Lookup Functions}
chemicals.refractivity.RI(CASRN, method=None)
This function handles the retrieval of a chemical's refractive index. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Function has data for approximately 4500 chemicals.

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}

RI [float] Refractive Index on the Na D line, [-]
T [float or None] Temperature at which refractive index reading was made; None if not available, [K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined by constants in RI_methods

\section*{Notes}

The available sources are as follows:
- 'CRC', a compillation of Organic RI data in [1].
- 'WIKIDATA', data from the Wikidata project [2]

\section*{References}
[1], [2]

\section*{Examples}
```

>>> RI(CASRN='64-17-5')
(1.3611, 293.15)
>>> RI("60-35-5")
(1.4278, None)
>>> RI('100-41-4', method='WIKIDATA')
(1.495, None)

```
chemicals.refractivity.RI_methods(CASRN)
Return all methods available to obtain the refractive index for the desired chemical.

\section*{Parameters}

\section*{CASRN [str] CASRN, [-]}

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the RI with the given inputs.

\section*{See also:}

RI
chemicals.refractivity.RI_all_methods = ('CRC', 'WIKIDATA')
Tuple of method name keys. See the RI for the actual references

\subsection*{1.24.2 Correlations for Specific Substances}
chemicals.refractivity.RI_IAPWS ( \(T\), rho, wavelength \(=5.893 e-07\) )
Calculates the refractive index of water at a given temperature, density, and wavelength.
\[
\begin{gathered}
n(\rho, T, \lambda)=\left(\frac{2 A+1}{1-A}\right)^{0.5} \\
A(\delta, \theta, \Lambda)=\delta\left(a_{0}+a_{1} \delta+a_{2} \theta+a_{3} \Lambda^{2} \theta+a_{4} \Lambda^{-2} \frac{a_{5}}{\Lambda^{2}-\Lambda_{U V}^{2}}+\frac{a_{6}}{\Lambda^{2}-\Lambda_{I R}^{2}}+a_{7} \delta^{2}\right) \\
\delta=\rho /\left(1000 \mathrm{~kg} / \mathrm{m}^{3}\right) \\
\theta=T / 273.15 \mathrm{~K} \\
\Lambda=\lambda / 0.589 \mu m \\
\Lambda_{I R}=5.432937 \\
\Lambda_{U V}=0.229202
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the water [K]
rho [float] Density of the water \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]\)
wavelength [float] Wavelength of fluid [meters]

\section*{Returns}

RI [float] Refractive index of the water, [-]

\section*{Notes}

This function is valid in the following range: \(261.15 \mathrm{~K}<\mathrm{T}<773.15 \mathrm{~K} 0<\) rho \(<1060 \mathrm{~kg} / \mathrm{m} \wedge 30.2<\) wavelength < 1.1 micrometers

Test values are from IAPWS 2010 book.

\section*{References}
[1]

\section*{Examples}
```

>>> RI_IAPWS(298.15, 997.047435)

```
1.3328581926471605

\subsection*{1.24.3 Unit Conversions}
chemicals.refractivity.brix_to_RI(brix)
Convert a refractive index measurement on the brix scale to a standard refractive index.

\section*{Parameters}
brix [float] Degrees brix to be converted, [ \({ }^{\circ} \mathrm{Bx}\) ]

\section*{Returns}

RI [float] Refractive index, [-]

\section*{Notes}

The scale is officially defined from 0 to 85 ; but the data source contains values up to 95 . Linear extrapolation outside of the bounds is performed; and a table of 96 values are linearly interpolated.
The ICUMSA (International Committee of Uniform Method of Sugar Analysis) published a document setting out the reference values in 1974; but an original data source has not been found and reviewed.

\section*{References}
[1]

\section*{Examples}
>>> brix_to_RI(5.8)
1.341452
>>> brix_to_RI(0.0)
1.33299
>>> brix_to_RI(95.0)
1.532
chemicals.refractivity.RI_to_brix ( \(R I\) )
Convert a standard refractive index measurement to the brix scale.

\section*{Parameters}

RI [float] Refractive index, [-]

\section*{Returns}
brix [float] Degrees brix to be converted, [ \({ }^{\circ} \mathrm{Bx}\) ]

\section*{Notes}

The scale is officially defined from 0 to 85 ; but the data source contains values up to 95 .
Linear extrapolation to values under 0 or above 95 is performed.
The ICUMSA (International Committee of Uniform Method of Sugar Analysis) published a document setting out the reference values in 1974; but an original data source has not been found and reviewed.

\section*{References}
[1]

Examples
```

>>> RI_to_brix(1.341452)
5.8000000000000059
>>> RI_to_brix(1.33299)
0.0
>>> RI_to_brix(1.532)
95.0

```

\subsection*{1.24.4 Utility functions}
chemicals.refractivity.polarizability_from_RI(RI, Vm)
Returns the polarizability of a fluid given its molar volume and refractive index.
\[
\alpha=\left(\frac{3}{4 \pi N_{A}}\right)\left(\frac{n^{2}-1}{n^{2}+2}\right) V_{m}
\]

\section*{Parameters}

RI [float] Refractive Index on Na D line, [-]

Vm [float] Molar volume of fluid, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
alpha [float] Polarizability [m^3]

\section*{Notes}

This Lorentz-Lorentz-expression is most correct when van der Waals interactions dominate. Alternate conversions have been suggested. This is often expressed in units of \(\mathrm{cm}^{\wedge} 3\) or Angstrom^3. To convert to these units, multiply by 1 E 9 or 1 E 30 respectively.

\section*{References}
[1]

\section*{Examples}
>>> polarizability_from_RI(1.3611, 5.8676E-5)
\(5.147658206528923 e-30\)
chemicals.refractivity.molar_refractivity_from_RI (RI, Vm)
Returns the molar refractivity of a fluid given its molar volume and refractive index.
\[
R_{m}=\left(\frac{n^{2}-1}{n^{2}+2}\right) V_{m}
\]

\section*{Parameters}

RI [float] Refractive Index on Na D line, [-]
Vm [float] Molar volume of fluid, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
\(\mathbf{R m}\) [float] Molar refractivity [m^3/mol]

\section*{References}
[1]

\section*{Examples}
>>> molar_refractivity_from_RI(1.3611, 5.8676E-5)
1.2985217089649597e-05
chemicals.refractivity.RI_from_molar_refractivity ( \(\mathrm{Rm}, \mathrm{Vm}\) )
Returns the refractive index of a fluid given its molar volume and molar refractivity.
\[
R I=\sqrt{\frac{-2 R_{m}-V_{m}}{R_{m}-V_{m}}}
\]

\section*{Parameters}
\(\mathbf{R m}\) [float] Molar refractivity [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

Vm [float] Molar volume of fluid, [m^3/mol]

\section*{Returns}

RI [float] Refractive Index on Na D line, [-]

\section*{References}
[1]

\section*{Examples}
>>> RI_from_molar_refractivity(1.2985e-5, 5.8676E-5)
1.3610932757685672

\subsection*{1.24.5 Pure Component Liquid Fit Correlations}
chemicals.refractivity.TDE_RIXExpansion ( \(T, B s, C s\), wavelength \(=5.8926 e-07\) )
Calculates the refractive index of a pure liquid at a given temperature, and wavelength, using the NIST TDE RIXExpansion formula [1].
\[
\begin{gathered}
n(T, \lambda)=\sum_{i=0}^{i} B_{i} t^{i}+\sum_{j} C_{j} w^{j} \\
t=T-298.15 \\
w=W L \times 10^{9}-589.26
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
Bs [list[float]] Polynomial temperature expansion coefficients, in reverse order to the polynomial (as needed for efficient computation with horner's method'), [-]

Cs [list[float]] Polynomial wavelength expansion coefficients, in reverse order to the polynomial (as needed for efficient computation with horner's method'), [-]
wavelength [float] Wavelength of fluid [meters]

\section*{Returns}

RI [float] Refractive index of the pure fluid, [-]

\section*{References}
[1]

\section*{Examples}
>>> TDE_RIXExpansion(330.0, Bs=[-0.000125041, 1.33245], Cs=[1.20771e-7, -3.56795e-5, \(\rightarrow\) O.0], wavelength \(=589.26 \mathrm{e}-9 * .7\) )
1.33854894426073

\subsection*{1.25 Health, Safety, and Flammability Properties (chemicals.safety)}

This module contains functions for lookup the following properties for a chemical:
- Short-term Exposure Limit (STEL)
- Time-Weighted Average Exposure Limit (TWA)
- Celing limit for working exposure
- Whether a chemicals is absorbed thorough human skin
- Whether a chemical is a carcinogen, suspected of being a carcinogen, or has been identified as unlikely to be a carcinogen
- Flash point
- Auto ignition point
- Lower flammability limit
- Upper flammability limit

In addition, several estimation methods for chemicals without flammability limits are provided and for calculating the flammability limits of mixtures.
This module also contains several utility functions.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Short-term Exposure Limit
- Time-Weighted Average Exposure Limit
- Ceiling Limit
- Skin Absorbance
- Carcinogenicity
- Flash Point
- Autoignition Point
- Lower Flammability Limit
- Upper Flammability Limit
- Mixture Flammability Limit
- Utility Methods

\subsection*{1.25.1 Short-term Exposure Limit}
chemicals.safety.STEL (CASRN, method=None)
This function handles the retrieval of Short-term Exposure Limit (STEL) on worker exposure to dangerous chemicals.

\section*{Parameters}

CASRN [str] CASRN, [-]
method [str] Name of method to use, [-]

\section*{Returns}

STEL [float] Short-term Exposure Limit, [ppm or mg/m^3]
units [str] One of ppm or \(\mathrm{mg} / \mathrm{m}^{\wedge} 3,[-]\)

\section*{Notes}

The ppm value is preferentially returned if both are available. While they can be converted in specific cases, it is better to work with the specified units of the original source.

\section*{Examples}
```

>>> STEL('67-64-1')

```
(750.0, 'ppm')
>>> STEL('7664-38-2')
(Q.7489774978301237, 'ppm')
>>> STEL('55720-99-5')
(2.0, 'mg/m^3')
chemicals.safety.STEL_methods (CASRN)
Return all methods available to obtain STEL for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain STEL with the given inputs.
See also:

STEL
chemicals.safety.STEL_all_methods = ('Ontario Limits',)
Tuple of method name keys. See the STEL for the actual references

\subsection*{1.25.2 Time-Weighted Average Exposure Limit}
chemicals.safety.TWA(CASRN, method=None)
Return the Time-Weighted Average exposure limits (TWA) for the desired chemical if it is available.

\section*{Parameters}

CASRN [str] CASRN, [-]
method [str] Name of method to use, [-]

\section*{Returns}

TWA [float] Time-Weighted Average exposure, \([\mathrm{ppm}\) or \(\mathrm{mg} / \mathrm{m} \wedge 3\) ]
units [str] One of ppm or \(\mathrm{mg} / \mathrm{m}^{\wedge} 3,[-]\)

\section*{Notes}

The ppm value is preferentially returned if both are available. While they can be converted in specific cases, it is better to work with the specified units of the original source.

\section*{Examples}
>>> TWA ('98-00-0')
(10.0, 'ppm')
>> TWA ('1303-00-0')
(5.0742430905659505e-05, 'ppm')

\section*{chemicals.safety.TWA_methods(CASRN)}

Return all methods available to obtain the Time-Weighted Average exposure limits (TWA) for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain TWA with the given inputs.

\section*{See also:}

TWA

\section*{Examples}
>>> TWA_methods('71-43-2')
['Ontario Limits']
chemicals.safety.TWA_all_methods = ('Ontario Limits',)
Tuple of method name keys. See the TWA for the actual references

\subsection*{1.25.3 Ceiling Limit}

\section*{chemicals.safety.Ceiling(CASRN, method=None)}

This function handles the retrieval of ceiling limits on worker exposure to dangerous chemicals. Ceiling limits are not to be exceeded at any time.

\section*{Parameters}

CASRN [str] CASRN, [-]
method [str] Name of method to use, [-]

\section*{Returns}

Ceiling [float] Ceiling Limit, [ppm or \(\mathrm{mg} / \mathrm{m}^{\wedge} 3\) ]
units [str] One of ppm or \(\mathrm{mg} / \mathrm{m}^{\wedge} 3,[-]\)

\section*{Examples}
>>> Ceiling('75-07-0')
(25.0, 'ppm')
>>> Ceiling('1395-21-7')
(6e-05, 'mg/m^3')
chemicals.safety. Ceiling_methods (CASRN)
Return all methods available to obtain Ceiling limits for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain Ceiling limits with the given inputs.

\section*{See also:}

Ceiling
```

chemicals.safety.Ceiling_all_methods = ('Ontario Limits',)

```

Tuple of method name keys. See the Ceiling for the actual references

\subsection*{1.25.4 Skin Absorbance}
chemicals.safety.Skin(CASRN, method=None)
This function handles the retrieval of whether or not a chemical can be absorbed through the skin, relevant to chemical safety calculations.

\section*{Parameters}

CASRN [str] CASRN, [-]
method [str] Name of method to use, [-]

\section*{Returns}
skin [bool] Whether or not the substance is absorbed through human skin, [-]

\section*{Examples}
>>> Skin('108-94-1')
True
>>> Skin('1395-21-7')
False
chemicals.safety.Skin_methods(CASRN)
Return all methods available to obtain whether or not a chemical can be absorbed through the skin.

\section*{Parameters}

\section*{CASRN [str] CASRN, [-]}

\section*{Returns}
methods [list[str]] Methods which can be used to obtain whether or not a chemical can be absorbed through the skin.

\section*{See also:}

Skin
chemicals.safety.Skin_all_methods = ('Ontario Limits',)
Tuple of method name keys. See the Skin for the actual references

\subsection*{1.25.5 Carcinogenicity}
chemicals.safety.Carcinogen (CASRN, method=None)
Looks up if a chemical is listed as a carcinogen or not according to either a specifc method or with all methods. Returns either the status as a string for a specified method, or the status of the chemical in all available data sources, in the format \(\{\) source: status \(\}\).

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}
status [str or dict] Carcinogen status information [-].

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, Carcinogen_all_methods.

\section*{Notes}

\section*{Supported methods are:}
- IARC: International Agency for Research on Cancer, [1]. As extracted with a last update of February 22, 2016. Has listing information of 863 chemicals with CAS numbers. Chemicals without CAS numbers not included here. If two listings for the same CAS were available, the harshest rating was used. If two listings were available published at different times, the latest value was used. All else equal, the most pessimistic value was used.
- NTP: National Toxicology Program, [2]. Has data on 228 chemicals.

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Carcinogen('61-82-5')
{'International Agency for Research on Cancer': 'Not classifiable as to its_
carcinogenicity to humans (3)', 'National Toxicology Program 13th Report on}
\rightarrow Carcinogens': 'Reasonably Anticipated'\}

```
chemicals.safety.Carcinogen_methods (CASRN)
Return all methods available to obtain Carcinogen listings for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain Carcinogen listings with the given inputs.

See also:
Carcinogen
```

chemicals.safety.Carcinogen_all_methods = ('International Agency for Research on Cancer',

```
'National Toxicology Program 13th Report on Carcinogens')

Tuple of method name keys. See the Carcinogen for the actual references

\subsection*{1.25.6 Flash Point}

\section*{chemicals.safety.T_flash(CASRN, method=None)}

This function handles the retrieval or calculation of a chemical's flash point. Lookup is based on CASRNs. No predictive methods are currently implemented. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

T_flash [float] Flash point of the chemical, [K]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, T_flash_all_methods,

See also:

T_flash_methods

\section*{Notes}

Preferred source is 'IEC 60079-20-1 (2010)' [1], with the secondary source 'NFPA 497 (2008)' [2] having very similar data. A third source 'Serat DIPPR (2017)' [3] provides third hand experimental but evaluated data from the DIPPR database, version unspecified, for 870 compounds.

The predicted values from the DIPPR databank are also available in the supporting material in [3], but are not included.

\section*{References}
[1], [2], [3], [4]

\section*{Examples}
```

>>> T_flash(CASRN='64-17-5')
285.15
>>> T_flash('111-69-3', method='WIKIDATA')
365.92778

```
chemicals.safety.T_flash_methods(CASRN)
Return all methods available to obtain \(\mathrm{T}_{-}\)flash for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain T_flash with the given inputs.
See also:
T_flash
chemicals.safety.T_flash_all_methods = ('IEC 60079-20-1 (2010)', 'NFPA 497 (2008)', 'Serat DIPPR (2017)', 'WIKIDATA')

Tuple of method name keys. See the \(T_{-} f l a s h\) for the actual references

\subsection*{1.25.7 Autoignition Point}

\section*{chemicals.safety.T_autoignition(CASRN, method=None)}

This function handles the retrieval or calculation of a chemical's autoifnition temperature. Lookup is based on CASRNs. No predictive methods are currently implemented. Will automatically select a data source to use if no Method is provided; returns None if the data is not available.

\section*{Parameters}

CASRN [str] CASRN [-]

\section*{Returns}

Tautoignition [float] Autoignition point of the chemical, [K].

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, T_autoignition_all_methods.
See also:
T_autoignition_methods

\section*{Notes}

Preferred source is 'IEC 60079-20-1 (2010)' [1], with the secondary source 'NFPA 497 (2008)' [2] having very similar data.

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> T_autoignition(CASRN='71-43-2')
771.15
>>> T_autoignition('111-69-3', method='WIKIDATA')
823.15

```
chemicals.safety.T_autoignition_methods(CASRN)
Return all methods available to obtain T_autoignition for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain T_autoignition with the given inputs.
See also:
T_autoignition
```

chemicals.safety.T_autoignition_all_methods = ('IEC 60079-20-1 (2010)', 'NFPA 497

```
(2008)', 'WIKIDATA')

Tuple of method name keys. See the T_autoignition for the actual references

\subsection*{1.25.8 Lower Flammability Limit}
chemicals.safety.LFL \(\left(H c=\right.\) None, atoms \(=\) None, \(C A S R N={ }^{\prime \prime}\), method \(=\) None \()\)
This function handles the retrieval or calculation of a chemical's Lower Flammability Limit. Lookup is based on CASRNs. Will automatically select a data source to use if no Method is provided; returns None if the data is not available.

\section*{Parameters}

He [float, optional] Heat of combustion of gas [J/mol].
atoms [dict, optional] Dictionary of atoms and atom counts.
CASRN [str, optional] CASRN, [-]

\section*{Returns}

LFL [float] Lower flammability limit of the gas in an atmosphere at STP, [mole fraction].

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, LFL_all_methods.

\section*{Notes}

Preferred source is 'IEC 60079-20-1 (2010)' [1], with the secondary source 'NFPA 497 (2008)' [2] having very similar data. If the heat of combustion is provided, the estimation method Suzuki_LFL can be used. If the atoms of the molecule are available, the method Crowl_Louvar_LFL can be used.

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> LFL(CASRN='71-43-2')
0.012
>> LFL(Hc=-890590.0, atoms={'C': 1, 'H': 4}, CASRN='74-82-8')
0.044
>>> LFL(CASRN='111-69-3', method='WIKIDATA')
0.017

```
chemicals.safety.LFL_methods(Hc=None, atoms=None, \(C A S R N=\) ")
Return all methods available to obtain LFL for the desired chemical.

\section*{Parameters}

Hc [float, optional] Heat of combustion of gas [J/mol].
atoms [dict, optional] Dictionary of atoms and atom counts.
CASRN [str, optional] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain LFL with the given inputs.

\section*{See also:}

LFL

\section*{Examples}

Methane
```

>>> LFL_methods(Hc=-890590.0, atoms={'C': 1, 'H': 4}, CASRN='74-82-8')
['IEC 60079-20-1 (2010)', 'NFPA 497 (2008)', 'Suzuki (1994)', 'Crowl and Louvar_
->(2001)']

```
chemicals.safety.LFL_all_methods = ('IEC 60079-20-1 (2010)', 'NFPA 497 (2008)', 'WIKIDATA', 'Suzuki (1994)', 'Crowl and Louvar (2001)')

Tuple of method name keys. See the LFL for the actual references
chemicals.safety.Suzuki_LFL ( \(H c\) )
Calculates lower flammability limit, using the Suzuki [1] correlation. Uses heat of combustion only.
The lower flammability limit of a gas is air is:
\[
\begin{gathered}
\mathrm{LFL}=\frac{-3.42}{\Delta H_{c}^{\circ}}+0.569 \\
\Delta H_{c}^{\circ}+0.0538 \Delta H_{c}^{\circ 2}+1.80
\end{gathered}
\]

\section*{Parameters}

Hc [float] Heat of combustion of gas [J/mol]

\section*{Returns}

LFL [float] Lower flammability limit, mole fraction [-]

\section*{Notes}

Fit performed with 112 compounds, \(\mathrm{r}^{\wedge} 2\) was 0.977 . LFL in percent volume in air. Hc is at standard conditions, in \(\mathrm{MJ} / \mathrm{mol} .11\) compounds left out as they were outliers. Equation does not apply for molecules with halogen atoms, only hydrocarbons with oxygen or nitrogen or sulfur. No sample calculation provided with the article. However, the equation is straightforward. Limits of equations's validity are -6135596 J where it predicts a LFL of 0 , and -48322129 J where it predicts a LFL of 1 .

\section*{References}

\section*{[1]}

\section*{Examples}

Pentane, 1.5 \% LFL in literature
```

>>> Suzuki_LFL(-3536600)
0.014276107095811815

```

\section*{chemicals.safety. Crowl_Louvar_LFL(atoms)}

Calculates lower flammability limit, using the Crowl-Louvar [1] correlation. Uses molecular formula only. The lower flammability limit of a gas is air is:
\[
\begin{aligned}
& C_{m} H_{x} O_{y}+z O_{2} \rightarrow m \mathrm{CO}_{2}+\frac{x}{2} \mathrm{H}_{2} \mathrm{O} \\
& \mathrm{LFL}=\frac{0.55}{4.76 m+1.19 x-2.38 y+1}
\end{aligned}
\]

\section*{Parameters}
atoms [dict] Dictionary of atoms and atom counts

\section*{Returns}

LFL [float] Lower flammability limit, mole fraction

\section*{Notes}

Coefficient of 0.55 taken from [2]

\section*{References}
[1], [2]

\section*{Examples}

Hexane, example from [1], lit. \(1.2 \%\)
```

>>> Crowl_Louvar_LFL({'H': 14, 'C': 6})
0.011899610558199915

```
chemicals.safety.LFL_ISO_10156_2017 (zs, LFLs, CASs)
Calculate the lower flammability limit of a mixture of combustible gases and inert gases according to ISO 10156 (2017) [1].
\[
\begin{gathered}
\mathrm{LFL}=\frac{1}{\sum_{i=1}^{n_{\text {combustible }}} \frac{A_{i}}{\mathrm{LFL}_{i}^{\prime}}} \\
\mathrm{LFL}_{i}^{\prime}=\frac{1-\mathrm{LFL}_{m}^{\prime}-(1-K) \frac{\sum_{j}^{n_{\text {inert }}} B_{j}}{\sum_{j}^{n_{\text {combustible }}} A_{j}} \mathrm{LFL}_{m}^{\prime}}{100-\mathrm{LFL}_{m}^{\prime}} \mathrm{LFL}_{i} \\
K=\sum_{i}^{n_{\text {inert }}} z_{i} K_{k}
\end{gathered}
\]

The \(B\) sum is the total mole fraction of all inert gas compounds; and the \(A\) sum is the total mole fraction of all combustible compounds. \(K_{k}\) are the looked up inert gas coefficients. \(\mathrm{LFL}_{m}^{\prime}\) is calculated as the Le Chatelier's lower flammability limit if there were no inert gases in the mixture.

\section*{Parameters}
zs [list[float]] Mole fractions of all components in a gas including inerts, [-]
LFLs [list[float]] Lower or upper flammability limits for each flammable component in a gas, [-]
CASs [list[str]] CAS numbers of each compound; required to look up inert gas factors, [-]

\section*{Returns}

LFL [float] Lower or flammability limit of a gas mixture, [-]

\section*{Notes}

Inert gas parameters are available for \(\mathrm{O} 2, \mathrm{~N} 2, \mathrm{CO} 2, \mathrm{He}, \mathrm{Ar}, \mathrm{Ne}, \mathrm{Kr}, \mathrm{Xe}, \mathrm{SO} 2, \mathrm{SF} 6, \mathrm{CF} 4, \mathrm{C} 3 F 8\), and C2HF5.

\section*{References}
[1]

\section*{Examples}

All the sample problems from [1] have been implemented as tests.
```

>>> zs = [.15, .15, .3, .35+.05*.79, .05*.21]
>>> LFLs = [.04, .044, None, None, None]
>>> CASs = ['1333-74-0', '74-82-8', '124-38-9', '7727-37-9', '7782-44-7']
>>> LFL_ISO_10156_2017(zs, LFLs, CASs)
0.1427372274

```

\subsection*{1.25.9 Upper Flammability Limit}
chemicals.safety.UFL ( \(H c=\) None, atoms=None, CASRN=", method=None)
This function handles the retrieval or calculation of a chemical's Upper Flammability Limit. Lookup is based on CASRNs. Two predictive methods are currently implemented. Will automatically select a data source to use if no Method is provided; returns None if the data is not available.

\section*{Parameters}

He [float, optional] Heat of combustion of gas [J/mol]
atoms [dict, optional] Dictionary of atoms and atom counts
CASRN [str, optional] CASRN [-]

\section*{Returns}

UFL [float] Upper flammability limit of the gas in an atmosphere at STP, [mole fraction]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, UFL_all_methods.

\section*{Notes}

Preferred source is 'IEC 60079-20-1 (2010)' [1], with the secondary source 'NFPA 497 (2008)' [2] having very similar data. If the heat of combustion is provided, the estimation method Suzuki_UFL can be used. If the atoms of the molecule are available, the method Crowl_Louvar_UFL can be used.

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> UFL(CASRN='71-43-2')
0.086

```

Methane
```

>> UFL(Hc=-890590.0, atoms={'C': 1, 'H': 4}, CASRN='74-82-8')
0.17
>>> UFL(CASRN='111-69-3', method='WIKIDATA')
0.05

```
chemicals.safety.UFL_methods ( \(H c=\) None, atoms=None, CASRN=")
Return all methods available to obtain UFL for the desired chemical.

\section*{Parameters}

Hc [float, optional] Heat of combustion of gas [J/mol].
atoms [dict, optional] Dictionary of atoms and atom counts.
CASRN [str, optional] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain UFL with the given inputs.
See also:
UFL

\section*{Examples}

Methane
```

>>> UFL_methods(Hc=-890590.0, atoms={'C': 1, 'H': 4}, CASRN='74-82-8')
['IEC 60079-20-1 (2010)', 'NFPA 497 (2008)', 'Suzuki (1994)', 'Crowl and Louvar_
->(2001)']

```
chemicals.safety.UFL_all_methods = ('IEC 60079-20-1 (2010)', 'NFPA 497 (2008)',
'WIKIDATA', 'Suzuki (1994)', 'Crowl and Louvar (2001)')

Tuple of method name keys. See the UFL for the actual references
chemicals.safety. Suzuki_UFL ( \(H c\) )
Calculates upper flammability limit, using the Suzuki [1] correlation. Uses heat of combustion only. The upper flammability limit of a gas is air is:
\[
\mathrm{UFL}=6.3 \Delta H_{c}^{\circ}+0.567 \Delta H_{c}^{\circ 2}+23.5
\]

\section*{Parameters}

Hc [float] Heat of combustion of gas [ \(\mathrm{J} / \mathrm{mol}\) ]

\section*{Returns}

UFL [float] Upper flammability limit, mole fraction

\section*{Notes}

UFL in percent volume in air according to original equation. Hc is at standard conditions in the equation, in units of MJ/mol. AAPD \(=1.2 \%\) for 95 compounds used in fit. Somewhat better results than the High and Danner method. \(4.9 \%<\mathrm{UFL}<23.0 \%-890.3 \mathrm{~kJ} / \mathrm{mol}<\mathrm{dHc}<-6380 \mathrm{~kJ} / \mathrm{mol} \mathrm{r}^{\wedge} 2=0.989\) Sample calculations provided for all chemicals, both this method and High and Danner. Examples are from the article. Predicts a UFL of 1 at 7320190 J and a UFL of 0 at -5554160 J .

\section*{References}

\section*{[1]}

\section*{Examples}

Pentane, literature 7.8\% UFL
>>> Suzuki_UFL(-3536600)
0.0831119493052

\section*{chemicals.safety.Crowl_Louvar_UFL(atoms)}

Calculates upper flammability limit, using the Crowl-Louvar [1] correlation. Uses molecular formula only. The upper flammability limit of a gas is air is:
\[
\begin{aligned}
& \mathrm{C}_{m} \mathrm{H}_{x} \mathrm{O}_{y}+z \mathrm{O}_{2} \rightarrow m \mathrm{CO}_{2}+\frac{x}{2} \mathrm{H}_{2} \mathrm{O} \\
& \mathrm{UFL}=\frac{3.5}{4.76 m+1.19 x-2.38 y+1}
\end{aligned}
\]

\section*{Parameters}
atoms [dict] Dictionary of atoms and atom counts

\section*{Returns}

UFL [float] Upper flammability limit, mole fraction

\section*{Notes}

Coefficient of 3.5 taken from [2]

\section*{References}
[1], [2]

\section*{Examples}

Hexane, example from [1], lit. 7.5 \%
```

>>> Crowl_Louvar_UFL({'H': 14, 'C': 6})

```
0.07572479446127219

\subsection*{1.25.10 Mixture Flammability Limit}
chemicals.safety.fire_mixing ( \(y s, F L s\) )
Le Chatelier's mixing rule for lower and upper flammability limits of mixtures of gases.

\section*{Parameters}
ys [list[float]] Normalized mole fractions of all flammable components in a gas, [-]
FLs [list[float]] Lower or upper flammability limits for each flammable component in a gas, [-]

\section*{Returns}

FL [float] Lower or upper flammability limit of a gas, [-]

\section*{Notes}

This equation has a higher accuracy for lower flammability limits than upper flammability limits. Some sources recommend not using it for upper flammability limits.

\section*{References}
[1]

\section*{Examples}

Sample problems from [1] for the lower and upper flammability limit.
>>> fire_mixing(ys=normalize([0.0024, 0.0061, 0.0015]), FLs=[.012, .053, .031]) 0.02751172136637642
>>> fire_mixing(ys=normalize([0.0024, 0.0061, 0.0015]), FLs=[.075, .15, .32]) Q. 12927551844869378

\subsection*{1.25.11 Utility Methods}
chemicals.safety.ppmv_to_mgm3(ppmv, \(M W, T=298.15, P=101325.0\) )
Converts a concentration in ppmv to units of \(\mathrm{mg} / \mathrm{m}^{\wedge} 3\). Used in industrial toxicology.
\[
\frac{m g}{m^{3}}=\frac{p p m v \cdot P}{R T} \cdot \frac{M W}{1000}
\]

\section*{Parameters}
ppmv [float] Concentration of a component in a gas mixure [parts per million, volumetric]

MW [float] Molecular weight of the trace gas [ \(\mathrm{g} / \mathrm{mol}\) ]
\(\mathbf{T}\) [float, optional] Temperature of the gas at which the ppmv is reported, [K]
\(\mathbf{P}\) [float, optional] Pressure of the gas at which the ppmv is reported, [Pa]

\section*{Returns}
\(\mathbf{m g m} 3\) [float] Concentration of a substance in an ideal gas mixture \(\left[\mathrm{mg} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Notes}

The term \(\mathrm{P} /(\mathrm{RT}) / 1000\) converts to 0.040874 at STP. Its inverse is reported as 24.45 in [1].

\section*{References}

\section*{[1]}

\section*{Examples}
```

>>> ppmv_to_mgm3(1.0, 40.0)

```
1.6349617809430446
chemicals.safety.mgm3_to_ppmv( \(m g m 3, M W, T=298.15, P=101325.0\) )
Converts a concentration in \(\mathrm{mg} / \mathrm{m}^{\wedge} 3\) to units of ppmv. Used in industrial toxicology.
\[
p p m v=\frac{1000 R T}{M W \cdot P} \cdot \frac{m g}{m^{3}}
\]

\section*{Parameters}
mgm3 [float] Concentration of a substance in an ideal gas mixture [ \(\mathrm{mg} / \mathrm{m}^{\wedge} 3\) ]
MW [float] Molecular weight of the trace gas [g/mol]
T [float, optional] Temperature of the gas at which the ppmv is reported, [K]
\(\mathbf{P}\) [float, optional] Pressure of the gas at which the ppmv is reported, [Pa]

\section*{Returns}
ppmv [float] Concentration of a component in a gas mixure [parts per million, volumetric]

\section*{Notes}

The term \(\mathrm{P} /(\mathrm{RT}) / 1000\) converts to 0.040874 at STP . Its inverse is reported as 24.45 in [1].

\section*{References}
[1]

\section*{Examples}
>>> mgm3_to_ppmv(1.635, 40.0)
1.0000233761164334
chemicals.safety.NFPA_30_classification(T_flash, \(T b=\) None, Psat_100F=None)
Classify a chemical's flammability/combustibility according to the NFPA 30 standard Flammable and Combustible Liquids Code.

Class IA: Flash Point \(<73^{\circ} \mathrm{F}\); Boiling Point \(<100^{\circ} \mathrm{F}\) Class IB: Flash Point \(<73^{\circ} \mathrm{F} ; 100^{\circ} \mathrm{F}<=\) Boiling Point Class IC: \(73^{\circ} \mathrm{F}<=\) Flash Point \(<100^{\circ} \mathrm{F}\) Class II: \(100^{\circ} \mathrm{F}<=\) Flash Point \(<140^{\circ} \mathrm{F}\) Class IIIA: \(140^{\circ} \mathrm{F}<=\) Flash Point \(<\) \(200^{\circ} \mathrm{F}\) Class IIIB: \(200^{\circ} \mathrm{F}<=\) Flash Point

Class I liquids are designated as flammable; class II and II liquids are designated as combustible.

\section*{Parameters}

T_flash [float] Flash point (closed-cup method, adjusted for sea level), [K]
Tb [float, optional] Normal boiling point (needed to classify IA and IB liquids), [K]
Psat_100F [float, optional] Vapor pressure at \(100^{\circ} \mathrm{F}\) (needed to classify IA and IB liquids), [K]

\section*{Returns}
classification [str] One of 'IA', 'IB', 'IC', 'II', 'IIIA', 'IIIB', [-]

\section*{Notes}

Only one of \(T b\) or Psat_100F is needed.
Class 'IA' also includes unstable liquids.

\section*{References}
[1]

\section*{Examples}

Ethylene oxide
```

>>> NFPA_30_classification(253.15, 283.55)
'IA'

```

Butyl alcohol
```

>>> NFPA_30_classification(308.15)
'IC'

```

\subsection*{1.26 Solubility (chemicals.solubility)}

This module contains various solubility calculation routines and a Henry's law coefficient converter.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Henry's Law
- Utility functions

\subsection*{1.26.1 Henry's Law}
chemicals.solubility.Henry_pressure ( \(T, A, B=0.0, C=0.0, D=0.0, E=0.0, F=0.0\) )
Calculates Henry's law constant as a function of temperature according to the SI units of Pa and using a common temperature dependence as used in many process simulation applications.

Only the \(A\) parameter is required - which has no temperature dependence when used by itself. As the model is exponential, a sufficiently high temperature may cause an OverflowError. A negative temperature (or just low, if fit poorly) may cause a math domain error.
\[
H_{12}=\exp \left(A_{12}+\frac{B_{12}}{T}+C_{12} \ln (T)+D_{12} T+\frac{E_{12}}{T^{2}}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature, [K]
A-F [float] Parameter for the equation; chemical and property specific [-]

\section*{Returns}

H12 [float] Henry's constant [Pa]

\section*{Notes}

Add 11.51292 to the \(A\) constant if it is said to provide units of bar, so that it provides units of \(P a\) instead.
The \(F\) parameter is not often included in models. It is rare to fit all parameters.

\section*{References}
[1]

\section*{Examples}

Random test example.
```

>>> Henry_pressure(300.0, A=15.0, B=300.0, C=.04, D=1e-3, E=1e2, F=1e-5)
37105004.47898146

```
chemicals.solubility.Henry_pressure_mixture(Hs, weights=None, zs=None)
Mixing rule for Henry's law components. Applies a logarithmic average to all solvent components and mole fractions. Optionally, weight factors can be provided instead of using mole fractions - only specify one of them.

A common weight factor is using volume fractions of powers of them, or using critical volumes.

\section*{Parameters}

Hs [list[float or None]] Henry's law constant between each gas and the solvent (None for other solvents of gases without parameters available), [Pa]
weights [list[float], optional] Weight factors, [-]
zs [list[float]] Mole fractions of all species in phase, [-]

\section*{Returns}

H [value] Henry's law constant for the gas in the liquid phase, [-]

\section*{Notes}

The default weight factor formulation is from [1].

\section*{References}
[1]

\section*{Examples}
>>> Henry_pressure_mixture([1072330.36341, 744479.751106, None], zs=[.48, .48, .04]) 893492.1611602883
chemicals.solubility.Henry_converter (val, old_scale, new_scale, rhom=None, \(M W=\) None) Converts Henry's law constant for a gas with respect to a solvent from one scale to another.
There are many scales, but it is recommemed to operate in the scale of \(S I\) - which returns a value with units \(P a\), and directly gets used in place of vapor pressure inside a flash calculation. This removes the complexity of Henry's law, avoiding possible simplication in favor of use with other thermodynamic models.

Only some scales require the molecular weight and the molar density of the solvent. Values for water, the most common solute, are \(55344.59 \mathrm{~mol} / \mathrm{m}^{\wedge} 3\) at STP and \(18.01528 \mathrm{~g} / \mathrm{mol}\).

\section*{Parameters}
val [float] Henry's law constant, various units
old_scale [str] String representing the scale that val is in originally.
new_scale [str] String representing the scale that val should be converted to.

\section*{Returns}
result [float] Input val converted from old_scale to new_scale, various units

\section*{Notes}

The valid scales for this function are any of the following:
('Hcp', 'mol/(m^3*Pa)', 'M/atm', ‘Hcc', 'mol/(kg*Pa)', 'Hbp', 'mol/(kg*atm)', 'Hxp', '1/atm', 'alpha', 'bunsen coefficient', 'KHpx', 'atm', 'm^3*Pa/mol', 'KHpc', 'm^3*atm/mol', 'KHcc', 'SI')

\section*{References}
[1]

\section*{Examples}
```

>>> Henry_converter(1.2e-5, old_scale='Hcp', new_scale='SI', rhom=55344.59,
... MW=18.01528)
4612049166.666666

```
>>> Henry_converter(Q.0297475, old_scale='Hcc', new_scale='KHcc',
... rhom=55344.59, MW=18.01528)
33.61627027481301
chemicals.solubility.Henry_constants(lnHenry_matrix, zs, henry_components, skip_zero=True, Hs=None)
Calculate the Henry's law constants for a list of components, only some of which are henry's law following components (solutes) and the rest that are solvents. The empirical mixing rule from [1] is used as follows:
\[
H_{i}=\exp \left(\frac{\sum_{\mathrm{j}=\text { solvent }} z_{j} \ln H_{i, j}}{\sum_{\mathrm{j}=\text { solvent }} z_{j}}\right)
\]

\section*{Parameters}

InHenry_matrix [list[list[float]]] Henry's law constants between every species; 0.0 for nonapplicable solvents, \([\log (\mathrm{Pa})]\)
zs [list[float]] Mole fractions of all species in phase; this can be mass or volume fractions as well, [-]
henry_components [list[bool]] Whether or not each component is a henry's law solvent or not, [-]
skip_zero [bool] If true, if parameters are missing from a solvent-solute pair, that pair will not be counted as part of the solvent fraction. If false, the calculation proceeds and the solubility is underestimated. Missing parameters are assumed from the value of lnHenry_matrix being \(0,[-]\)
Hs [list[float], optional] Henry's law constants for each component; 0 for non-henry components (input array), [Pa]

\section*{Returns}

Hs [list[float]] Henry's law constants for each component; 0 for non-henry components, [Pa]

\section*{References}
[1]

\section*{Examples}

Oxygen and methane in water:
```

>>> lnHenry_matrix = [[0.0, 0.0, 0.0], [22.13581843104147, 0.0, 0.0], [22.
\rightarrow 2 3 9 0 3 8 4 5 9 4 7 5 7 3 3 , ~ 0 . 0 , ~ 0 . 0 ] ] ~
>>> Henry_constants(lnHenry_matrix, [0.8, 0.15, 0.05], [False, True, True], True)
[0.0, 4106424071.093, 4552937470.331]

```
chemicals.solubility.dHenry_constants_dT(lnHenry_matrix, dlnHenry_matrix_dT, zs, henry_components, skip_zero=True, \(d H_{-} d T s=\) None)
Calculate the first temperature derivative of Henry's law constants for a list of components, only some of which are henry's law following components (solutes) and the rest that are solvents. The empirical mixing rule from [1] is used as follows:

\section*{Parameters}

InHenry_matrix [list[list[float]]] Henry's law constants between every species; 0.0 for nonapplicable solvents, \([\log (\mathrm{Pa})]\)
dlnHenry_matrix_dT [list[list[float]]] First temperature derivative of Henry's law constants between every species; 0.0 for non-applicable solvents, \([\log (\mathrm{Pa}) / \mathrm{K}]\)
zs [list[float]] Mole fractions of all species in phase; this can be mass or volume fractions as well, [-]
henry_components [list[bool]] Whether or not each component is a henry's law solvent or not, [-]
skip_zero [bool] If true, if parameters are missing from a solvent-solute pair, that pair will not be counted as part of the solvent fraction. If false, the calculation proceeds and the solubility is underestimated. Missing parameters are assumed from the value of lnHenry_matrix being 0, [-]
dH_dTs [list[float], optional] First temperature derivative of Henry's law constants for each component; 0 for non-henry components (input array), \([\mathrm{Pa} / \mathrm{K}]\)

\section*{Returns}
dH_dTs [list[float]] First temperature derivative of Henry's law constants for each component; 0 for non-henry components, \([\mathrm{Pa} / \mathrm{K}]\)

\section*{References}
[1]

\section*{Examples}

Oxygen and methane in water:
```

>>> lnHenry_matrix = [[0.0, 0.0, 0.0], [22.13581843104147, 0.0, 0.0], [22.
->239038459475733, 0.0, 0.0]]
>>> dlnHenry_matrix_dT = [[0.0, 0.0, 0.0], [0.017113988888888904, 0.0, 0.0], [0.
->015461911111111101, 0.0, 0.0]]
>>> dHenry_constants_dT(lnHenry_matrix, dlnHenry_matrix_dT, [0.8, 0.15, 0.05],七
[False, True, True], True)
[0.0, 70277295.92576516, 70397114.46071726]

```
chemicals.solubility.d2Henry_constants_dT2 (lnHenry_matrix, dlnHenry_matrix_dT, \(d 2 \ln H e n r y \_m a t r i x \_d T 2, z s\), henry_components, skip_zero=True, \(d 2 H_{-} d T 2 s=\) None)
Calculate the second temperature derivative of Henry's law constants for a list of components, only some of which are henry's law following components (solutes) and the rest that are solvents. The empirical mixing rule from [1] is used as follows:

\section*{Parameters}

InHenry_matrix [list[list[float]]] Henry's law constants between every species; 0.0 for nonapplicable solvents, \([\log (\mathrm{Pa})]\)
dInHenry_matrix_dT [list[list[float]]] First temperature derivative of Henry's law constants between every species; 0.0 for non-applicable solvents, \([\log (\mathrm{Pa}) / \mathrm{K}]\)
d2InHenry_matrix_dT2 [list[list[float]]] Second temperature derivative of Henry's law constants between every species; 0.0 for non-applicable solvents, \(\left[\log (\mathrm{Pa}) / \mathrm{K}^{\wedge} 2\right]\)
zs [list[float]] Mole fractions of all species in phase; this can be mass or volume fractions as well, [-]
henry_components [list[bool]] Whether or not each component is a henry's law solvent or not, [-]
skip_zero [bool] If true, if parameters are missing from a solvent-solute pair, that pair will not be counted as part of the solvent fraction. If false, the calculation proceeds and the solubility is underestimated. Missing parameters are assumed from the value of lnHenry_matrix being \(0,[-]\)
d2H_dT2s [list[float], optional] Second temperature derivative of Henry's law constants for each component; 0 for non-henry components (input array), \(\left[\mathrm{Pa} / \mathrm{K}^{\wedge} 2\right]\)

\section*{Returns}
d2H_dT2s [list[float]] Second temperature derivative of Henry's law constants for each component; 0 for non-henry components, \(\left[\mathrm{Pa} / \mathrm{K}^{\wedge} 2\right]\)

\section*{References}
[1]

\section*{Examples}

Oxygen and methane in water:
```

>>> lnHenry_matrix = [[0.0, 0.0, 0.0], [22.13581843104147, 0.0, 0.0], [22.
\hookrightarrow239038459475733, 0.0, 0.0]]
>>> dlnHenry_matrix_dT = [[0.0, 0.0, 0.0], [0.0171139888888888904, 0.0, 0.0], [0.
๑015461911111111101, 0.0, 0.0]]
>>> d2lnHenry_matrix_dT2 = [[0.0, 0.0, 0.0], [-0.0004070325925925928, 0.0, 0.0], [-
\rightarrow 0 . 0 0 0 3 4 0 1 6 5 1 8 5 1 8 5 1 8 5 2 4 , ~ 0 . 0 , ~ 0 . 0 ] ] ~
>>> d2Henry_constants_dT2(lnHenry_matrix, dlnHenry_matrix_dT, d2lnHenry_matrix_dT2,,
[0.8, 0.15, 0.05], [False, True, True], True)
[0.0, -468723.574327235, -460276.89146166]

```

\subsection*{1.26.2 Utility functions}
chemicals.solubility.solubility_eutectic (T, Tm, \(H m, C p l=0, C p s=0\), gamma=1)
Returns the maximum solubility of a solute in a solvent.
\[
\begin{gathered}
\ln x_{i}^{L} \gamma_{i}^{L}=\frac{\Delta H_{m, i}}{R T}\left(1-\frac{T}{T_{m, i}}\right)-\frac{\Delta C_{p, i}\left(T_{m, i}-T\right)}{R T}+\frac{\Delta C_{p, i}}{R} \ln \frac{T_{m}}{T} \\
\Delta C_{p, i}=C_{p, i}^{L}-C_{p, i}^{S}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the system [K]
Tm [float] Melting temperature of the solute [K]
\(\mathbf{H m}\) [float] Heat of melting at the melting temperature of the solute [ \(\mathrm{J} / \mathrm{mol}\) ]
Cpl [float, optional] Molar heat capacity of the solute as a liquid [J/mol/K]
Cps: float, optional Molar heat capacity of the solute as a solid [J/mol/K]
gamma [float, optional] Activity coefficient of the solute as a liquid [-]

\section*{Returns}
\(\mathbf{x}\) [float] Mole fraction of solute at maximum solubility [-]

\section*{Notes}
gamma is of the solute in liquid phase

\section*{References}
[1]

\section*{Examples}

From [1], matching example
```

>>> solubility_eutectic(T=260., Tm=278.68, Hm=9952., Cpl=0, Cps=0, gamma=3.0176)

```
0.243400713

\section*{chemicals.solubility.solubility_parameter(T, Hvapm, Vml)}

This function handles the calculation of a chemical's solubility parameter. Calculation is a function of temperature, but is not always presented as such. Hvapm, Vml, T are required.
\[
\delta=\sqrt{\frac{\Delta H_{v a p}-R T}{V_{m}}}
\]

\section*{Parameters}

T [float] Temperature of the fluid [k]
Hvapm [float] Heat of vaporization [J/mol/K]
Vml [float] Specific volume of the liquid [m^3/mol]

\section*{Returns}
delta [float] Solubility parameter, \(\left[\mathrm{Pa}^{\wedge} 0.5\right]\)

\section*{Notes}

Undefined past the critical point. For convenience, if Hvap is not defined, an error is not raised; None is returned instead. Also for convenience, if Hvapm is less than RT, None is returned to avoid taking the root of a negative number.

This parameter is often given in units of \(\mathrm{cal} / \mathrm{ml}\), which is 2045.48 times smaller than the value returned here.

\section*{References}
[1]

\section*{Examples}

Pentane at STP
>>> solubility_parameter(T=298.2, Hvapm=26403.3, Vml=0.000116055) 14357.68128600315
chemicals.solubility.Tm_depression_eutectic (Tm, Hm, \(x=\) None, \(M=\) None, \(M W=\) None)
Returns the freezing point depression caused by a solute in a solvent. Can use either the mole fraction of the solute or its molality and the molecular weight of the solvent. Assumes ideal system behavior.
\[
\Delta T_{m}=\frac{R T_{m}^{2} x}{\Delta H_{m}}
\]
\[
\Delta T_{m}=\frac{R T_{m}^{2}(M W) M}{1000 \Delta H_{m}}
\]

\section*{Parameters}

Tm [float] Melting temperature of the solute [K]
\(\mathbf{H m}\) [float] Heat of melting at the melting temperature of the solute [ \(\mathrm{J} / \mathrm{mol}\) ]
x [float, optional] Mole fraction of the solute [-]
M [float, optional] Molality [mol/kg]
MW: float, optional Molecular weight of the solvent [g/mol]

\section*{Returns}
dTm [float] Freezing point depression [K]

\section*{Notes}

MW is the molecular weight of the solvent. M is the molality of the solute.

\section*{References}
[1]

\section*{Examples}

From [1], matching example.
```

>>> Tm_depression_eutectic(353.35, 19110, .02)
1.0864598583150

```

\subsection*{1.27 ITS Temperature Scales (chemicals.temperature)}

This module contains functionality for converting between the temperature scales ITS-90, ITS-76, ITS-68, ITS-48, and ITS-27. These historical temperature scales can deviate quite a bit from modern temperature measurements! It is important to convert old measurements of temperature to their modern equivalent.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

\footnotetext{
- Conversion functions
}

\subsection*{1.27.1 Conversion functions}

\section*{chemicals.temperature.T_converter ( \(T\), current, desired)}

Converts the a temperature reading made in any of the scales 'ITS-90', 'ITS-68','ITS-48', 'ITS-76', or 'ITS-27' to any of the other scales. Not all temperature ranges can be converted to other ranges; for instance, 'ITS-76' is purely for low temperatures, and 5 K on it has no conversion to 'ITS-90' or any other scale. Both a conversion to ITS-90 and to the desired scale must be possible for the conversion to occur. The conversion uses cubic spline interpolation.
ITS-68 conversion is valid from 14 K to 4300 K . ITS-48 conversion is valid from 93.15 K to 4273.15 K ITS-76 conversion is valid from 5 K to 27 K . ITS-27 is valid from 903.15 K to 4273.15 k .

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature, on current scale [K]
current [str] String representing the scale T is in, 'ITS-90', 'ITS-68', 'ITS-48', 'ITS-76', or 'ITS-27'.
desired [str] String representing the scale T will be returned in, 'ITS-90', 'ITS-68', 'ITS-48', 'ITS-76', or 'ITS-27'.

\section*{Returns}
\(\mathbf{T}\) [float] Temperature, on scale desired [K]

\section*{Notes}

Because the conversion is performed by spline functions, a re-conversion of a value will not yield exactly the original value. However, it is quite close.

The use of splines is quite quick ( 20 micro seconds/calculation). While just a spline for one-way conversion could be used, a numerical solver would have to be used to obtain an exact result for the reverse conversion. This was found to take approximately \(1 \mathrm{~ms} /\) calculation, depending on the region.

\section*{References}
[1], [2]

\section*{Examples}
>>> T_converter(500, 'ITS-68', 'ITS-48')
499.9470092992346
chemicals.temperature.ITS90_68_difference( \(T\) )
Calculates the difference between ITS-90 and ITS-68 scales using a series of models listed in [1], [2], and [3].
The temperature difference is given by the following equations:
From 13.8 K to 73.15 K:
\[
T_{90}-T_{68}=a_{0}+\sum_{i=1}^{12} a_{i}\left[\left(T_{90} / K-40\right) / 40\right]^{i}
\]

From 83.8 K to 903.75 K:
\[
T_{90}-T_{68}=\sum_{i=1}^{8} b_{i}\left[\left(T_{90} / K-273.15\right) / 630\right]^{i}
\]

From 903.75 K to 1337.33 K :
\[
T_{90}-T_{68}=\sum_{i=0}^{5} c_{i}\left[T_{90} /{ }^{\circ} C\right]^{i}
\]

Above 1337.33 K :
\[
T_{90}-T_{68}=-1.398 \cdot 10^{-7}\left(\frac{T_{90}}{K}\right)^{2}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature, ITS-90, or approximately ITS-68 [K]

\section*{Returns}
dT [float] Temperature, difference between ITS-90 and ITS-68 at T [K]

\section*{Notes}

The conversion is straightforward when T90 is known. Theoretically, the model should be solved numerically to convert the reverse way. However, according to [4], the difference is under 0.05 mK from 73.15 K to 903.15 K , and under 0.26 mK up to 1337.33 K .

For temperatures under 13.8 K , no conversion is performed.
The first set of coefficients is:
\(-0.005903,0.008174,-0.061924,-0.193388,1.490793,1.252347,-9.835868,1.411912,25.277595,-19.183815\), \(-18.437089,27.000895,-8.716324\).

The second set of coefficients is:
\(0,-0.148759,-0.267408,1.08076,1.269056,-4.089591,-1.871251,7.438081,-3.536296\).
The third set of coefficients is:
\(7.8687209 \mathrm{E} 1,-4.7135991 \mathrm{E}-1,1.0954715 \mathrm{E}-3,-1.2357884 \mathrm{E}-6,6.7736583 \mathrm{E}-10,-1.4458081 \mathrm{E}-13\).
These last coefficients use the temperature in degrees Celcius. A slightly older model used the following coefficients but a different equation over the same range:
\(-0.00317,-0.97737,1.2559,2.03295,-5.91887,-3.23561,7.23364,5.04151\).
The model for these coefficients was:
\[
T_{90}-T_{68}=c_{0}+\sum_{i=1}^{7} c_{i}\left[\left(T_{90} / K-1173.15\right) / 300\right]^{i}
\]

For temperatures larger than several thousand K , the differences have no meaning and grows quadratically.

\section*{References}
[1], [2], [3], [4]

\section*{Examples}
>>> ITS90_68_difference(1000.)
0.01231818956580355

\subsection*{1.28 Thermal Conductivity (chemicals.thermal_conductivity)}

This module contains various thermal conductivity estimation routines, dataframes of fit coefficients, and mixing rules.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Pure Low Pressure Liquid Correlations
- Pure High Pressure Liquid Correlations
- Liquid Mixing Rules
- Pure Low Pressure Gas Correlations
- Pure High Pressure Gas Correlations
- Gas Mixing Rules
- Correlations for Specific Substances
- Fit Correlations
- Fit Coefficients

\subsection*{1.28.1 Pure Low Pressure Liquid Correlations}
chemicals.thermal_conductivity.Sheffy_Johnson(T, MW, Tm)
Calculate the thermal conductivity of a liquid as a function of temperature using the Sheffy-Johnson (1961) method. Requires Temperature, molecular weight, and melting point.
\[
k=1.951 \frac{1-0.00126\left(T-T_{m}\right)}{T_{m}^{0.216} M W^{0.3}}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid [ \(\mathrm{g} / \mathrm{mol}\) ]
Tm [float] Melting point of the fluid [K]

\section*{Returns}
\(\mathbf{k l}\) [float] Thermal conductivity of the fluid, W/m/k

\section*{Notes}

The origin of this equation has been challenging to trace. It is presently unknown, and untested.

\section*{References}
[1]

\section*{Examples}
>>> Sheffy_Johnson(300, 47, 280)
0.17740150413112193
chemicals.thermal_conductivity.Sato_Riedel ( \(T, M W, T b, T c\) )
Calculate the thermal conductivity of a liquid as a function of temperature using the CSP method of Sato-Riedel [1], [2], published in Reid [3]. Requires temperature, molecular weight, and boiling and critical temperatures.
\[
k=\frac{1.1053}{\sqrt{M W}} \frac{3+20\left(1-T_{r}\right)^{2 / 3}}{3+20\left(1-T_{b r}\right)^{2 / 3}}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid \([\mathrm{g} / \mathrm{mol}]\)
Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

This equation has a complicated history. It is proposed by Reid [3]. Limited accuracy should be expected. Uncheecked.

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> Sato_Riedel(300, 47, 390, 520)

```
0.21037692461337687
chemicals.thermal_conductivity.Lakshmi_Prasad ( \(T, M W\) )
Estimates thermal conductivity of pure liquids as a function of temperature using a reference fluid approach. Low accuracy but quick. Developed using several organic fluids.
\[
\lambda=0.0655-0.0005 T+\frac{1.3855-0.00197 T}{M W^{0.5}}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

This equation returns negative numbers at high T sometimes. This equation is one of those implemented by DDBST. If this results in a negative thermal conductivity, no value is returned.

\section*{References}
[1]

\section*{Examples}
```

>>> Lakshmi_Prasad(273.15, 100)
0.013664450

```
chemicals.thermal_conductivity. Gharagheizi_liquid ( \(T, M W, T b, P c\), omega)
Estimates the thermal conductivity of a liquid as a function of temperature using the CSP method of Gharagheizi [1]. A convoluted method claiming high-accuracy and using only statistically significant variable following analalysis.
Requires temperature, molecular weight, boiling temperature and critical pressure and acentric factor.
\[
\begin{gathered}
k=10^{-4}\left[10 \omega+2 P_{c}-2 T+4+1.908\left(T_{b}+\frac{1.009 B^{2}}{M W^{2}}\right)+\frac{3.9287 M W^{4}}{B^{4}}+\frac{A}{B^{8}}\right] \\
A=3.8588 M W^{8}(1.0045 B+6.5152 M W-8.9756) \\
B=16.0407 M W+2 T_{b}-27.9074
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid \([\mathrm{g} / \mathrm{mol}]\)
Tb [float] Boiling temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor of the fluid [-]

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

Pressure is internally converted into bar, as used in the original equation.
This equation was derived with 19000 points representing 1640 unique compounds.

\section*{References}
[1]

\section*{Examples}
>>> Gharagheizi_liquid(300, 40, 350, 1E6, 0.27)
0. 2171113029534838
chemicals.thermal_conductivity.Nicola_original ( \(T, M W, T c\), omega, Hfus)
Estimates the thermal conductivity of a liquid as a function of temperature using the CSP method of Nicola [1]. A simpler but long method claiming high-accuracy and using only statistically significant variable following analalysis.
Requires temperature, molecular weight, critical temperature, acentric factor and the heat of vaporization.
\[
\frac{\lambda}{1 \mathrm{Wm} / \mathrm{K}}=-0.5694-0.1436 T_{r}+5.4893 \times 10^{-10} \frac{\Delta_{\text {fus }} H}{\mathrm{kmol} / \mathrm{J}}+0.0508 \omega+\left(\frac{1 \mathrm{~kg} / \mathrm{kmol}}{M W}\right)^{0.0622}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid \([\mathrm{g} / \mathrm{mol}]\)
Tc [float] Critical temperature of the fluid [K]
omega [float] Acentric factor of the fluid [-]
Hfus [float] Heat of fusion of the fluid [ \(\mathrm{J} / \mathrm{mol}\) ]

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

A weird statistical correlation. Recent and yet to be reviewed. This correlation has been superceded by the author's later work. Hfus is internally converted to be in J/kmol.

\section*{References}
[1]

\section*{Examples}
>>> Nicola_original(300, 142.3, 611.7, 0.49, 201853)
Q. 2305018632230984
chemicals.thermal_conductivity.Nicola(T, \(M W, T c, P c\), omega)
Estimates the thermal conductivity of a liquid as a function of temperature using the CSP method of [1]. A statistically derived equation using any correlated terms.

Requires temperature, molecular weight, critical temperature and pressure, and acentric factor.
\[
\frac{\lambda}{0.5147 W / m / K}=-0.2537 T_{r}+\frac{0.0017 P c}{\operatorname{bar}}+0.1501 \omega+\left(\frac{1}{M W}\right)^{-0.2999}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid \([\mathrm{g} / \mathrm{mol}\) ]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor of the fluid [-]

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

A statistical correlation. A revision of an original correlation.

\section*{References}
[1]

\section*{Examples}
```

>>> Nicola(300, 142.3, 611.7, 2110000.0, 0.49)

```
0. 10863821554584034
chemicals.thermal_conductivity.Bahadori_liquid \((T, M W)\)
Estimates the thermal conductivity of parafin liquid hydrocarbons. Fits their data well, and is useful as only MW is required. X is the Molecular weight, and Y the temperature.
\[
\begin{gathered}
K=a+b Y+C Y^{2}+d Y^{3} \\
a=A_{1}+B_{1} X+C_{1} X^{2}+D_{1} X^{3} \\
b=A_{2}+B_{2} X+C_{2} X^{2}+D_{2} X^{3} \\
c=A_{3}+B_{3} X+C_{3} X^{2}+D_{3} X^{3} \\
d=A_{4}+B_{4} X+C_{4} X^{2}+D_{4} X^{3}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

The accuracy of this equation has not been reviewed.

\section*{References}

\section*{[1]}

\section*{Examples}

Data point from [1].
```

>>> Bahadori_liquid(273.15, 170)
0.1427427810827268

```
chemicals.thermal_conductivity.kl_Mersmann_Kind \((T, M W, T c, V c, n a)\)
Estimates the thermal conductivity of organic liquid substances according to the method of [1].
\[
\begin{aligned}
& \lambda^{*}=\frac{\lambda \cdot V_{c}^{2 / 3} \cdot T_{c} \cdot \mathrm{MW}^{0.5}}{\left(k \cdot T_{c}\right)^{1.5} \cdot N_{A}^{7 / 6}} \\
& \lambda^{*}=\frac{2}{3}\left(n_{a}+40 \sqrt{1-T_{r}}\right)
\end{aligned}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
MW [float] Molecular weight of the fluid [ \(\mathrm{g} / \mathrm{mol}\) ]
Tc [float] Critical temperature of the fluid [K]
Vc [float] Critical volume of the fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
na [float] Number of atoms in the molecule, [-]

\section*{Returns}
kl [float] Estimated liquid thermal conductivity [W/m/k]

\section*{Notes}

In the equation, all quantities must be in SI units but \(\mathrm{N} \_\mathrm{A}\) is in a kmol basis and Vc is in units of ( \(\mathrm{m}^{\wedge} 3 / \mathrm{kmol}\) ); this is converted internally.

\section*{References}
[1]

\section*{Examples}

Dodecane at 400 K :
>>> kl_Mersmann_Kind(400, 170.33484, 658.0,
... 0.000754 , 38)
0.0895271829899285

\subsection*{1.28.2 Pure High Pressure Liquid Correlations}
chemicals.thermal_conductivity. DIPPR9G \((T, P, T c, P c, k l)\)
Adjustes for pressure the thermal conductivity of a liquid using an emperical formula based on [1], but as given in [2].
\[
k=k^{*}\left[0.98+0.0079 P_{r} T_{r}^{1.4}+0.63 T_{r}^{1.2}\left(\frac{P_{r}}{30+P_{r}}\right)\right]
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
\(\mathbf{P}\) [float] Pressure of fluid [Pa]
Tc: float Critical point of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
kl [float] Thermal conductivity of liquid at 1 atm or saturation, [W/m/K]

\section*{Returns}
kl_dense [float] Thermal conductivity of liquid at \(\mathrm{P},[\mathrm{W} / \mathrm{m} / \mathrm{K}\) ]

\section*{Notes}

This equation is entrely dimensionless; all dimensions cancel. The original source has not been reviewed.
This is DIPPR Procedure 9G: Method for the Thermal Conductivity of Pure Nonhydrocarbon Liquids at High Pressures

\section*{References}
[1], [2]

\section*{Examples}

From [2], for butyl acetate.
>>> DIPPR9G(515.05, 3.92E7, 579.15, 3.212E6, 7.085E-2)
0.0864419738671184
chemicals.thermal_conductivity.Missenard ( \(T, P, T c, P c, k l\) )
Adjustes for pressure the thermal conductivity of a liquid using an emperical formula based on [1], but as given in [2].
\[
\frac{k}{k^{*}}=1+Q P_{r}^{0.7}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
\(\mathbf{P}\) [float] Pressure of fluid [Pa]
Tc: float Critical point of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
kl [float] Thermal conductivity of liquid at 1 atm or saturation, [W/m/K]

\section*{Returns}
kl_dense [float] Thermal conductivity of liquid at \(\mathrm{P},[\mathrm{W} / \mathrm{m} / \mathrm{K}\) ]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. An interpolation routine is used here from tabulated values of Q . The original source has not been reviewed.

\section*{References}
[1], [2]

\section*{Examples}

Example from [2], toluene; matches.
>>> Missenard(304., 6330E5, 591.8, 41E5, 0.129)
0. 2198375777069657

\subsection*{1.28.3 Liquid Mixing Rules}

\section*{chemicals.thermal_conductivity.DIPPR9H(ws, ks)}

Calculates thermal conductivity of a liquid mixture according to mixing rules in [1] and also in [2].
\[
\lambda_{m}=\left(\sum_{i} w_{i} \lambda_{i}^{-2}\right)^{-1 / 2}
\]

This is also called the Vredeveld (1973) equation. A review in [3] finds this the best model on average. However, they did caution that in some cases a linear mole-fraction mixing rule performs better. This equation according to Poling [1] should not be used if some components have thermal conductivities more than twice other components. They also say this should not be used with water.

\section*{Parameters}
ws [float] Mass fractions of components
ks [float] Liquid thermal conductivites of all components, [W/m/K]

\section*{Returns}
kl [float] Thermal conductivity of liquid mixture, [W/m/K]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The example is from [2]; all results agree. The original source has not been reviewed.
DIPPR Procedure 9H: Method for the Thermal Conductivity of Nonaqueous Liquid Mixtures
Average deviations of \(3 \%\). for 118 nonaqueous systems with 817 data points. Max deviation \(20 \%\). According to DIPPR.

In some sources, this equation is given with the molecular weights included:
\[
\lambda_{m}^{-2}=\frac{\sum_{i} z_{i} M W_{i} \lambda_{i}^{-2}}{\sum_{i} z_{i} M W_{i}}
\]

\section*{References}
[1], [2], [3]

\section*{Examples}
```

>>> DIPPR9H([0.258, 0.742], [0.1692, 0.1528])
0.15657104706719646

```
chemicals.thermal_conductivity.DIPPR9I ( \(z s, V m s, k s\) )
Calculates thermal conductivity of a liquid mixture according to mixing rules in [1]. This is recommended in [2] for aqueous and nonaqueous systems.
\[
\begin{gathered}
k_{m i x}=\sum_{i} \sum_{j} \phi_{i} \phi_{j} k_{i, j} \\
k_{i, j}=\frac{2}{\frac{1}{k_{i}}+\frac{1}{k_{j}}}
\end{gathered}
\]
\[
\phi_{i}=\frac{z_{i} V_{m, i}}{\sum_{j}^{n} z_{j} V_{m, j}}
\]

\section*{Parameters}
zs [list[float]] Mole fractions of components, [-]
Vms [list[float]] Molar volumes of each component, [m^3/mol]
\(\mathbf{k s}\) [float] Liquid thermal conductivites of all components, [W/m/K]

\section*{Returns}
kl [float] Thermal conductivity of liquid mixture, [W/m/K]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The example is from [2]; all results agree.
[2] found average deviations of 4-6\% for 118 nonaqueous systems and 15 aqueous systems at atmospheric pressure, with a maximum deviation of \(33 \%\).

The computational complexity here is \(\mathrm{N}^{\wedge} 2\), with a division present in the inner loop.

\section*{References}
[1], [2]

\section*{Examples}
>>> DIPPR9I(zs=[.682, .318], Vms=[1.723e-2, 7.338e-2], ks=[.6037, .1628])
0. 25397430656658937
chemicals.thermal_conductivity.Filippov(ws, ks)
Calculates thermal conductivity of a binary liquid mixture according to mixing rules in [2] as found in [1].
\[
\lambda_{m}=w_{1} \lambda_{1}+w_{2} \lambda_{2}-0.72 w_{1} w_{2}\left(\lambda_{2}-\lambda_{1}\right)
\]

\section*{Parameters}
ws [float] Mass fractions of components
ks [float] Liquid thermal conductivites of all components, [W/m/K]

\section*{Returns}
kl [float] Thermal conductivity of liquid mixture, [W/m/K]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The original source has not been reviewed. Only useful for binary mixtures.

\section*{References}
[1], [2]

\section*{Examples}
>>> Filippov([0.258, 0.742], [0.1692, 0.1528])
0.15929167628799998

\subsection*{1.28.4 Pure Low Pressure Gas Correlations}

\section*{chemicals.thermal_conductivity.Eucken( \(M W, C v m, m u\) )}

Estimates the thermal conductivity of a gas as a function of temperature using the CSP method of Eucken [1].
\[
\frac{\lambda M W}{\eta C_{v}}=1+\frac{9 / 4}{C_{v} / R}
\]

\section*{Parameters}

MW [float] Molecular weight of the gas [g/mol]
Cvm [float] Molar contant volume heat capacity of the gas [ \(\mathrm{J} / \mathrm{mol} / \mathrm{K}\) ]
mu [float] Gas viscosity [ Pa *s]

\section*{Returns}
kg [float] Estimated gas thermal conductivity [W/m/k]

\section*{Notes}

Temperature dependence is introduced via heat capacity and viscosity. A theoretical equation. No original author located. MW internally converted to \(\mathrm{kg} / \mathrm{g}-\mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}

2-methylbutane at low pressure, 373.15 K . Mathes calculation in [1].
>>> Eucken(MW=72.151, Cvm=135.9, mu=8.77E-6)
0.018792645058456698

\section*{chemicals.thermal_conductivity.Eucken_modified( \(M W, C v m, m u\) )}

Estimates the thermal conductivity of a gas as a function of temperature using the Modified CSP method of Eucken [1].
\[
\frac{\lambda M W}{\eta C_{v}}=1.32+\frac{1.77}{C_{v} / R}
\]

\section*{Parameters}

MW [float] Molecular weight of the gas [g/mol]
Cvm [float] Molar contant volume heat capacity of the gas [J/mol/K]
mu [float] Gas viscosity [ Pa *s]

\section*{Returns}
\(\mathbf{k g}\) [float] Estimated gas thermal conductivity [W/m/k]

\section*{Notes}

Temperature dependence is introduced via heat capacity and viscosity. A theoretical equation. No original author located. MW internally converted to \(\mathrm{kg} / \mathrm{g}-\mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}

2-methylbutane at low pressure, 373.15 K . Mathes calculation in [1].
```

>>> Eucken_modified(MW=72.151, Cvm=135.9, mu=8.77E-6)

```
0.02359353760551249
chemicals.thermal_conductivity. \(\operatorname{DIPPR9B}(T, M W, C v m, m u, T c=N o n e\), chemtype \(=\) None \()\)
Calculates the thermal conductivity of a gas using one of several emperical equations developed in [1], [2], and presented in [3].

For monoatomic gases:
\[
k=2.5 \frac{\eta C_{v}}{M W}
\]

For linear molecules:
\[
k=\frac{\eta}{M W}\left(1.30 C_{v}+14644.00-\frac{2928.80}{T_{r}}\right)
\]

For nonlinear molecules:
\[
k=\frac{\eta}{M W}\left(1.15 C_{v}+16903.36\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]
MW [float] Molwcular weight of fluid [ \(\mathrm{g} / \mathrm{mol}\) ]
Cvm [float] Molar heat capacity at constant volume of fluid, [J/mol/K]
mu [float] Viscosity of gas, [ Pa *s]

\section*{Returns}
\(\mathbf{k}\) _g [float] Thermal conductivity of gas, [W/m/k]

\section*{Notes}

Tested with DIPPR values. Cvm is internally converted to \(\mathrm{J} / \mathrm{kmol} / \mathrm{K}\).

\section*{References}
[1], [2], [3]

\section*{Examples}

CO:
>>> DIPPR9B(200., 28.01, 20.826, 1.277E-5, 132.92, chemtype='linear')
0.01813208676438415
chemicals.thermal_conductivity. Chung ( \(T, M W, T c\), omega, \(C v m, m u\) )
Estimates the thermal conductivity of a gas as a function of temperature using the CSP method of Chung [1].
\[
\begin{gathered}
\frac{\lambda M W}{\eta C_{v}}=\frac{3.75 \Psi}{C_{v} / R} \\
\Psi=1+\alpha\{[0.215+0.28288 \alpha-1.061 \beta+0.26665 Z] /[0.6366+\beta Z+1.061 \alpha \beta]\} \\
\alpha=\frac{C_{v}}{R}-1.5 \\
\beta=0.7862-0.7109 \omega+1.3168 \omega^{2} \\
Z=2+10.5 T_{r}^{2}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the gas [K]
MW [float] Molecular weight of the gas [ \(\mathrm{g} / \mathrm{mol}\) ]
Tc [float] Critical temperature of the gas [K]
omega [float] Acentric factor of the gas [-]
Cvm [float] Molar contant volume heat capacity of the gas [J/mol/K]
\(\mathbf{m u}\) [float] Gas viscosity [ \(\mathrm{Pa}^{*}\) s]

\section*{Returns}
kg [float] Estimated gas thermal conductivity [W/m/k]

\section*{Notes}

MW internally converted to \(\mathrm{kg} / \mathrm{g}-\mathrm{mol}\).

\section*{References}
[1], [2]

\section*{Examples}

2-methylbutane at low pressure, 373.15 K . Mathes calculation in [2].
>>> Chung(T=373.15, MW=72.151, Tc=460.4, omega=0.227, Cvm=135.9, mu=8.77E-6)
0.023015653797111124
chemicals.thermal_conductivity.Eli_Hanley (T, \(M W, T c, V c, Z c\), omega, \(C v m\) )
Estimates the thermal conductivity of a gas as a function of temperature using the reference fluid method of Eli and Hanley [1] as shown in [2].
\[
\begin{gathered}
\lambda=\lambda^{*}+\frac{\eta^{*}}{M W}(1.32)\left(C_{v}-\frac{3 R}{2}\right) \\
T r=\min (T r, 2) \\
\theta=1+(\omega-0.011)\left(0.56553-0.86276 \ln T r-\frac{0.69852}{T r}\right) \\
\psi=[1+(\omega-0.011)(0.38560-1.1617 \ln T r)] \frac{0.288}{Z_{c}} \\
f=\frac{T_{c}}{190.4} \theta \\
h=\frac{V_{c}}{9.92 E-5} \psi \\
T_{0}=T / f \\
\eta_{0}^{*}\left(T_{0}\right)=\sum_{n=1}^{9} C_{n} T_{0}^{(n-4) / 3} \\
\theta_{0}=1944 \eta_{0} \\
\lambda^{*}=\lambda_{0} H \\
\eta^{*}=\eta_{0}^{*} H \frac{M W}{16.04} \\
H=\left(\frac{16.04}{M W}\right)^{0.5} f^{0.5} / h^{2 / 3}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the gas [K]
MW [float] Molecular weight of the gas \([\mathrm{g} / \mathrm{mol}]\)
Tc [float] Critical temperature of the gas [K]
Vc [float] Critical volume of the gas [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
Zc [float] Critical compressibility of the gas []
omega [float] Acentric factor of the gas [-]
Cvm [float] Molar contant volume heat capacity of the gas [ \(\mathrm{J} / \mathrm{mol} / \mathrm{K}\) ]

\section*{Returns}
\(\mathbf{k g}\) [float] Estimated gas thermal conductivity [W/m/k]

\section*{Notes}

Reference fluid is Methane. MW internally converted to \(\mathrm{kg} / \mathrm{g}-\mathrm{mol}\).

\section*{References}
[1], [2]

\section*{Examples}

2-methylbutane at low pressure, 373.15 K . Matches calculation in [2].
>>> Eli_Hanley(T=373.15, MW=72.151, Tc=460.4, Vc=3.06E-4, Zc=0.267,
... omega=0.227, Cvm=135.9)
0.02247951724513664
chemicals.thermal_conductivity. Gharagheizi_gas ( \(T, M W, T b, P c\), omega)
Estimates the thermal conductivity of a gas as a function of temperature using the CSP method of Gharagheizi [1]. A convoluted method claiming high-accuracy and using only statistically significant variable following analalysis.
Requires temperature, molecular weight, boiling temperature and critical pressure and acentric factor.
\[
\begin{gathered}
k=7.9505 \times 10^{-4}+3.989 \times 10^{-5} T-5.419 \times 10^{-} 5 M W+3.989 \times 10^{-5} A \\
A=\frac{\left(2 \omega+T-\frac{(2 \omega+3.2825) T}{T_{b}}+3.2825\right)}{0.1 M P_{c} T} \times\left(3.9752 \omega+0.1 P_{c}+1.9876 B+6.5243\right)^{2}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
MW: float Molecular weight of the fluid [ \(\mathrm{g} / \mathrm{mol}\) ]
Tb [float] Boiling temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor of the fluid [-]

\section*{Returns}
kg [float] Estimated gas thermal conductivity [W/m/k]

\section*{Notes}

Pressure is internally converted into \(10 * \mathrm{kPa}\) but author used correlation with kPa ; overall, errors have been corrected in the presentation of the formula.
This equation was derived with 15927 points and 1574 compounds. Example value from [1] is the first point in the supportinf info, for CH 4 .

\section*{References}
[1]

\section*{Examples}
\(\gg\) Gharagheizi_gas(580., 16.04246, 111.66, 4599000.0, 0.0115478000)
0.09594861261873211
chemicals.thermal_conductivity.Bahadori_gas ( \(T, M W\) )
Estimates the thermal conductivity of hydrocarbons gases at low P. Fits their data well, and is useful as only MW is required. Y is the Molecular weight, and X the temperature.
\[
\begin{gathered}
K=a+b Y+C Y^{2}+d Y^{3} \\
a=A_{1}+B_{1} X+C_{1} X^{2}+D_{1} X^{3} \\
b=A_{2}+B_{2} X+C_{2} X^{2}+D_{2} X^{3} \\
c=A_{3}+B_{3} X+C_{3} X^{2}+D_{3} X^{3} \\
d=A_{4}+B_{4} X+C_{4} X^{2}+D_{4} X^{3}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the gas [K]
MW [float] Molecular weight of the gas \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}
\(\mathbf{k g}\) [float] Estimated gas thermal conductivity [W/m/k]

\section*{Notes}

The accuracy of this equation has not been reviewed.

\section*{References}
[1]

\section*{Examples}
```

>>> Bahadori_gas(40+273.15, 20.0) \# Point from article
0.03196816533787329

```

\subsection*{1.28.5 Pure High Pressure Gas Correlations}
chemicals.thermal_conductivity.Stiel_Thodos_dense ( \(T, M W, T c, P c, V c, Z c, V m, k g\) )
Estimates the thermal conductivity of a gas at high pressure as a function of temperature using difference method of Stiel and Thodos [1] as shown in [2].
if \(\rho_{r}<0.5\) :
\[
\left(\lambda-\lambda^{\circ}\right) \Gamma Z_{c}^{5}=1.22 \times 10^{-2}\left[\exp \left(0.535 \rho_{r}\right)-1\right]
\]
if \(0.5<\rho_{r}<2.0\) :
\[
\left(\lambda-\lambda^{\circ}\right) \Gamma Z_{c}^{5}=1.22 \times 10^{-2}\left[\exp \left(0.535 \rho_{r}\right)-1\right]
\]
if \(2<\rho_{r}<2.8\) :
\[
\begin{aligned}
\left(\lambda-\lambda^{\circ}\right) \Gamma Z_{c}^{5} & =1.22 \times 10^{-2}\left[\exp \left(0.535 \rho_{r}\right)-1\right] \\
\Gamma & =210\left(\frac{T_{c} M W^{3}}{P_{c}^{4}}\right)^{1 / 6}
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the gas [K]
MW [float] Molecular weight of the gas [ \(\mathrm{g} / \mathrm{mol}\) ]
Tc [float] Critical temperature of the gas [K]
Pc [float] Critical pressure of the gas [Pa]
Vc [float] Critical volume of the gas [m^3/mol]
Zc [float] Critical compressibility of the gas [-]
Vm [float] Molar volume of the gas at T and \(\mathrm{P}\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)
\(\mathbf{k g}\) [float] Low-pressure gas thermal conductivity [W/m/k]

\section*{Returns}
\(\mathbf{k g}\) [float] Estimated dense gas thermal conductivity [W/m/k]

\section*{Notes}

Pc is internally converted to bar.

\section*{References}
[1], [2]

\section*{Examples}
>> Stiel_Thodos_dense(T=378.15, MW=44.013, Tc=309.6, Pc=72.4E5,
... Vc=97.4E-6, Zc=0.274, Vm=144E-6, kg=2.34E-2)
0.041245574404863684
chemicals.thermal_conductivity.Eli_Hanley_dense( \(T, M W, T c, V c, Z c\), omega, \(C v m, V m\) )
Estimates the thermal conductivity of a gas at high pressure as a function of temperature using the reference fluid method of Eli and Hanley [1] as shown in [2].
\[
\begin{aligned}
& \operatorname{Tr}=\min (T r, 2) \\
& V r=\min (V r, 2) \\
& f=\frac{T_{c}}{190.4} \theta \\
& h=\frac{V_{c}}{9.92 E-5} \psi \\
& T_{0}=T / f \\
& \rho_{0}=\frac{16.04}{V} h \\
& \theta=1+(\omega-0.011)\left(0.09057-0.86276 \ln T r+\left(0.31664-\frac{0.46568}{T r}\right)\left(V_{r}-0.5\right)\right) \\
& \psi=\left[1+(\omega-0.011)\left(0.39490\left(V_{r}-1.02355\right)-0.93281\left(V_{r}-0.75464\right) \ln T_{r}\right] \frac{0.288}{Z_{c}}\right. \\
& \lambda_{1}=1944 \eta_{0} \\
& \lambda_{2}=\left\{b_{1}+b_{2}\left[b_{3}-\ln \left(\frac{T_{0}}{b_{4}}\right)\right]^{2}\right\} \rho_{0} \\
& \lambda_{3}=\exp \left(a_{1}+\frac{a_{2}}{T_{0}}\right)\left\{\exp \left[\left(a_{3}+\frac{a_{4}}{T_{0}^{1.5}}\right) \rho_{0}^{0.1}+\left(\frac{\rho_{0}}{0.1617}-1\right) \rho_{0}^{0.5}\left(a_{5}+\frac{a_{6}}{T_{0}}+\frac{a_{7}}{T_{0}^{2}}\right)\right]-1\right\} \\
& \lambda^{* *}=\left[\lambda_{1}+\lambda_{2}+\lambda_{3}\right] H \\
& H=\left(\frac{16.04}{M W}\right)^{0.5} f^{0.5} / h^{2 / 3} \\
& X=\left\{\left[1-\frac{T}{f}\left(\frac{d f}{d T}\right)_{v}\right] \frac{0.288}{Z_{c}}\right\}^{1.5} \\
& \left(\frac{d f}{d T}\right)_{v}=\frac{T_{c}}{190.4}\left(\frac{d \theta}{d T}\right)_{v} \\
& \left(\frac{d \theta}{d T}\right)_{v}=(\omega-0.011)\left[\frac{-0.86276}{T}+\left(V_{r}-0.5\right) \frac{0.46568 T_{c}}{T^{2}}\right]
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the gas [K]
MW [float] Molecular weight of the gas \([\mathrm{g} / \mathrm{mol}]\)
Tc [float] Critical temperature of the gas [K]
Vc [float] Critical volume of the gas [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

Zc [float] Critical compressibility of the gas [-]
omega [float] Acentric factor of the gas [-]
Cvm [float] Molar contant volume heat capacity of the gas [J/mol/K]
\(\mathbf{V m}\) [float] Volume of the gas at T and \(\mathrm{P}\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Returns}
\(\mathbf{k g}\) [float] Estimated dense gas thermal conductivity [W/m/k]

\section*{Notes}

Reference fluid is Methane. MW internally converted to \(\mathrm{kg} / \mathrm{g}-\mathrm{mol}\).

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Eli_Hanley_dense(T=473., MW=42.081, Tc=364.9, Vc=1.81E-4, Zc=0.274,
... omega=0.144, Cvm=82.70, Vm=1.721E-4)
0.06038475754109959

```
chemicals.thermal_conductivity.Chung_dense \((T, M W, T c, V c\), omega, \(C v m, V m\), mu, dipole, association=0.0)
Estimates the thermal conductivity of a gas at high pressure as a function of temperature using the reference fluid method of Chung [1] as shown in [2].
\[
\begin{gathered}
\lambda=\frac{31.2 \eta^{\circ} \Psi}{M^{\prime}}\left(G_{2}^{-1}+B_{6} y\right)+q B_{7} y^{2} T_{r}^{1 / 2} G_{2} \\
\Psi=1+\alpha\{[0.215+0.28288 \alpha-1.061 \beta+0.26665 Z] /[0.6366+\beta Z+1.061 \alpha \beta]\} \\
\alpha=\frac{C_{v}}{R}-1.5 \\
\beta=0.7862-0.7109 \omega+1.3168 \omega^{2} \\
Z=2+10.5 T_{r}^{2} \\
q=3.586 \times 10^{-3}\left(T_{c} / M^{\prime}\right)^{1 / 2} / V_{c}^{2 / 3} \\
y=\frac{V_{c}}{6 V} \\
G_{1}=\frac{1-0.5 y}{(1-y)^{3}} \\
G_{2}=\frac{\left(B_{1} / y\right)\left[1-\exp \left(-B_{4} y\right)\right]+B_{2} G_{1} \exp \left(B_{5} y\right)+B_{3} G_{1}}{B_{1} B_{4}+B_{2}+B_{3}} \\
B_{i}=a_{i}+b_{i} \omega+c_{i} \mu_{r}^{4}+d_{i} \kappa
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the gas [K]

MW [float] Molecular weight of the gas [ \(\mathrm{g} / \mathrm{mol}\) ]
Tc [float] Critical temperature of the gas [K]
Vc [float] Critical volume of the gas [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omega [float] Acentric factor of the gas [-]
Cvm [float] Molar contant volume heat capacity of the gas [J/mol/K]
Vm [float] Molar volume of the gas at T and \(\mathrm{P}\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right.\) ]
mu [float] Low-pressure gas viscosity [ Pa *s]
dipole [float] Dipole moment [debye]
association [float, optional] Association factor [-]

\section*{Returns}
\(\mathbf{k g}\) [float] Estimated dense gas thermal conductivity [W/m/k]

\section*{Notes}

MW internally converted to \(\mathrm{kg} / \mathrm{g}-\mathrm{mol}\). Vm internally converted to \(\mathrm{mL} / \mathrm{mol}\). [1] is not the latest form as presented in [1]. Association factor is assumed 0. Relates to the polarity of the gas.
Coefficients as follows:
\[
\begin{aligned}
\text { ais } & =[2.4166 \mathrm{E}+0,-5.0924 \mathrm{E}-1,6.6107 \mathrm{E}+0,1.4543 \mathrm{E}+1,7.9274 \mathrm{E}-1,-5.8634 \mathrm{E}+0,9.1089 \mathrm{E}+1] \\
\text { bis } & =[7.4824 \mathrm{E}-1,-1.5094 \mathrm{E}+0,5.6207 \mathrm{E}+0,-8.9139 \mathrm{E}+0,8.2019 \mathrm{E}-1,1.2801 \mathrm{E}+1,1.2811 \mathrm{E}+2] \\
\text { cis } & =[-9.1858 \mathrm{E}-1,-4.9991 \mathrm{E}+1,6.4760 \mathrm{E}+1,-5.6379 \mathrm{E}+0,-6.9369 \mathrm{E}-1,9.5893 \mathrm{E}+0,-5.4217 \mathrm{E}+1] \\
\text { dis } & =[1.2172 \mathrm{E}+2,6.9983 \mathrm{E}+1,2.7039 \mathrm{E}+1,7.4344 \mathrm{E}+1,6.3173 \mathrm{E}+0,6.5529 \mathrm{E}+1,5.2381 \mathrm{E}+2]
\end{aligned}
\]

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Chung_dense(T=473., MW=42.081, Tc=364.9, Vc=184.6E-6, omega=0.142,
\#.Cvm=82.67, Vm=172.1E-6, mu=134E-7, dipole=0.4)
0.06160569232570781

```

\subsection*{1.28.6 Gas Mixing Rules}
chemicals.thermal_conductivity.Lindsay_Bromley (T, ys, ks, mus, Tbs, MWs)
Calculates thermal conductivity of a gas mixture according to mixing rules in [1] and also in [2]. It is significantly more complicated than other kinetic theory models.
\[
k=\sum_{i} \frac{y_{i} k_{i}}{\sum_{j} y_{i} A_{i j}}
\]
\[
\begin{gathered}
A_{i j}=\frac{1}{4}\left\{1+\left[\frac{\eta_{i}}{\eta_{j}}\left(\frac{M W_{j}}{M W_{i}}\right)^{0.75}\left(\frac{T+S_{i}}{T+S_{j}}\right)\right]^{0.5}\right\}^{2}\left(\frac{T+S_{i j}}{T+S_{i}}\right) \\
S_{i j}=S_{j i}=\left(S_{i} S_{j}\right)^{0.5} \\
S_{i}=1.5 T_{b}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of gas [K]
ys [float] Mole fractions of gas components
ks [float] Gas thermal conductivites of all components, [W/m/K]
mus [float] Gas viscosities of all components, \([\mathrm{Pa} * \mathrm{~s}]\)
Tbs [float] Boiling points of all components, [K]
MWs [float] Molecular weights of all components, [g/mol]

\section*{Returns}
\(\mathbf{k g}\) [float] Thermal conductivity of gas mixture, [W/m/K]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The example is from [2]; all results agree. The original source has not been reviewed.
DIPPR Procedure 9D: Method for the Thermal Conductivity of Gas Mixtures
Average deviations of \(4-5 \%\) for 77 binary mixtures reviewed in [2], from 1342 points; also six ternary mixtures (70 points); max deviation observed was \(40 \%\). (DIPPR)

\section*{References}

\section*{[1], [2], [3]}

\section*{Examples}
>> Lindsay_Bromley(323.15, [0.23, 0.77], [1.939E-2, 1.231E-2], [1.002E-5, 1.015E-
\(\rightarrow 5],[248.31,248.93],[46.07,50.49])\)
0.013902644179693132
chemicals.thermal_conductivity.Wassiljewa_Herning_Zipperer (zs, ks, MWs, MW_roots=None)
Calculates thermal conductivity of a gas mixture according to the kinetic theory expression of Wassiljewa with the interaction term from the Herning-Zipperer expression. This is also used for the prediction of gas mixture viscosity.
\[
\begin{aligned}
k & =\sum \frac{y_{i} k_{i}}{\sum y_{i} A_{i j}} \\
A_{i j} & =\left(\frac{M W_{j}}{M W_{i}}\right)^{0.5}
\end{aligned}
\]

\section*{Parameters}
zs [float] Mole fractions of gas components, [-]
ks [float] gas thermal conductivites of all components, [W/m/K]
MWs [float] Molecular weights of all components, [ \(\mathrm{g} / \mathrm{mol}\) ]
MW_roots [float, optional] Square roots of molecular weights of all components; speeds up the calculation if provided, \(\left[\mathrm{g}^{\wedge} 0.5 / \mathrm{mol}^{\wedge} 0.5\right]\)

\section*{Returns}
\(\mathbf{k g}\) [float] Thermal conductivity of gas mixture, [W/m/K]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel.

\section*{References}
[1]

\section*{Examples}
>>> Wassiljewa_Herning_Zipperer(zs=[.1, .4, .5], ks=[1.002E-5, 1.15E-5, 2e-5], ь \(\rightarrow\) MWs=[40.0, 50.0, 60.0])
1.5861181979916883e-05

\subsection*{1.28.7 Correlations for Specific Substances}
chemicals.thermal_conductivity.k_IAPWS \(\left(T, r h o, C p=N o n e, C v=N o n e, m u=N o n e, d r h o \_d P=N o n e\right.\), \(\left.d r h o \_d P \_T r=N o n e\right)\)
Calculate the thermal conductivity of water or steam according to the 2011 IAPWS [1] formulation. Critical enhancement is ignored unless parameters for it are provided.
\[
\begin{gathered}
\bar{\lambda}=\bar{\lambda}_{0} \times \bar{\lambda}_{1}(\bar{T}, \bar{\rho})+\bar{\lambda}_{2}(\bar{T}, \bar{\rho}) \\
\bar{\lambda}_{0}=\frac{\sqrt{\bar{T}}}{\sum_{k=0}^{4} \frac{L_{k}}{T^{k}}} \\
\bar{\lambda}_{1}(\bar{T}, \bar{\rho})=\exp \left[\bar{\rho} \sum_{i=0}^{4}\left(\left(\frac{1}{\bar{T}}-1\right)^{i} \sum_{j=0}^{5} L_{i j}(\bar{\rho}-1)^{j}\right)\right] \\
\bar{\lambda}_{2}=\Gamma \frac{\bar{\rho} \bar{c}_{p} \bar{T}}{\bar{\mu}} Z(y) \\
y(y)=\frac{2}{\pi y}\left\{\left[\left(1-\kappa^{-1}\right) \arctan (y)+\kappa^{-1} y\right]-\left[1-\exp \left(\frac{-1}{y^{-1}+y^{-2} / 3 \bar{\rho}^{2}}\right)\right]\right\} \\
y=\bar{q}_{D} \xi(\bar{T}, \bar{\rho}) \\
\xi=\xi_{0}\left(\frac{\Delta \bar{\chi}}{\Gamma_{0}}\right)^{\nu / \gamma}
\end{gathered}
\]
\[
\begin{gathered}
\Delta \bar{\chi}(\bar{T}, \bar{\rho})=\bar{\rho}\left[\zeta(\bar{T}, \bar{\rho})-\zeta\left(\bar{T}_{R}, \bar{\rho}\right) \frac{\bar{T}_{R}}{\bar{T}}\right] \\
\zeta=\left(\frac{\partial \bar{\rho}}{\partial \bar{p}}\right)_{\bar{T}}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature water [K]
rho [float] Density of water [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
Cp [float, optional] Constant pressure heat capacity of water, [J/kg/K]
Cv [float, optional] Constant volume heat capacity of water, [J/kg/K]
\(\mathbf{m u}\) [float, optional] Viscosity of water, [ \(\mathrm{Pa} * \mathrm{~s}\) ]
drho_dP [float, optional] Partial derivative of density with respect to pressure at constant temperature, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3 / \mathrm{Pa}\right]\)
drho_dP_Tr [float, optional] Partial derivative of density with respect to pressure at constant temperature (at the reference temperature \((970.644 \mathrm{~K})\) and the actual density of water); will be calculated from the industrial formulation fit if omitted, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3 / \mathrm{Pa}\right]\)

\section*{Returns}
\(\mathbf{k}\) [float] Thermal condiuctivity, [W/m/K]

\section*{Notes}

Gamma \(=177.8514 ;\)
\(q d=0.4 \mathrm{E}-9\);
\(n u=0.630 ;\)
gamma \(=1.239 ;\)
zeta0 \(=0.13 \mathrm{E}-9 ;\)
Gamma0 \(=0.06\);
\(\mathrm{TRC}=1.5\)
The formulation uses the industrial variant of the critical enhancement. It matches to 5E-6 relative tolerance at the check temperature, and should match even closer outside it.

\section*{References}
[1]

\section*{Examples}
```

>>> k_IAPWS(647.35, 750.)
0.5976194153179502

```

Region 1, test 1, from MPEI, exact match:
```

>>> k_IAPWS(T=620., rho=613.227777440324, Cp=7634.337046792,
\#.Cv=3037.934412104, mu=70.905106751524E-6, drho_dP=5.209378197916E-6)
0.48148519510200044

```

Full scientific calculation:
>>> from chemicals.iapws import iapws95_properties, iapws95_P, iapws95_Tc
>>> from chemicals.viscosity import mu_IAPWS
\(\gg \mathrm{T}, \mathrm{P}=298.15,1 \mathrm{e} 5\)
>>> rho, _, _, _, Cv, Cp, _, _, _, _, drho_dP = iapws95_properties(T, P)
>>> P_ref = iapws95_P(1.5*iapws95_Tc, rho)
>>> _, _, _, _, _, _, _, _, _, _, drho_dP_Tr = iapws95_properties(1.5*iapws95_Tc, P_ \(\rightarrow\) ref)
>>> mu = mu_IAPWS(T, rho, drho_dP, drho_dP_Tr)
>>> k_IAPWS(T, rho, Cp, Cv, mu, drho_dP, drho_dP_Tr)
0.60651532815
chemicals.thermal_conductivity.k_air_lemmon \(\left(T, r h o, C p=N o n e, C v=N o n e, d r h o \_d P=N o n e\right.\), drho_dP_Tr=None, \(m u=\) None)
Calculate the thermal conductivity of air using the Lemmon and Jacobsen (2004) [1] formulation. The critical enhancement term is ignored unless all the rquired parameters for it are provided.
\[
\begin{gathered}
\lambda=\lambda^{0}(T)+\lambda^{r}(\tau, \delta)+\lambda^{c}(\tau, \delta) \\
\lambda^{0}=N_{1}\left[\frac{\eta^{0}(T)}{1 \mu \mathrm{~Pa} \cdot \mathrm{~s}}\right]+N_{2} \tau^{t_{2}}+N_{3} \tau^{t_{3}} \\
\lambda^{r}=\sum_{i=4}^{n} N_{i} \tau^{t_{i}} \delta^{d_{i}} \exp \left(-\gamma_{i} \delta^{l_{i}}\right) \\
\lambda^{c}=\rho C_{p} \frac{k R_{0} T}{6 \pi \xi \cdot \eta(T, \rho)}\left(\tilde{\Omega}-\tilde{\Omega}_{0}\right) \\
\tilde{\Omega}=\frac{2}{\pi}\left[\left(\frac{C_{p}-C_{v}}{C_{p}}\right) \tan ^{-1}\left(\xi / q_{D}\right)+\frac{C_{v}}{C_{p}}\left(\xi / q_{D}\right)\right] \\
\tilde{\Omega}_{0}=\frac{2}{\pi}\left\{1-\exp \left[\frac{-1}{q_{D} / \xi+1 / 3\left(\xi / q_{D}\right)^{2}\left(\rho_{c} / \rho\right)^{2}}\right]\right\} \\
\xi=\xi_{0}\left[\frac{\tilde{\chi}(T, \rho)-\tilde{\chi}\left(T_{r e f}, \rho\right) \frac{T_{r e f}}{T}}{\Gamma}\right]^{\nu / \gamma} \\
\tilde{\chi}(T, \rho)=\frac{P_{c} \rho}{\rho_{c}^{2}}\left(\frac{\partial \rho}{\partial P}\right)_{T}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature air [K]
rho [float] Molar density of air [ \(\mathrm{mol} / \mathrm{m}^{\wedge} 3\) ]

Cp [float, optional] Molar constant pressure heat capacity of air, [J/mol/K]
Cv [float, optional] Molar constant volume heat capacity of air, [J/mol/K]
mu [float, optional] Viscosity of air, [ \(\mathrm{Pa}^{*} \mathrm{~s}\) ]
drho_dP [float, optional] Partial derivative of density with respect to pressure at constant temperature, \(\left[\mathrm{mol} / \mathrm{m}^{\wedge} 3 / \mathrm{Pa}\right]\)
drho_dP_Tr [float, optional] Partial derivative of density with respect to pressure at constant temperature (at the reference temperature ( 265.262 K ) and the actual density of air), [ \(\mathrm{mol} / \mathrm{m}^{\wedge} 3 / \mathrm{Pa}\) ]

\section*{Returns}
\(\mathbf{k}\) [float] Thermal condiuctivity of air, [W/m/K]

\section*{Notes}

The constnts are as follows:
\(\mathrm{Ni}=[1.308,1.405,-1.036,8.743,14.76,-16.62,3.793,-6.142,-0.3778]\)
\(\mathrm{ti}=[\) None, \(-1.1,-0.3,0.1,0.0,0.5,2.7,0.3,1.3]\)
\(\mathrm{di}=[\) None, None, None, 1, 2, 3, 7, 7, 11]
\(\mathrm{li}=[\) None, None, None, \(0,0,2,2,2,2]\)
gammai \(=[\) None, None, None, \(0,0,1,1,1,1]\)
\(\mathrm{R} 0=1.01 ; \mathrm{Pc}=3.78502 \mathrm{E} 6 \mathrm{~Pa} ; \mathrm{xi} 0=0.11 \mathrm{E}-9 \mathrm{~nm} ; \mathrm{qd}=0.31 \mathrm{E}-9 \mathrm{~nm} ; \mathrm{Tc}=132.6312 \mathrm{~K}\) (actually the maxcondentherm); T_ref \(=265.262\) ( 2 Tc rounded differently); rhoc \(=10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3\) (actually the maxcondentherm); k \(=1.380658 \mathrm{E}-23 \mathrm{~J} / \mathrm{K} ; \mathrm{nu}=0.63\) and gamma \(=1.2415\), \(\mathrm{sigma}=0.36, \mathrm{MW}=28.9586 \mathrm{~g} / \mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}

Basic calculation at 300 K and approximately 1 bar:
```

>>> k_air_lemmon(300, 40.0)
0.0263839695044

```

Calculation near critical point:
```

>>> k_air_lemmon(132.64, 10400, 2137.078854678728, 35.24316159996235,0.
\rightarrow 0 7 4 1 7 8 7 8 6 1 4 3 1 5 7 6 9 , ~ 0 . 0 0 0 3 5 9 1 9 0 2 7 2 4 1 5 2 8 2 5 6 , ~ 1 . 7 7 6 2 2 5 3 2 6 5 8 6 8 5 9 5 e - 0 5 ) ~
0.07562307234760

```

\subsection*{1.28.8 Fit Correlations}
chemicals.thermal_conductivity. PPDS8 ( \(T, T c, a 0, a 1, a 2, a 3\) )
Calculate the thermal conductivity of a liquid using the 4-term tau polynomial developed by the PPDS and named PPDS equation 8.
\[
k_{l}=a_{0}\left(1+\sum_{i}^{3} a_{i} \tau^{i / 3}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Te [float] Critical temperature of fluid [K]
a0 [float] Coefficient, [-]
a1 [float] Coefficient, [-]
a2 [float] Coefficient, [-]
a3 [float] Coefficient, [-]

\section*{Returns}
\(\mathbf{k}\) [float] Low pressure liquid thermal conductivity, [W/(m*K)]

\section*{References}
[1]

\section*{Examples}

Sample coefficients for benzene in [1], at 500 K :
\(\gg\) PPDS8 (T=500.0, Tc=562.05, \(\mathrm{a} 0=0.0641126, \mathrm{a} 1=0.61057, \mathrm{a} 2=-1.72442, \mathrm{a} 3=3.94394)\)
0.08536381765218425
chemicals.thermal_conductivity. PPDS3 ( \(T, T c, a 1, a 2, a 3\) )
Calculate the thermal conductivity of a low-pressure gas using the 3-term \(\operatorname{Tr}\) polynomial developed by the PPDS and named PPDS equation 3 .
\[
k_{g}=\sqrt{T_{r}}\left(\sum_{i=1}^{3} \frac{a_{i}}{T_{r}^{i}}\right)^{-1}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
a1 [float] Coefficient, [-]
a2 [float] Coefficient, [-]
a3 [float] Coefficient, [-]

\section*{Returns}
\(\mathbf{k}\) [float] Low pressure gas thermal conductivity, [W/(m*K)]

\section*{References}
[1]

\section*{Examples}

Sample coefficients for pentane in [1], at 400 K :
>>> PPDS3 (T=400.0, Tc=470.008, \(\mathrm{a} 1=11.6366, \mathrm{a} 2=25.1191, \mathrm{a} 3=-7.21674)\)
0.0251734811601927
chemicals.thermal_conductivity.Chemsep_16(T, \(A, B, C, D, E)\)
Calculate the thermal conductivity of a low-pressure liquid using the 5-term \(T\) exponential polynomial found in ChemSep.
\[
k_{l}=A+\exp \left(\frac{B}{T}+C+D T+E T^{2}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [W/(m*K)]
B [float] Coefficient, [K]
C [float] Coefficient, [-]
D [float] Coefficient, [1/K]
\(\mathbf{E}\) [float] Coefficient, [1/K^2]

\section*{Returns}
\(\mathbf{k}\) [float] Low pressure liquid thermal conductivity, [W/(m*K)]

\section*{References}
[1]

\section*{Examples}

Sample coefficients for liquid thermal conductivity of n-hexane in [1], at 300 K :
```

>>> Chemsep_16(300.0, -0.12682, -1.5015, -1.0467, -0.00088709, -9.3679E-07)

```
0.11924904787869

\subsection*{1.28.9 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.thermal_conductivity.k_data_Perrys_8E_2_315
Data from [1] with chemicals. dippr. EQ100 coefficients for liquids.
chemicals.thermal_conductivity.k_data_Perrys_8E_2_314
Data from [1] with chemicals.dippr.EQ102 coefficients for gases.
chemicals.thermal_conductivity.k_data_VDI_PPDS_9
Data from [2] with polynomial coefficients for liquids.
chemicals.thermal_conductivity.k_data_VDI_PPDS_10
Data from [2] with polynomial coefficients for gases.
```

In [1]: import chemicals
In [2]: chemicals.thermal_conductivity.k_data_Perrys_8E_2_315
Out[2]:

|  | Chemical | C1 | C2 | $\ldots$ | C5 | Tmin | Tmax |
| :--- | ---: | ---: | ---: | :--- | ---: | ---: | ---: |
| CAS |  |  | $\ldots$ |  |  |  |  |
| $50-00-0$ | Formaldehyde | 0.37329 | -0.000650 | $\ldots$ | 0.0 | 204.00 | 234.00 |
| $55-21-0$ | Benzamide | 0.28485 | -0.000252 | $\ldots$ | 0.0 | 403.00 | 563.15 |
| $56-23-5$ | Carbon tetrachloride | 0.15890 | -0.000199 | $\ldots$ | 0.0 | 250.33 | 349.79 |
| $57-55-6$ | 1,2 -Propylene glycol | 0.21520 | -0.000050 | $\ldots$ | 0.0 | 213.15 | 460.75 |
| $60-29-7$ | Diethyl ether | 0.24950 | -0.000407 | $\ldots$ | 0.0 | 156.85 | 433.15 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| $10028-15-6$ | Ozone | 0.17483 | 0.000753 | $\ldots$ | 0.0 | 77.35 | 161.85 |
| $10035-10-6$ | Hydrogen bromide | 0.23400 | -0.000464 | $\ldots$ | 0.0 | 185.15 | 290.62 |
| $10102-43-9$ | Nitric oxide | 0.18780 | 0.001029 | $\ldots$ | 0.0 | 110.00 | 176.40 |
| $13511-13-2$ | Propenylcyclohexene | 0.18310 | -0.000203 | $\ldots$ | 0.0 | 199.00 | 431.65 |
| $132259-10-0$ | Air | 0.28472 | -0.001739 | $\ldots$ | 0.0 | 75.00 | 125.00 |

[340 rows x 8 columns]
In [3]: chemicals.thermal_conductivity.k_data_Perrys_8E_2_314
Out[3]:
Chemical C1 ... Tmin Tmax
CAS

| 50-00-0 | Formaldehyde | 44.847000 | $\ldots$ | 254.05 | 994.05 |
| :--- | ---: | ---: | :--- | ---: | ---: |
| $55-21-0$ | Benzamide | 0.025389 | $\ldots$ | 563.15 | 1000.00 |
| $56-23-5$ | Carbon tetrachloride | 0.000166 | $\ldots$ | 349.79 | 1000.00 |
| $57-55-6$ | $1,2-$ Propylene glycol | 0.000167 | $\ldots$ | 460.75 | 1000.00 |
| $60-29-7$ | Diethyl ether | -0.004489 | $\ldots$ | 200.00 | 600.00 |
| $\ldots$ | $\ldots$. | $\ldots$. | $\ldots$ | $\ldots$ | $\ldots$ |
| $10028-15-6$ | Ozone | 0.004315 | $\ldots$ | 161.85 | 1000.00 |
| $10035-10-6$ | Hydrogen bromide | 0.000497 | $\ldots$ | 206.45 | 600.00 |
| $10102-43-9$ | Nitric oxide | 0.000410 | $\ldots$ | 121.38 | 750.00 |
| $13511-13-2$ | Propenylcyclohexene | 0.000102 | $\ldots$ | 431.65 | 1000.00 |
| $132259-10-0$ | Air | 0.000314 | $\ldots$ | 70.00 | 2000.00 |

[345 rows x 7 columns]
In [4]: chemicals.thermal_conductivity.k_data_VDI_PPDS_9

```
```

Out[4]:
CAS
50-00-0
56-23-5
56-81-5
60-29-7
62-53-3

```

```

10097-32-2 Bromine -0.1426 _ .. 2. 2.690200e-08 -1.774400e-11
10102-44-0 Nitrogen dioxide 0.3147 ... 2.620000e-10 -6.980000e-13
10544-72-6 Dinitrogentetroxide 0.1864 ... -5.440000e-10 1.509000e-12
132259-10-0 Air -0.0006 ... 1.114335e-06 -2.670110e-09
Chemical

```

```

[271 rows x 6 columns]
In [5]: chemicals.thermal_conductivity.k_data_VDI_PPDS_10
Out[5]:
Chemical
A ...
D E
CAS
50-00-0
56-23-5
Carbon tetrachloride -2.101000e-03
\cdots... 0 0000000+00
0.000000e+00
... 0.000000e+00
0.000000e+00
56-81-5
60-29-7
62-53-3
...
Formaldehyde
0.3834 \cdots
Carbon tetrachloride
Glycerol
Diethyl ether
0.1509 ... 1.156000e-09 -2.638000e-12
0.1509 ... -7.100000e-11 3.980000e-13
0.2562 ... -1.0500000e-10 1.020000e-13
Aniline 0.2365 ... -3.600000e-11 2.1000000-14
0.2499 [.. -8.600000e-11
...
Bromine
Nitric oxide
Nitrogen dioxide
Dinitrogentetroxide
Air -0.0006 ... 1.114335e-06 -2.670110e-09
D
E
0.2365
... -3.600000e-11
A ...

| A | $\ldots$ | D | $E$ |
| ---: | :---: | ---: | ---: |
|  | $\ldots$ |  |  |
| 0.3834 | $\ldots$ | $1.156000 \mathrm{e}-09$ | $-2.638000 \mathrm{e}-12$ |
| 0.1509 | $\ldots$ | $-7.100000 \mathrm{e}-11$ | $3.980000 \mathrm{e}-13$ |
| 0.2562 | $\ldots$ | $-1.050000 \mathrm{e}-10$ | $1.020000 \mathrm{e}-13$ |
| 0.2499 | $\ldots$ | $-8.600000 \mathrm{e}-11$ | $7.300000 \mathrm{e}-14$ |
| 0.2365 | $\ldots$ | $-3.600000 \mathrm{e}-11$ | $2.100000 \mathrm{e}-14$ |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| -0.1426 | $\ldots$ | $2.690200 \mathrm{e}-08$ | $-1.774400 \mathrm{e}-11$ |
| 0.2268 | $\ldots$ | $-1.993600 \mathrm{e}-08$ | $1.448400 \mathrm{e}-11$ |
| 0.3147 | $\ldots$ | $2.620000 \mathrm{e}-10$ | $-6.980000 \mathrm{e}-13$ |
| 0.1864 | $\ldots$ | $-5.440000 \mathrm{e}-10$ | $1.509000 \mathrm{e}-12$ |
| -0.0006 | $\ldots$ | $1.114335 \mathrm{e}-06$ | $-2.670110 \mathrm{e}-09$ |

```

\subsection*{1.29.1 Triple Temperature}

\section*{chemicals.triple.Tt (CASRN, method=None)}

This function handles the retrieval of a chemical's triple temperature. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Returns data from [1], [2] or [3], or a chemical's melting point if available.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Tt [float] Triple point temperature, [K].

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, Tt_all_methods.

\section*{See also:}

Tt_methods

\section*{Notes}

Median difference between melting points and triple points is 0.02 K . Accordingly, this should be more than good enough for engineering applications.

The data in [1] is originally on the ITS-68 temperature scale, but was converted to ITS-90. The numbers were rounded to 6 decimal places arbitrarily and the conversion was performed with this library.

\section*{References}
[1], [2], [3]

\section*{Examples}

Ammonia
```

>>> Tt('7664-41-7')

```
195.49
chemicals.triple.Tt_methods (CASRN)
Return all methods available to obtain the triple temperature for the desired chemical.

\section*{Parameters}

CASRN [str] CASRN, [-]

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Tt with the given inputs.

\section*{See also:}
\(T t\)
```

chemicals.triple.Tt_all_methods = ('HEOS', 'STAVELEY', 'WEBBOOK', 'MELTING')

```

Tuple of method name keys. See the \(T t\) for the actual references

\subsection*{1.29.2 Triple Pressure}
```

chemicals.triple.Pt(CASRN, method=None)

```

This function handles the retrieval of a chemical's triple pressure. Lookup is based on CASRNs. Will automatically select a data source to use if no method is provided; returns None if the data is not available.

Returns data from [1], [2], or [3].
This function does not implement it but it is also possible to calculate the vapor pressure at the triple temperature from a vapor pressure correlation, if data is available; note most Antoine-type correlations do not extrapolate well to this low of a pressure.

\section*{Parameters}

\section*{CASRN [str] CASRN [-]}

\section*{Returns}

Pt [float] Triple point pressure, [Pa]

\section*{Other Parameters}
method [string, optional] A string for the method name to use, as defined in the variable, Pt_all_methods.

\section*{See also:}

Pt_methods

\section*{References}
[1], [2], [3]

Examples
Ammonia
>>> Pt('7664-41-7')
6053.386
chemicals.triple.Pt_methods (CASRN)
Return all methods available to obtain the Pt for the desired chemical.

\section*{Parameters}

\section*{CASRN [str] CASRN, [-]}

\section*{Returns}
methods [list[str]] Methods which can be used to obtain the Pt with the given inputs.

\section*{See also:}

Pt
```

chemicals.triple.Pt_all_methods = ('HEOS', 'STAVELEY', 'WEBBOOK')

```

Tuple of method name keys. See the \(P t\) for the actual references

\subsection*{1.30 Utilities (chemicals.utils)}

This module contains miscellaneous functions which may be useful. This includes definitions of some chemical properties, and conversions between others.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
chemicals.utils.API_to_SG(API)
Calculates specific gravity of a liquid given its API, as shown in [1].
\[
\text { SG at } 60^{\circ} \mathrm{F}=\frac{141.5}{\text { API gravity }+131.5}
\]

\section*{Parameters}

API [float] API of the fluid [-]

\section*{Returns}

SG [float] Specific gravity of the fluid at 60 degrees Farenheight [-]

\section*{Notes}

Defined only at 60 degrees Fahrenheit.

\section*{References}
[1]

\section*{Examples}
>>> API_to_SG(60.62)
0. 7365188423901728
chemicals.utils.API_to_rho (API, rho_ref=999.0170824078306)
Calculates mass density of a liquid given its API, as shown in [1].
\[
\rho 60^{\circ} \mathrm{F}=\frac{141.5 \rho_{r e f}}{\mathrm{API}+131.5}
\]

\section*{Parameters}

API [float] API of the fluid [-]
rho_ref [float, optional] Density of the reference substance, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Returns}
rho [float] Mass density the fluid at 60 degrees Farenheight \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Notes}

Defined only at 60 degrees Fahrenheit.

\section*{References}
[1]

\section*{Examples}
>>> API_to_rho(rho_to_API(820))
820.0

\section*{chemicals.utils.Cp_minus_Cv( \(\left.T, d P \_d T, d P \_d V\right)\)}

Calculate the difference between a real gas's constant-pressure heat capacity and constant-volume heat capacity, as given in [1], [2], and [3]. The required derivatives should be calculated with an equation of state.
\[
C_{p}-C_{v}=-T\left(\frac{\partial P}{\partial T}\right)_{V}^{2} /\left(\frac{\partial P}{\partial V}\right)_{T}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
dP_dT [float] Derivative of \(P\) with respect to \(T,[\mathrm{~Pa} / \mathrm{K}]\)
\(\mathbf{d P}\) _dV [float] Derivative of \(P\) with respect to \(V\), \(\left[\mathrm{Pa} * \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Returns}

Cp_minus_Cv [float] \(\mathrm{Cp}-\mathrm{Cv}\) for a real gas, \([\mathrm{J} / \mathrm{mol} / \mathrm{K}]\)

\section*{Notes}

Equivalent expressions are:
\[
\begin{aligned}
C_{p}-C_{v} & =-T\left(\frac{\partial V}{\partial T}\right)_{P}^{2} /\left(\frac{\partial V}{\partial P}\right)_{T} \\
C_{p}-C_{v} & =T\left(\frac{\partial P}{\partial T}\right)\left(\frac{\partial V}{\partial T}\right)
\end{aligned}
\]

Note that these are not second derivatives, only first derivatives, some of which are squared.

\section*{References}
[1], [2], [3]

\section*{Examples}

Calculated for hexane from the PR EOS at 299 K and 1 MPa (liquid):
>>> Cp_minus_Cv(299, 582232.475794113, -3665180614672.253)
27.654681381642394
chemicals.utils.Joule_Thomson( \(T, V, C p, d V \_d T=N o n e\), beta=None)
Calculate a real fluid's Joule Thomson coefficient. The required derivative should be calculated with an equation of state, and \(C p\) is the real fluid versions. This can either be calculated with \(d V_{-} d T\) directly, or with beta if it is already known.
\[
\mu_{J T}=\left(\frac{\partial T}{\partial P}\right)_{H}=\frac{1}{C_{p}}\left[T\left(\frac{\partial V}{\partial T}\right)_{P}-V\right]=\frac{V}{C_{p}}(\beta T-1)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
\(\mathbf{V}\) [float] Molar volume of fluid, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
\(\mathbf{C p}\) [float] Real fluid heat capacity at constant pressure, [J/mol/K]
dV_dT [float, optional] Derivative of \(V\) with respect to \(T,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
beta [float, optional] Isobaric coefficient of a thermal expansion, [1/K]

\section*{Returns}
mu_JT [float] Joule-Thomson coefficient [K/Pa]

\section*{References}
[1], [2]

\section*{Examples}

Example from [2]:
>>> Joule_Thomson(T=390, V=0.00229754, \(\mathrm{Cp}=153.235\), dV_dT=1.226396e-05)
\(1.621956080529905 \mathrm{e}-05\)
chemicals.utils.Parachor (MW, rhol, rhog, sigma)
Calculate Parachor for a pure species, using its density in the liquid and gas phases, surface tension, and molecular weight.
\[
P=\frac{\sigma^{0.25} M W}{\rho_{L}-\rho_{V}}
\]

\section*{Parameters}

MW [float] Molecular weight, \([\mathrm{g} / \mathrm{mol}]\)
rhol [float] Liquid density [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
rhog [float] Gas density [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
sigma [float] Surface tension, [N/m]

\section*{Returns}
\(\mathbf{P}\) [float] Parachor, [ \(\left.\mathrm{N}^{\wedge} 0.25 * \mathrm{~m}^{\wedge} 2.75 / \mathrm{mol}\right]\)

\section*{Notes}

To convert the output of this function to units of \(\left[\mathrm{mN}^{\wedge} 0.25 * \mathrm{~m}^{\wedge} 2.75 / \mathrm{kmol}\right]\), multiply by 5623.4132519 .
Values in group contribution tables for Parachor are often listed as dimensionless, in which they are multiplied by 5623413 and the appropriate units to make them dimensionless.

\section*{References}
[1], [2], [3]

\section*{Examples}

Calculating Parachor from a known surface tension for methyl isobutyl ketone at 293.15 K
```

>>> Parachor(100.15888, 800.8088185536124, 4.97865317223119, 0.02672166960656005)

```
\(5.088443542210164 e-05\)

Converting to the dimensionless form:
```

>>> 5623413*5.088443542210164e-05
286.14419565030687

```

Compared to 274.9 according to a group contribution method described in [3].
chemicals.utils.SG(rho, rho_ref=999.0170824078306)
Calculates the specific gravity of a substance with respect to another substance; by default, this is water at 15.555 \({ }^{\circ} \mathrm{C}\left(60^{\circ} \mathrm{F}\right)\). For gases, normally the reference density is \(1.2 \mathrm{~kg} / \mathrm{m}^{\wedge} 3\), that of dry air. However, in general specific gravity should always be specified with respect to the temperature and pressure of its reference fluid. This can vary widely.
\[
S G=\frac{\rho}{\rho_{r e f}}
\]

\section*{Parameters}
rho [float] Density of the substance, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]\)
rho_ref [float, optional] Density of the reference substance, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Returns}

SG [float] Specific gravity of the substance with respect to the reference density, [-]

\section*{Notes}

Another common reference point is water at \(4^{\circ} \mathrm{C}\) (rho_ref \(=999.9748691393087\) ). Specific gravity is often used by consumers instead of density. The reference for solids is normally the same as for liquids - water.

\section*{Examples}
>>> SG(860)
0. 8608461408159591
chemicals.utils.SG_to_API (SG)
Calculates API of a liquid given its specific gravity, as shown in [1].
\[
\text { API gravity }=\frac{141.5}{\mathrm{SG}}-131.5
\]

\section*{Parameters}

SG [float] Specific gravity of the fluid at 60 degrees Farenheight [-]

\section*{Returns}

API [float] API of the fluid [-]

\section*{Notes}

Defined only at 60 degrees Fahrenheit.

\section*{References}
[1]

\section*{Examples}
```

>>> SG_to_API(0.7365)

```
60.62491513917175

\section*{chemicals.utils.Vfs_to_zs(Vfs, Vms)}

Converts a list of mass fractions to mole fractions. Requires molecular weights for all species.
\[
z_{i}=\frac{\frac{\mathrm{Vf}_{i}}{V_{m, i}}}{\sum_{i} \frac{\mathrm{Vf}_{i}}{V_{m, i}}}
\]

\section*{Parameters}

Vfs [iterable] Molar volume fractions [-]
VMs [iterable] Molar volumes of species [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
zs [list] Mole fractions [-]

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.
Molar volumes are specified in terms of pure components only. Function works with any phase.

\section*{Examples}

Acetone and benzene example
>>> Vfs_to_zs([0.596, 0.404], [8.0234e-05, 9.543e-05])
[0.6369779395901142, 0.3630220604098858]
chemicals.utils.Vm_to_rho(Vm, MW)
Calculate the density of a chemical, given its molar volume and molecular weight.
\[
\rho=\frac{M W}{1000 \cdot V M}
\]

\section*{Parameters}

Vm [float] Molar volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
MW [float] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
rho [float] Density, [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]

\section*{References}
[1]

\section*{Examples}
>>> Vm_to_rho(0.000132, 86.18)
652.8787878787879
chemicals.utils.Watson_K \((T b, S G)\)
Calculates the Watson or UOP K Characterization factor of a liquid of a liquid given its specific gravity, and its average boiling point as shown in [1].
\[
K_{W}=\frac{T_{b}^{1 / 3}}{\mathrm{SG} \text { at } 60^{\circ} \mathrm{F}}
\]

\section*{Parameters}

SG [float] Specific gravity of the fluid at 60 degrees Farenheight [-]
Tb [float] Average normal boiling point, [K]

\section*{Returns}
\(\mathbf{K} \mathbf{W}\) [float] Watson characterization factor

\section*{Notes}

There are different ways to compute the average boiling point, so two different definitions are often used - K_UOP using volume average boiling point (VABP) using distillation points of \(10 \%, 30 \%, 50 \%, 70 \%\), and \(90 \%\); and K_Watson using mean average boiling point (MeABP).

\section*{References}
[1]

\section*{Examples}
```

>>> Watson_K(400, .8)

```
11.20351186639291

Sample problem in Comments on Procedure 2B5.1 of [1]; a fluids has a MEAB of 580 F and a SG of 34.5.
```

>>> from fluids.core import F2K
>>> Watson_K(F2K(580), API_to_SG(34.5))
11.884570347084471

```
chemicals.utils. \(\mathrm{Z}(T, P, V)\)

Calculates the compressibility factor of a gas, given its temperature, pressure, and molar volume.
\[
Z=\frac{P V}{R T}
\]

\section*{Parameters}

T [float] Temperature, [K]
\(\mathbf{P}\) [float] Pressure [Pa]
\(\mathbf{V}\) [float] Molar volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
\(\mathbf{Z}\) [float] Compressibility factor, [-]

\section*{References}
[1]

\section*{Examples}
>>> \(\mathrm{Z}(600, \mathrm{P}=1 \mathrm{E} 6, \mathrm{~V}=0.00463)\)
0. 9281016730797026
chemicals.utils.d2ns_to_dn2_partials(d2ns, \(d n s\) )

Convert second-order mole number derivatives of a quantity to the following second-order partial derivative:
\[
\frac{\partial^{2} n F}{\partial n_{j} \partial n_{i}}=\frac{\partial^{2} F}{\partial n_{i} \partial n_{j}}+\frac{\partial F}{\partial n_{i}}+\frac{\partial F}{\partial n_{j}}
\]

Requires the second order mole number derivatives and the first order mole number derivatives of the mixture only.

\section*{Parameters}
d2ns [list[float]] Second order derivatives of a quantity with respect to mole number (summing to 1 ), \(\left[\mathrm{prop} / \mathrm{mol}^{\wedge} 2\right]\)
dns [list[float]] Derivatives of a quantity with respect to mole number (summing to 1 ), [prop/mol]

\section*{Returns}
second_partial_properties [list[list[float]]] Derivatives of a quantity with respect to mole number (summing to 1 ), [prop]

\section*{See also:}
```

dxs_to_dns
dns_to_dn_partials
dxs_to_dn_partials

```

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.
This was originally implemented to allow for the calculation of first mole number derivatices of log fugacity coefficients; the two arguments are the second and first mole number derivatives of the overall mixture log fugacity coefficient.
Derived with the following SymPy code.
```

>>> from sympy import *
>>> n1, n2 = symbols('n1, n2')
>>> f, g, h = symbols('f, g, h', cls=Function)
>>> diff(h(n1, n2)*f(n1, n2), n1, n2)
f(n1, n2)*Derivative(h(n1, n2), n1, n2) + h(n1, n2)*Derivative(f(n1, n2), n1, n2) +
๑Derivative(f(n1, n2), n1)*Derivative(h(n1, n2), n2) + Derivative(f(n1, n2),ь
n2)*Derivative(h(n1, n2), n1)

```

\section*{Examples}
```

>> d2ns = [[0.152, 0.08, 0.547], [0.08, 0.674, 0.729], [0.547, 0.729, 0.131]]
>>> d2ns_to_dn2_partials(d2ns, [20.0, .124, 900.52])
[[40.152, 20.203999999999997, 921.067], [20.204, 0.922, 901.3729999999999], [921.
->067, 901.373, 1801.1709999999998]]

```
chemicals.utils.d2xs_to_d2xsn1 ( \(d 2 x s\) )
Convert the second mole fraction derivatives of a quantity (calculated so they do not sum to 1 ) to derivatives such that they do sum to 1 Requires the second derivatives of the mixture only. The size of the returned array is one less than the input in both dimensions
\[
\left(\frac{\partial^{2} F}{\partial x_{i} \partial x_{j}}\right)_{\sum_{x_{i}}^{N}=1}=\left(\frac{\partial^{2} F}{\partial x_{i} \partial x_{j}}-\frac{\partial^{2} F}{\partial x_{i} \partial x_{N}}-\frac{\partial^{2} F}{\partial x_{j} \partial x_{N}}+\frac{\partial^{2} F}{\partial x_{N} \partial x_{N}}\right)_{\sum_{x_{i}}^{N} \neq 1}
\]

\section*{Parameters}
second [list[float]] Second of a quantity with respect to mole fraction (not summing to 1), [prop]

\section*{Returns}
d2xsm1 [list[float]] Second derivatives of a quantity with respect to mole fraction (summing to 1 by altering the last component's composition), [prop]

\section*{Examples}
```

>>> d2xs_to_d2xsn1([[-2890.4327598108, -6687.0990540960065, -1549.375443699441], [-
\hookrightarrow6687.099054095983, -2811.2832904869883, -1228.6223853777503], [-1549.
\hookrightarrow3754436994498, -1228.6223853777562, -3667.388098758508]])
[[-3459.069971170426, -7576.489323777324], [-7576.489323777299, -4021.
๑4266184899957]]

```
chemicals.utils.d2xs_to_dxdn_partials( \(d 2 x s, x s)\)
Convert second-order mole fraction derivatives of a quantity (calculated so they do not sum to 1 ) to the following second-order partial derivative:
\[
\frac{\partial^{2} n F}{\partial x_{j} \partial n_{i}}=\frac{\partial^{2} F}{\partial x_{i} x_{j}}-\sum_{k} x_{k} \frac{\partial^{2} F}{\partial x_{k} \partial x_{j}}
\]

Requires the second derivatives and the mole fractions of the mixture only.

\section*{Parameters}
d2xs [list[float]
Second derivatives of a quantity with respect to mole fraction (not summing to 1 ), [prop]
xs [list[float]] Mole fractions of the species, [-]

\section*{Returns}
partial_properties [list[float]] Derivatives of a quantity with respect to mole number (summing to 1), [prop]

\section*{See also:}
```

dxs_to_dns
dns_to_dn_partials
dxs_to_dn_partials

```

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.

\section*{Examples}
```

>>> d2xs = [[0.152, 0.08, 0.547], [0.08, 0.674, 0.729], [0.547, 0.729, 0.131]]
>>> d2xs_to_dxdn_partials(d2xs, [0.7, 0.2, 0.1])
[[-0.02510000000000001, -0.183699999999999997, 0.005199999999999982], [-0.0971, 0.
441030000000000005, 0.18719999999999992], [0.3699, 0.4653, -0.41080000000000005]]

```
chemicals.utils.dns_to_dn_partials(dns, F, partial_properties=None)
Convert the mole number derivatives of a quantity (calculated so they do sum to 1 ) to partial molar quantites.
\[
\left(\frac{\partial n F}{\partial n_{i}}\right)_{n_{k \neq i}}=F_{i}+n\left(\frac{\partial F}{\partial n_{i}}\right)_{n_{k \neq i}}
\]

In the formula, the \(n\) is 1 .

\section*{Parameters}
dns [list[float]] Derivatives of a quantity with respect to mole number (summing to 1 ), [prop/mol]
F [float] Property evaluated at constant composition, [prop]
partial_properties [list[float], optional] Optional output array for derivatives of a quantity with respect to mole number (summing to 1 ), [prop]

\section*{Returns}
partial_properties [list[float]] Derivatives of a quantity with respect to mole number (summing to 1), [prop]

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.
This applies to a specific phase only, not to a mixture of multiple phases.
This is especially useful for fugacity calculations.

\section*{Examples}
```

>>> dns_to_dn_partials([0.001459, -0.002939, -0.004334], -0.0016567)
[-0.0001977000000000001, -0.0045957, -0.0059907]

```
chemicals.utils.dxs_to_dn_partials( \(d x s, x s, F\), partial_properties=None)
Convert the mole fraction derivatives of a quantity (calculated so they do not sum to 1) to partial molar quantites. Requires the derivatives and the mole fractions of the mixture.
\[
\left(\frac{\partial n F}{\partial n_{i}}\right)=\left(\frac{\partial F}{\partial x_{i}}\right)+F-\sum_{j} x_{j}\left(\frac{\partial F}{\partial x_{j}}\right)
\]

\section*{Parameters}
dxs [list[float]] Derivatives of a quantity with respect to mole fraction (not summing to 1 ), [prop]
xs [list[float]] Mole fractions of the species, [-]
F [float] Property evaluated at constant composition, [prop]
partial_properties [list[float], optional] Array for Derivatives of a quantity with respect to mole number (summing to 1 ), [prop]

\section*{Returns}
partial_properties [list[float]] Derivatives of a quantity with respect to mole number (summing to 1), [prop]

\section*{See also:}
```

dxs_to_dns
dns_to_dn_partials

```

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.
This applies to a specific phase only, not to a mixture of multiple phases.

\section*{Examples}
```

>>> dxs_to_dn_partials([-0.0026404, -0.00719, -0.00859], [0.7, 0.2, 0.1],
\#.- -0.0016567)
[-0.00015182, -0.0047014199999999996, -0.00610142]

```

\section*{chemicals.utils.dxs_to_dns( \(d x s, x s, d n s=N o n e)\)}

Convert the mole fraction derivatives of a quantity (calculated so they do not sum to 1) to mole number derivatives (where the mole fractions do sum to one). Requires the derivatives and the mole fractions of the mixture.
\[
\left(\frac{\partial M}{\partial n_{i}}\right)_{n_{k \neq i}}=\left[\left(\frac{\partial M}{\partial x_{i}}\right)_{x_{k \neq i}}-\sum_{j} x_{j}\left(\frac{\partial M}{\partial x_{j}}\right)_{x_{k \neq j}}\right]
\]

\section*{Parameters}
dxs [list[float]] Derivatives of a quantity with respect to mole fraction (not summing to 1 ), [prop]
xs [list[float]] Mole fractions of the species, [-]
dns [list[float], optional] Return array, [prop/mol]

\section*{Returns}
dns [list[float]] Derivatives of a quantity with respect to mole number (summing to 1 ), [prop/mol]

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.
This applies to a specific phase only, not to a mixture of multiple phases.

\section*{Examples}
>>> dxs_to_dns([-0.0028, -0.00719, -0.00859], [0.7, 0.2, 0.1])
[0.0014570000000000004, -0.002933, -0.004333]

\section*{chemicals.utils.dxs_to_dxsn1( \(d x s\) )}

Convert the mole fraction derivatives of a quantity (calculated so they do not sum to 1 ) to derivatives such that they do sum to 1 by changing the composition of the last component in the negative of the component which is changed. Requires the derivatives of the mixture only. The size of the returned array is one less than the input.
\[
\left(\frac{\partial F}{\partial x_{i}}\right)_{\sum_{x_{i}}^{N}=1}=\left(\frac{\partial F}{\partial x_{i}}-\frac{\partial F}{\partial x_{N}}\right)_{\sum_{x_{i}}^{N} \neq 1}
\]

\section*{Parameters}
dxs [list[float]] Derivatives of a quantity with respect to mole fraction (not summing to 1 ), [prop]

\section*{Returns}
dxsm1 [list[float]] Derivatives of a quantity with respect to mole fraction (summing to 1 by altering the last component's composition), [prop]

\section*{Examples}
```

>>> dxs_to_dxsn1([-2651.3181821109024, -2085.574403592012, -2295.0860830203587])

```
[-356.23209909054367, 209.51167942834672]
chemicals.utils.isentropic_exponent ( \(C p, C v\) )
Calculate the isentropic coefficient of an ideal gas, given its constant- pressure and constant-volume heat capacity.
\[
k=\frac{C_{p}}{C_{v}}
\]

\section*{Parameters}

Cp [float] Ideal gas heat capacity at constant pressure, [J/mol/K]
Cv [float] Ideal gas heat capacity at constant volume, [J/mol/K]

\section*{Returns}
k [float] Isentropic exponent, [-]

\section*{See also:}
isentropic_exponent_PV
isentropic_exponent_PT
isentropic_exponent_TV

\section*{Notes}

For real gases, there are more complexities and formulas. Each of the formulas reverts to this formula in the case of an ideal gas.

\section*{References}
[1]

\section*{Examples}
>>> isentropic_exponent(33.6, 25.27)
1.329639889196676

\section*{chemicals.utils.isentropic_exponent_PT ( \(C p, P, d V_{-} d T_{-} P\) )}

Calculate the isentropic coefficient of real fluid using the definition of \(P^{(1-k)} T^{k}=\) const.
\[
k=\frac{1}{1-\frac{P}{C_{p}}\left(\frac{\partial V}{\partial T}\right)_{P}}
\]

\section*{Parameters}

Cp [float] Real heat capacity at constant pressure, [J/mol/K]
\(\mathbf{P}\) [float] Pressure [Pa]
\(\mathbf{d V} \_\mathbf{d T}\) _P [float] Derivative of \(V\) with respect to \(T\) (at constant pressure), [m^3/(mol*K)]

\section*{Returns}
\(\mathbf{k}\) _PT [float] Isentropic exponent of a real fluid, [-]

\section*{See also:}
isentropic_exponent_PV
isentropic_exponent
isentropic_exponent_TV

\section*{References}
[1], [2]

\section*{Examples}

Isentropic exponent of air according to Lemmon (2000) at 1000 bar and 300 K :
```

>>> isentropic_exponent_PT(Cp=38.36583283578205, P=100000000.0, dV_dT_P=9.
407705210161724e-08)
1.32487270350443

```
chemicals.utils.isentropic_exponent_PV \(\left(C p, C v, V m, P, d P \_d V_{-} T\right)\)
Calculate the isentropic coefficient of real fluid using the definition of \(P V^{k}=\) const.
\[
k=-\frac{V}{P} \frac{C_{p}}{C_{v}}\left(\frac{\partial P}{\partial V}\right)_{T}
\]

\section*{Parameters}

Cp [float] Real heat capacity at constant pressure, [J/mol/K]
Cv [float] Real heat capacity at constant volume, [J/mol/K]
Vm [float] Molar volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
\(\mathbf{P}\) [float] Pressure [Pa]
\(\mathbf{d P}\) _dV_T [float] Derivative of \(P\) with respect to \(V\) (at constant temperature), \(\left[\mathrm{Pa} * \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right]\)

\section*{Returns}
\(\mathbf{k}\) _PV [float] Isentropic exponent of a real fluid, [-]
See also:
isentropic_exponent
isentropic_exponent_PT
isentropic_exponent_TV

\section*{References}
[1], [2]

\section*{Examples}

Isentropic exponent of air according to Lemmon (2000) at 1000 bar and 300 K :
```

>>> isentropic_exponent_PV(Cp=38.36583283578205, Cv=23.98081290153672, Vm=4.
๑730885141495376e-05, P=100000000.0, dP_dV_T=-5417785576072.434)
4.100576762582646

```
chemicals.utils.isentropic_exponent_TV ( \(\left.C v, V m, d P_{-} d T_{-} V\right)\)
Calculate the isentropic coefficient of real fluid using the definition of \(T V^{k-1}=\) const.
\[
k=1+\frac{V}{C_{v}}\left(\frac{\partial P}{\partial T}\right)_{V}
\]

\section*{Parameters}

Cv [float] Real heat capacity at constant volume, [J/mol/K]
Vm [float] Molar volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
\(\mathbf{d P}\) _dT_V [float] Derivative of \(P\) with respect to \(T\) (at constant volume), \([\mathrm{Pa} / \mathrm{K}]\)

\section*{Returns}
k_TV [float] Isentropic exponent of a real fluid, [-]
See also:
```

isentropic_exponent_PV
isentropic_exponent_PT
isentropic_exponent

```

\section*{References}
[1], [2]

\section*{Examples}

Isentropic exponent of air according to Lemmon (2000) at 1000 bar and 300 K :
```

>>> isentropic_exponent_TV(Cv=23.98081290153672, Vm=4.730885141495376e-05, dP_dT_
V=509689.2959155567)
2.005504495083

```

\section*{chemicals.utils.isobaric_expansion \(\left(V, d V \_d T\right)\)}

Calculate the isobaric coefficient of a thermal expansion, given its molar volume at a certain \(T\) and \(P\), and its derivative of molar volume with respect to \(T\).
\[
\beta=\frac{1}{V}\left(\frac{\partial V}{\partial T}\right)_{P}
\]

\section*{Parameters}
\(\mathbf{V}\) [float] Molar volume at \(T\) and \(P,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol}\right]\)
\(\mathbf{d V}\) _dT [float] Derivative of molar volume with respect to \(T,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)

\section*{Returns}
beta [float] Isobaric coefficient of a thermal expansion, [1/K]

\section*{Notes}

For an ideal gas, this expression simplified to:
\[
\beta=\frac{1}{T}
\]

\section*{References}
[1]

Examples
Calculated for hexane from the PR EOS at 299 K and 1 MPa (liquid):
```

>>> isobaric_expansion(0.000130229900873546, 1.58875261849113e-7)
0.0012199599384121608

```
chemicals.utils.isothermal_compressibility \(\left(V, d V \_d P\right)\)
Calculate the isothermal coefficient of compressibility, given its molar volume at a certain \(T\) and \(P\), and its derivative of molar volume with respect to \(P\).
\[
\kappa=-\frac{1}{V}\left(\frac{\partial V}{\partial P}\right)_{T}
\]

\section*{Parameters}

V [float] Molar volume at \(T\) and \(P,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol}\right]\)
\(\mathbf{d V}\) _dP [float] Derivative of molar volume with respect to \(P,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol} / \mathrm{Pa}\right]\)

\section*{Returns}
kappa [float] Isothermal coefficient of compressibility, [1/Pa]

\section*{Notes}

For an ideal gas, this expression simplified to:
\[
\kappa=\frac{1}{P}
\]

The isothermal bulk modulus is the inverse of this quantity:
\[
K=-V\left(\frac{\partial P}{\partial V}\right)_{T}
\]

The ideal gas isothermal bulk modulus is simply the gas's pressure.

\section*{References}
[1]

\section*{Examples}

Calculated for hexane from the PR EOS at 299 K and 1 MPa (liquid):
```

>>> isothermal_compressibility(0.000130229900873546, -2.72902118209903e-13)
2.095541165119158e-09

```

Calculate the bulk modulus of propane from the PR EOS at 294 K as a gas:
```

>>> 1/isothermal_compressibility(0.0024576770482135617, -3.5943321700795866e-09)

```
683764.5859979445
chemicals.utils.mix_component_flows(IDs1, IDs2, flow1, flow2, fractions1, fractions2)
Mix two flows of potentially different chemicals of given overall flow rates and flow fractions to determine the outlet components, flow rates, and compositions. The flows do not need to be of the same length.

\section*{Parameters}

IDs1 [list[str]] List of identifiers of the chemical species in flow one, [-]
IDs2 [list[str]] List of identifiers of the chemical species in flow two, [-]
flow1 [float] Total flow rate of the chemicals in flow one, \([\mathrm{mol} / \mathrm{s}\) ]
flow2 [float] Total flow rate of the chemicals in flow two, [ \(\mathrm{mol} / \mathrm{s}\) ]
fractions1 [list[float]] Mole fractions of each chemical in flow one, [-]
fractions2 [list[float]] Mole fractions of each chemical in flow two, [-]

\section*{Returns}
cmps [list[str]] List of identifiers of the chemical species in the combined flow, [-]
moles [list[float]] Flow rates of all chemical species in the combined flow, [ \(\mathrm{mol} / \mathrm{s}\) ]

\section*{Notes}

Mass or volume flows and fractions can be used instead of molar ones.
If the two flows have the same components, the output list will be in the same order as the one given; otherwise they are sorted alphabetically.

\section*{Examples}
```

>>> mix_component_flows(['7732-18-5', '64-17-5'], ['7732-18-5', '67-56-1'], 1, 1,,七
[0.5, 0.5], [0.5, 0.5])
(['64-17-5', '67-56-1', '7732-18-5'], [0.5, 0.5, 1.0])

```
chemicals.utils.mix_component_partial_flows(IDs1,IDs2,ns1=None, ns \(2=\) None)

Mix two flows of potentially different chemicals; with the feature that the mole flows of either or both streams may be unknown.

The flows do not need to be of the same length.

\section*{Parameters}

IDs1 [list[str]] List of identifiers of the chemical species in flow one, [-]
IDs2 [list[str]] List of identifiers of the chemical species in flow two, [-]
ns1 [list[float]] Total flow rate of the chemicals in flow one, \([\mathrm{mol} / \mathrm{s}\) ]
ns2 [list[float]] Total flow rate of the chemicals in flow two, [ \(\mathrm{mol} / \mathrm{s}\) ]

\section*{Returns}
cmps [list[str]] List of identifiers of the chemical species in the combined flow, [-]
moles [list[float]] Flow rates of all chemical species in the combined flow, [ \(\mathrm{mol} / \mathrm{s}\) ]

\section*{Notes}

Mass or volume flows and fractions can be used instead of molar ones.
If the two flows have the same components, the output list will be in the same order as the one given; otherwise they are sorted alphabetically.

\section*{Examples}
```

>>> mix_component_partial_flows(['7732-18-5', '64-17-5'], ['7732-18-5', '67-56-1'],,
\hookrightarrow[0.5, 0.5], [0.5, 0.5])
(['64-17-5', '67-56-1', '7732-18-5'], [0.5, 0.5, 1.0])
>>> mix_component_partial_flows(['7732-18-5', '64-17-5'], ['7732-18-5', '67-56-1'],七
CNone, [0.5, 0.5])
(['64-17-5', '67-56-1', '7732-18-5'], [0.0, 0.5, 0.5])
>>> mix_component_partial_flows(['7732-18-5', '64-17-5'], ['7732-18-5', '67-56-1'],, ь
\rightarrow [ 0 . 5 , ~ 0 . 5 ] , ~ N o n e )
(['64-17-5', '67-56-1', '7732-18-5'], [0.5, 0.0, 0.5])
>>> mix_component_partial_flows(['7732-18-5', '64-17-5'], ['7732-18-5', '67-56-1'],,
\rightarrow None, None)
(['64-17-5', '67-56-1', '7732-18-5'], [0.0, 0.0, 0.0])

```
chemicals.utils.mix_multiple_component_flows(IDs, flows, fractions)
Mix multiple flows of potentially different chemicals of given overall flow rates and flow fractions to determine the outlet components, flow rates, and compositions. The flows do not need to be of the same length.

\section*{Parameters}

IDs [list[list[[str]]] List of lists of identifiers of the chemical species in the flows, [-]
flows [list[float]] List of total flow rates of the chemicals in the streams, [ \(\mathrm{mol} / \mathrm{s}\) ]
fractions [list[list[float]]] List of lists of mole fractions of each chemical in each flow, [-]

\section*{Returns}
cmps [list[strr]] List of identifiers of the chemical species in the combined flow, [-]
moles [list[float]] Flow rates of all chemical species in the combined flow, [mol/s]

\section*{Notes}

Mass or volume flows and fractions can be used instead of molar ones.
If the every flow have the same components, the output list will be in the same order as the one given; otherwise they are sorted alphabetically.

\section*{Examples}
```

>>> mix_multiple_component_flows([['7732-18-5', '64-17-5'], ['7732-18-5', '67-56-1
↔']],
... [1, 1], [[0.5, 0.5], [0.5, 0.5]])
(['64-17-5', '67-56-1', '7732-18-5'], [0.5, 0.5, 1.0])

```

\section*{chemicals.utils.mixing_logarithmic (fracs, props)}

Simple function calculates a property based on weighted averages of logarithmic properties.
\[
y=\sum_{i} \operatorname{frac}_{i} \cdot \ln \left(\text { prop}_{i}\right)
\]

\section*{Parameters}
fracs [array-like] Fractions of a mixture
props: array-like Properties

\section*{Returns}
prop [value] Calculated property

\section*{Notes}

Does not work on negative values. Returns None if any fractions or properties are missing or are not of the same length.

\section*{Examples}
>>> mixing_logarithmic([0.1, 0.9], [0.01, 0.02])
0.01866065983073615
chemicals.utils.mixing_power (fracs, props, \(r\) )
Power law mixing rule for any property, with a variable exponent \(r\) as input. Optimiezd routines are available for \(r=-4,-3,-2,-1,1,2,3,4\).
\[
\operatorname{prop}_{m i x}^{r}=\sum_{i} z_{i}\left(\operatorname{prop}_{i}\right)^{r}
\]

\section*{Parameters}
fracs [list[float]] Mole fractions of components (or mass, or volume, etc.), [-]
props [list[float]] Properties of all components, [various]
r [float] Power mixing exponent, [-]

\section*{Returns}
prop [float] Property for mixture, [props]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel.
The following recommendations in [1] exist for different properties:
Surface tension: \(r=1\) Recommended by an author in [1]; but often non-linear behavior is shown and \(r=-1\) to \(r=-3\) is recommended. \(r=-1\) is most often used.

Liquid thermal conductivity: \(\mathrm{r}=-2\) in [1]; this is known also as procedure DIPPR9B.

\section*{References}
[1]

\section*{Examples}
>>> mixing_power([0.258, 0.742], [0.1692, 0.1528], -2)
0.15657104706719646
chemicals.utils.mixing_simple(fracs, props)
Simple function calculates a property based on weighted averages of properties. Weights could be mole fractions, volume fractions, mass fractions, or anything else.
\[
y=\sum_{i} \operatorname{frac}_{i} \cdot \operatorname{prop}_{i}
\]

\section*{Parameters}
fracs [array-like] Fractions of a mixture
props: array-like Properties

\section*{Returns}
prop [value] Calculated property

\section*{Notes}

Returns None if there is an error, normally if one of the properties is missing or if they are not the same length as the fractions.

\section*{Examples}
>>> mixing_simple([0.1, 0.9], [0.01, 0.02])
0.019000000000000003
chemicals.utils.molar_velocity_to_velocity (v_molar, MW)
Calculate the mass-based velocity ( \(\mathrm{m} / \mathrm{s}\) ) from the molar velocity of the fluid.
\[
v=\frac{v_{\text {molar }} \sqrt{1000}}{\sqrt{\mathrm{MW}}}
\]

\section*{Parameters}
v_molar [float] Molar velcoity, \(\left[\mathrm{m} * \mathrm{~kg}^{\wedge} 0.5 / \mathrm{s} / \mathrm{mol}^{\wedge} 0.5\right.\) ]
MW [float] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
\(\mathbf{v}\) [float] Velocity, [m/s]

\section*{Examples}
>>> molar_velocity_to_velocity(46., 40.445)
228.73
chemicals.utils.none_and_length_check(all_inputs, length=None)
Checks inputs for suitability of use by a mixing rule which requires all inputs to be of the same length and non-None. A number of variations were attempted for this function; this was found to be the quickest.

\section*{Parameters}
all_inputs [array-like of array-like] list of all the lists of inputs, [-]
length [int, optional] Length of the desired inputs, [-]

\section*{Returns}

False/True [bool] Returns True only if all inputs are the same length (or length length) and none of the inputs contain None [-]

\section*{Notes}

Does not check for nan values.

\section*{Examples}
>>> none_and_length_check(([1, 1], [1, 1], [1, 30], [10,0]), length=2)
True
chemicals.utils.normalize(values)
Simple function which normalizes a series of values to be from 0 to 1 , and for their sum to add to 1 .
\[
x=\frac{x}{\operatorname{sum}_{i} x_{i}}
\]

\section*{Parameters}
values [array-like] array of values

\section*{Returns}
fractions [array-like] Array of values from 0 to 1

\section*{Notes}

Does not work on negative values, or handle the case where the sum is zero.

\section*{Examples}
>>> normalize([3, 2, 1])
[0.5, 0.3333333333333333, 0.16666666666666666]
chemicals.utils.phase_identification_parameter \(\left(V, d P \_d T, d P \_d V, d 2 P \_d V 2, d 2 P \_d V d T\right)\)
Calculate the Phase Identification Parameter developed in [1] for the accurate and efficient determination of whether a fluid is a liquid or a gas based on the results of an equation of state. For supercritical conditions, this provides a good method for choosing which property correlations to use.
\[
\Pi=V\left[\frac{\frac{\partial^{2} P}{\partial V \partial T}}{\frac{\partial P}{\partial T}}-\frac{\frac{\partial^{2} P}{\partial V^{2}}}{\frac{\partial P}{\partial V}}\right]
\]

\section*{Parameters}

V [float] Molar volume at \(T\) and \(P,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol}\right]\)
\(\mathbf{d P}\) _dT [float] Derivative of \(P\) with respect to \(T,[\mathrm{~Pa} / \mathrm{K}]\)
\(\mathbf{d P}\) _dV [float] Derivative of \(P\) with respect to \(V,\left[\mathrm{~Pa} * \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right]\)
\(\mathbf{d 2 P}\) _dV2 [float] Second derivative of \(P\) with respect to \(V,\left[\mathrm{~Pa}^{*} \mathrm{~mol}^{\wedge} 2 / \mathrm{m}^{\wedge} 6\right]\)
d2P_dVdT [float] Second derivative of \(P\) with respect to both \(V\) and \(T,\left[\mathrm{~Pa}^{*} \mathrm{~mol} / \mathrm{m}^{\wedge} 3 / \mathrm{K}\right]\)

\section*{Returns}

PIP [float] Phase Identification Parameter, [-]

\section*{Notes}

Heuristics were used by process simulators before the invent of this parameter.
The criteria for liquid is \(\mathrm{Pi}>1\); for vapor, \(\mathrm{Pi}<=1\).
There is also a solid phase mechanism available. For solids, the Solid Phase Identification Parameter is greater than 1 , like liquids; however, unlike liquids, \(\mathrm{d} 2 \mathrm{P}_{\_} \mathrm{dVdT}\) is always \(>0\); it is \(<0\) for liquids and gases.

\section*{References}
[1], [2]

\section*{Examples}

Calculated for hexane from the PR EOS at 299 K and 1 MPa (liquid):
```

>>> phase_identification_parameter(0.000130229900874, 582169.397484,
... -3.66431747236e+12, 4.48067893805e+17, -20518995218.2)
11.33428990564796

```
chemicals.utils.phase_identification_parameter_phase \(\left(d 2 P \_d V d T, V=N o n e, d P \_d T=N o n e\right.\), \(d P \_d V=\) None,\(d 2 P \_d V 2=\) None \()\)
Uses the Phase Identification Parameter concept developed in [1] and [2] to determine if a chemical is a solid, liquid, or vapor given the appropriate thermodynamic conditions.

The criteria for liquid is PIP \(>1\); for vapor, \(\mathrm{PIP}<=1\).

For solids, PIP(solid) is defined to be d2P_dVdT. If it is larger than 0 , the species is a solid. It is less than 0 for all liquids and gases.

\section*{Parameters}
d2P_dVdT [float] Second derivative of \(P\) with respect to both \(V\) and \(T,\left[\mathrm{~Pa}^{*} \mathrm{~mol} / \mathrm{m}^{\wedge} 3 / \mathrm{K}\right]\)
V [float, optional] Molar volume at \(T\) and \(P,\left[\mathrm{~m}^{\wedge} 3 / \mathrm{mol}\right]\)
dP_dT [float, optional] Derivative of \(P\) with respect to \(T,[\mathrm{~Pa} / \mathrm{K}]\)
\(\mathbf{d P}\) _dV [float, optional] Derivative of \(P\) with respect to \(V,\left[\mathrm{~Pa}^{*} \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right]\)
\(\mathbf{d 2 P}\) _dV2 [float, optionsl] Second derivative of \(P\) with respect to \(V,\left[\mathrm{~Pa}^{*} \mathrm{~mol}^{\wedge} 2 / \mathrm{m}^{\wedge} 6\right]\)

\section*{Returns}
phase [str] Either 's', 'l' or 'g'

\section*{Notes}

The criteria for being a solid phase is checked first, which only requires d2P_dVdT. All other inputs are optional for this reason. However, an exception will be raised if the other inputs become needed to determine if a species is a liquid or a gas.

\section*{References}
[1], [2]

\section*{Examples}

Calculated for hexane from the PR EOS at 299 K and 1 MPa (liquid):
```

>>> phase_identification_parameter_phase(-20518995218.2, 0.000130229900874,
.. 582169.397484, -3.66431747236e+12, 4.48067893805e+17)
'l'

```
chemicals.utils.property_mass_to_molar(A_mass, \(M W\) )
Convert a quantity in mass units [thing/kg] to molar units [thing/mol]. The standard gram-mole is used here, as it is everwhere in this library.
\[
A_{\mathrm{molar}}=\frac{A_{\mathrm{mass}} \mathrm{MW}}{1000}
\]

\section*{Parameters}

A_mass [float] Quantity in molar units [thing/kg]
MW [float] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}

A_molar [float] Quantity in molar units [thing/mol]

\section*{Notes}

For legacy reasons, if the value \(A \_m a s s\) is None, None is also returned and no exception is returned.

\section*{Examples}
>>> property_mass_to_molar(20.0, 18.015)
0.3603

\section*{chemicals.utils.property_molar_to_mass(A_molar, \(M W\) )}

Convert a quantity in molar units [thing/mol] to mass units [thing \(/ \mathrm{kg}\) ]. The standard gram-mole is used here, as it is everwhere in this library.
\[
A_{\mathrm{mass}}=\frac{1000 A_{\mathrm{molar}}}{\mathrm{MW}}
\]

\section*{Parameters}

A_molar [float] Quantity in molar units [thing/mol]
MW [float] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}

A_mass [float] Quantity in molar units [thing/kg]

\section*{Notes}

For legacy reasons, if the value \(A_{-}\)molar is None, None is also returned and no exception is returned.

\section*{Examples}
>>> property_molar_to_mass(500, 18.015)
27754.648903691366

\section*{chemicals.utils.radius_of_gyration( \(M W, A, B, C\), planar=False)}

Calculates the radius of gyration of a molecule using the DIPPR definition. The parameters \(A, B\), and \(C\) must be obtained from either vibrational scpectra and analysis or quantum chemistry calculations of programs such as psi <https://psicode.org/>.
For planar molecules defined by only two moments of inertia,
\[
R_{g}=\sqrt{\sqrt{A B} \frac{N_{A}}{\mathrm{MW}}}
\]

For non-planar molecules with three moments of inertia,
\[
R_{g}=\sqrt{\frac{2 \pi(A B C)^{1 / 3} N_{A}}{\mathrm{MW}}}
\]

\section*{Parameters}

MW [float] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]
A [float] First principle moment of inertia, \(\left[\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2\right]\)
B [float] Second principle moment of inertia, [kg*m^2]

C [float] Third principle moment of inertia, [kg*m^2]
planar [bool] Whether the molecule is flat or not, [-]

\section*{Returns}
\(\mathbf{R g}\) [float] Radius of gyration, [m]

\section*{Notes}

There are many, many quantum chemistry models available which give different results.

\section*{References}
[1], [2]

\section*{Examples}

Example calcultion in [1] for hydrazine (optimized with HF/6-31G model):
```

>>> radius_of_gyration(MW=32.00452, planar=False, A=5.692E-47, B=3.367E-46, C=3.
๑681E-46)
1.50581642e-10

```

The same calculation was performed with \(p s i\) and somewhat different parameters obtained
```

>>> radius_of_gyration(MW=32.00452, planar=False, A=6.345205205562681e-47, B=3.
๑2663291891213418e-46, C=3.4321304373822523e-46)
1.507895671e-10

```

A planar molecule, bromosilane, has two principle moments of inertia in [2]. They are \(2.80700 \mathrm{~cm}^{\wedge}-1\) and \(0.14416 \mathrm{~cm}^{\wedge}-1\). These can be converted to MHz as follows:
These can then be converted to units of AMU*Angstrom^2, and from there to \(\mathrm{kg}^{*} \mathrm{~m}^{\wedge} 2\).
```

>>> A, B = 2.80700, 0.14416
>>> from scipy.constants import atomic_mass, c, angstrom
>> A, B = A*C*1e-4, B*C*1e-4 \# from cm^-1 to MHz
>> A, B = [505379.15/i for i in (A, B)] \# TODO which constants did this
Conversion factor come from, AMU*Angstrom^2
>> A, B = [i*atomic_mass*angstrom**2 for i in (A, B)] \# amu*angstrom^2 to kg*m^2
>>> radius_of_gyration(A=A, B=B, planar=True, MW=111.01, C=0)
4.8859099776e-11

```

Alternatively, doing the conversion all in one:
```

>>> A, B = 2.80700, 0.14416
>> from scipy.constants import c, h, pi
>> A, B = A*C*100, B*C*100 \# from cm^-1 to Hz
>> A, B = [h/(8*pi**2)/i for i in (A, B)] \# from Hz to kg*m^2
>>> radius_of_gyration(A=A, B=B, planar=True, MW=111.01, C=0)
4.885909296e-11

```

This is also nicely documented on this page: https://cccbdb.nist.gov/convertmomint.asp which was unfortunately found by the author after figuring it out the hard way.
chemicals.utils.remove_zeros (values, tol=1e-06)
Simple function which removes zero values from an array, and replaces them with a user-specified value, normally a very small number. Helpful for the case where a function can work with values very close to zero but not quite zero. The resulting array is normalized so the sum is still one.

\section*{Parameters}
values [array-like] array of values
tol [float] The replacement value for zeroes

\section*{Returns}
fractions [array-like] Array of values from 0 to 1

\section*{Notes}

Works on numpy arrays, and returns numpy arrays only for that case.

\section*{Examples}
```

>>> remove_zeros([0, 1e-9, 1], 1e-12)

```
```

[9.99999998999e-13, 9.99999998999e-10, 0.999999998999]

```
chemicals.utils.rho_to_API(rho, rho_ref=999.0170824078306)
Calculates API of a liquid given its mass density, as shown in [1].
\[
\text { API gravity }=\frac{141.5 \rho_{r e f}}{\rho}-131.5
\]

\section*{Parameters}
rho [float] Mass density the fluid at 60 degrees Farenheight \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.\) ]
rho_ref [float, optional] Density of the reference substance, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Returns}

API [float] API of the fluid [-]

\section*{Notes}

Defined only at 60 degrees Fahrenheit.

\section*{References}
[1]

\section*{Examples}
>>> rho_to_API(820)
40.8913623
>>> SG_to_API(SG(820))
40.8913623
chemicals.utils.rho_to_Vm(rho, \(M W\) )
Calculate the molar volume of a chemical, given its density and molecular weight.
\[
V_{m}=\left(\frac{1000 \rho}{M W}\right)^{-1}
\]

\section*{Parameters}
rho [float] Density, [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
MW [float] Molecular weight, \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}

Vm [float] Molar volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{References}
[1]

\section*{Examples}
>>> rho_to_Vm(652.9, 86.18)
0.0001319957114412621
chemicals.utils.solve_flow_composition_mix (Fs,zs, ws, MWs)
Solve a stream composition problem where some specs are mole flow rates; some are mass fractions; and some are mole fractions. This algorithm requires at least one mole flow rate; and for every other component, a single spec in mole or mass or a flow rate. It is permissible for no components to have mole fractions; or no components to have weight fractions; or both.

\section*{Parameters}

Fs [list[float]] List of mole flow rates; None if not specified for a component, [ \(\mathrm{mol} / \mathrm{s}\) ]
zs [list[float]] Mole fractions; None if not specified for a component [-]
ws [list[float]] Mass fractions; None if not specified for a component [-]
MWs [list[float]] Molecular weights, \([\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}

Fs [list[float]] List of mole flow rates, [ \(\mathrm{mol} / \mathrm{s}\) ]
zs [list[float]] Mole fractions, [-]
ws [list[float]] Mass fractions, [-]

\section*{Notes}

A fast path is used if no weight fractions are provided; the calculation is much simpler for that case.
This algorithm was derived using SymPy, and framed in a form which allows for explicit solving. This is capable of solving large-scale problems i.e. with 1000 components a solve time is 1 ms ; with 10000 it is 10 ms .

\section*{Examples}
```

>>> Fs = [3600, None, None, None, None]
>>> zs = [None, .1, .2, None, None]
>>> ws = [None, None, None, .01, .02]
>>> MWs = [18.01528, 46.06844, 32.04186, 72.151, 142.286]
>>> Fs, zs, ws = solve_flow_composition_mix(Fs, zs, ws, MWs)
>> Fs
[3600, 519.3039148597746, 1038.6078297195493, 17.44015034881175, 17.687253669610733]
>>> zs
[0.6932356751002141, 0.1, 0.2, 0.0033583706669188186, 0.003405954232867038]
>>> ws
[0.5154077420893426, 0.19012206531421305, 0.26447019259644433, 0.01, 0.02]

```
chemicals.utils.speed_of_sound ( \(\left.V, d P \_d V, C p, C v, M W=N o n e\right)\)
Calculate a real fluid's speed of sound. The required derivatives should be calculated with an equation of state, and \(C p\) and \(C v\) are both the real fluid versions. Expression is given in [1] and [2]; a unit conversion is further performed to obtain a result in \(\mathrm{m} / \mathrm{s}\). If MW is not provided the result is returned in units of \(\mathrm{m}^{*} \mathrm{~kg}^{\wedge} 0.5 / \mathrm{s} / \mathrm{mol}^{\wedge} 0.5\).
\[
w=\left[-V^{2}\left(\frac{\partial P}{\partial V}\right)_{T} \frac{C_{p}}{C_{v}}\right]^{1 / 2}
\]

\section*{Parameters}
\(\mathbf{V}\) [float] Molar volume of fluid, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
\(\mathbf{d P}\) _dV [float] Derivative of \(P\) with respect to \(V\), \(\left[\mathrm{Pa} * \mathrm{~mol} / \mathrm{m}^{\wedge} 3\right]\)
Cp [float] Real fluid heat capacity at constant pressure, [J/mol/K]
Cv [float] Real fluid heat capacity at constant volume, [J/mol/K]
MW [float, optional] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
\(\mathbf{w}\) [float] Speed of sound for a real gas, \(\mathrm{m} / \mathrm{s}\) or \(\mathrm{m}^{*} \mathrm{~kg}^{\wedge} 0.5 / \mathrm{s} / \mathrm{mol}^{\wedge} 0.5\) if MW missing

\section*{Notes}

An alternate expression based on molar density is as follows:
\[
w=\left[\left(\frac{\partial P}{\partial \rho}\right)_{T} \frac{C_{p}}{C_{v}}\right]^{1 / 2}
\]

The form with the unit conversion performed inside it is as follows:
\[
w=\left[-V^{2} \frac{1000}{M W}\left(\frac{\partial P}{\partial V}\right)_{T} \frac{C_{p}}{C_{v}}\right]^{1 / 2}
\]

\section*{References}
[1], [2]

\section*{Examples}

Example from [2]:
```

>>> speed_of_sound(V=0.00229754, dP_dV=-3.5459e+08, Cp=153.235, Cv=132.435, MW=67.
๑152)
179.5868138460819

```
chemicals.utils.to_num (values)
Legacy function to turn a list of strings into either floats (if numeric), stripped strings (if not) or None if the string is empty. Accepts any numeric formatting the float function does.

\section*{Parameters}
values [list] list of strings

\section*{Returns}
values [list] list of floats, strings, and None values [-]

\section*{Examples}
```

>>> to_num(['1', '1.1', '1E5', '0xB4', ''])

```
[1.0, 1.1, \(100000.0, ~ ' 0 x B 4 '\) ', None]
chemicals.utils.v_molar_to_v(v_molar, \(M W\) )
Convert a velocity from units of the molar velocity form to standard \(\mathrm{m} / \mathrm{s}\) units.
\[
v(\mathrm{~m} / \mathrm{s})=v\left(\frac{\mathrm{~m} \sqrt{\mathrm{~kg}}}{s \sqrt{\mathrm{~mol}}}\right) \mathrm{MW}(\mathrm{~g} / \mathrm{mol})^{-0.5} \cdot\left(\frac{1000 \mathrm{~g}}{1 \mathrm{~kg}}\right)^{0.5}
\]

\section*{Parameters}
v_molar [float] Molar velocity, [ \(\mathrm{m}^{*} \mathrm{~kg}^{\wedge} 0.5 / \mathrm{s} / \mathrm{mol}^{\wedge} 0.5\) ]
MW [float] Molecular weight, [g/mol]

\section*{Returns}
\(\mathbf{v}\) [float] Velocity, [m/s]

\section*{Examples}
>>> v_molar_to_v(67.10998435404377, 18.015)
499.99999999999994
chemicals.utils.v_to_v_molar \((v, M W)\)
Convert a velocity from units of \(\mathrm{m} / \mathrm{s}\) to a "molar" form of velocity, compatible with thermodynamic calculations on a molar basis.
\[
v\left(\frac{\mathrm{~m} \sqrt{\mathrm{~kg}}}{s \sqrt{\mathrm{~mol}}}\right)=v(\mathrm{~m} / \mathrm{s}) \sqrt{\mathrm{MW}(\mathrm{~g} / \mathrm{mol})} \cdot\left(\frac{1000 \mathrm{~g}}{1 \mathrm{~kg}}\right)^{-0.5}
\]

\section*{Parameters}
\(\mathbf{v}\) [float] Velocity, [m/s]
MW [float] Molecular weight, \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}
v_molar [float] Molar velocity, \(\left[\mathrm{m} * \mathrm{~kg}^{\wedge} 0.5 / \mathrm{s} / \mathrm{mol}^{\wedge} 0.5\right.\) ]

\section*{Examples}
>>> v_to_v_molar(500, 18.015)
67.10998435404377
chemicals.utils.vapor_mass_quality ( \(V F, M W l, M W g\) )
Calculates the vapor quality on a mass basis of a two-phase mixture; this is the most common definition, where 1 means a pure vapor and 0 means a pure liquid. The vapor quality on a mass basis is related to the mole basis vapor fraction according to the following relationship:
\[
x=\frac{\frac{V}{F} \cdot \mathrm{MW}_{g}}{\left(1-\frac{V}{F}\right) \mathrm{MW}_{l}+\frac{V}{F} \mathrm{MW}_{g}}
\]

\section*{Parameters}

VF [float] Mole-basis vapor fraction ( \(0=\) pure vapor, \(1=\) pure liquid), [-]
MWI [float] Average molecular weight of the liquid phase, \([\mathrm{g} / \mathrm{mol}\) ]
\(\mathbf{M W g}\) [float] Average molecular weight of the vapor phase, \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}
quality [float] Vapor mass fraction of the two-phase system, [-]

\section*{Notes}

Other definitions of vapor fraction use an enthalpy basis instead of a mass basis; still other less common ones take 1 to be the value of the liquid, and 0 as pure vapor.

\section*{References}
[1]

\section*{Examples}
```

>>> vapor_mass_quality(0.5, 60, 30)
0.3333333333333333

```
chemicals.utils.velocity_to_molar_velocity ( \(v, M W\) )
Calculate the molar velocity from the mass-based ( \(\mathrm{m} / \mathrm{s}\) ) velocity of the fluid.
\[
v_{\text {molar }}=\frac{v \sqrt{\mathrm{MW}}}{\sqrt{1000}}
\]

\section*{Parameters}
\(\mathbf{v}\) [float] Velocity, [m/s]
MW [float] Molecular weight, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
v_molar [float] Molar velcoity, \(\left[\mathrm{m}^{*} \mathrm{~kg}^{\wedge} 0.5 / \mathrm{s} / \mathrm{mol}^{\wedge} 0.5\right]\)

\section*{Examples}
>>> velocity_to_molar_velocity(228.73, 40.445)
46.
chemicals.utils.ws_to_zs ( \(w s, M W s\) )
Converts a list of mass fractions to mole fractions. Requires molecular weights for all species.
\[
z_{i}=\frac{\frac{w_{i}}{M W_{i}}}{\sum_{i} \frac{w_{i}}{M W_{i}}}
\]

\section*{Parameters}
ws [iterable] Mass fractions [-]
MWs [iterable] Molecular weights [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
zs [iterable] Mole fractions [-]

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.

Examples
>>> ws_to_zs([0.3333333333333333, 0.6666666666666666], [10, 20])
[0.5, 0.5]
chemicals.utils.zs_to_Vfs (zs,Vms)
Converts a list of mole fractions to volume fractions. Requires molar volumes for all species.
\[
\mathrm{Vf}_{i}=\frac{z_{i} V_{m, i}}{\sum_{i} z_{i} V_{m, i}}
\]

\section*{Parameters}
zs [iterable] Mole fractions [-]
VMs [iterable] Molar volumes of species [m^3/mol]

\section*{Returns}

Vfs [list] Molar volume fractions [-]

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.
Molar volumes are specified in terms of pure components only. Function works with any phase.

\section*{Examples}

Acetone and benzene example
>>> zs_to_Vfs([0.637, 0.363], [8.0234e-05, 9.543e-05])
[0.5960229712956298, 0.4039770287043703]
chemicals.utils.zs_to_ws \((z s, M W s)\)
Converts a list of mole fractions to mass fractions. Requires molecular weights for all species.
\[
\begin{array}{r}
w_{i}=\frac{z_{i} M W_{i}}{M W_{a v g}} \\
M W_{a v g}=\sum_{i} z_{i} M W_{i}
\end{array}
\]

\section*{Parameters}
zs [iterable] Mole fractions [-]
MWs [iterable] Molecular weights [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
ws [iterable] Mass fractions [-]

\section*{Notes}

Does not check that the sums add to one. Does not check that inputs are of the same length.

\section*{Examples}
```

>>> zs_to_ws([0.5, 0.5], [10, 20])
[0.3333333333333333, 0.6666666666666666]

```

\subsection*{1.31 Support for pint Quantities (chemicals.units)}

Basic module which wraps all chemicals functions and classes to be compatible with the pint unit handling library. All other object - dicts, lists, etc - are not wrapped.
```

>>> import chemicals
>>> chemicals.units.Antoine
<function Antoine at 0x...>

```

The chemicals.units module also supports star imports; the same objects exported when importing from the main library will be imported from chemicals.units.
```

>>> from chemicals.units import *
>>> CAS = CAS_from_any('methanol')
>>> Tc(CAS), Pc(CAS), Vc(CAS), Zc(CAS)
(<Quantity(513.38, 'kelvin')>, <Quantity(8215850.0, 'pascal')>, <Quantity(0.00011382819,
\hookrightarrow'meter ** 3 / mole')>, <Quantity(0.219093353, 'dimensionless')>)
>>> (Tt(CAS), Tm(CAS), Tb(CAS), Pt(CAS))
(<Quantity(175.61, 'kelvin')>, <Quantity(175.15, 'kelvin')>, <Quantity(337.632383,
\hookrightarrow'kelvin')>, <Quantity(0.186349762, 'pascal')>)

```
>>> iapws95_rho(T=55*u.degF, \(\mathrm{P}=500\) *u.psi)
<Quantity(1000.97992, 'kilogram / meter ** 3')>
>>> sigma_IAPWS(200*u.degR)
<Quantity(0.0897667127, 'newton / meter')>
>>> molecular_weight(\{'H': 12, 'C': 20, '0': 5\})
<Quantity(332.30628, 'gram / mole')>

Functions that do not return numbers are not converted into pint quantities, for example:
```

>>> atoms_to_Hill({'H': 5, 'C': 2, 'Br': 1})
'C2H5Br'

```

Functions that return dimensionless numbers are pint quantities.
```

>>> logP('67-56-1')
<Quantity(-0.74, 'dimensionless')>
>>> Stiel_polar_factor(Psat=169745*u.Pa, Pc=22048321.0*u.Pa, omega=0.344)
<Quantity(0.0232214674, 'dimensionless')>

```

It is also possible to use chemicals.units without the star import:
```

>>> import chemicals.units

```

When a function is used with inputs that should have units but they aren't provided by the user, an error is raised.
```

>>> ideal_gas(298.15, 101325.)
Traceback (most recent call last):
TypeError: 298.15 has no quantity

```

For further information on this interface, please see the documentation of fluids.units which is built in the same way.

\subsection*{1.32 Vapor Pressure (chemicals.vapor_pressure)}

This module contains various vapor pressure estimation routines, dataframes of fit coefficients, some compoundspecific equations, some analytical fitting routines, and sublimation pressure routines.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.

\section*{- Fit Correlations}
- Fit Correlation Derivatives
- Jacobians (for fitting)
- Vapor Pressure Estimation Correlations
- Sublimation Pressure Estimation Correlations
- Correlations for Specific Substances
- Analytical Fit Equations
- Fit Coefficients

\subsection*{1.32.1 Fit Correlations}
chemicals.vapor_pressure. Antoine \((T, A, B, C\), base \(=10.0\) )
Calculates vapor pressure of a chemical using the Antoine equation. Parameters \(A, B\), and \(C\) are chemicaldependent. Parameters can be found in numerous sources; however units of the coefficients used vary. Originally proposed by Antoine (1888) [2].
\[
\log _{\mathrm{base}} P^{\mathrm{sat}}=A-\frac{B}{T+C}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
A [float] Antoine \(A\) parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
base [float, optional] Optional base of logarithm; 10 by default

\section*{Returns}

Psat [float] Vapor pressure calculated with coefficients [Pa]

\section*{Notes}

Assumes coefficients are for calculating vapor pressure in Pascal. Coefficients should be consistent with input temperatures in Kelvin; however, if both the given temperature and units are specific to degrees Celcius, the result will still be correct.

\section*{Converting units in input coefficients:}
- In to \(\log 10\) : Divide \(A\) and \(B\) by \(\ln (10)=2.302585\) to change parameters for a \(\ln\) equation to a \(\log 10\) equation.
- \(\log 10\) to \(\ln :\) Multiply A and \(B\) by \(\ln (10)=2.302585\) to change parameters for a log equation to a ln equation.
- \(\mathbf{m m H g}\) to Pa: \(\operatorname{Add} \log 10(101325 / 760)=2.1249\) to A .
- kPa to Pa: Add \(\log _{-}\{\)base \(\}(1000)=6.908\) to A for \(\log\) (base)
- bar to Pa: Add \(\log _{-}\{\)base \(\}(100000)=11.5129254\) to A for \(\log\) (base)
- \({ }^{\circ} \mathbf{C}\) to K: Subtract 273.15 from C only!

Note that if \(C\) is negative and \(T\) is less than \(C\), the predicted vapor pressure would be high and positive at those temperatures under \(C\); and a singularity would occur at \(T==C\). This implementation is corrected to return zero for the case of \(T+C<0.0\), which matches the intention of the Antoine equation.

\section*{References}
[1], [2], [3]

\section*{Examples}

Methane, coefficients from [1], at 100 K :
```

>>> Antoine(100.0, 8.7687, 395.744, -6.469)
34478.367349639906

```

Tetrafluoromethane, coefficients from [1], at 180 K
```

>>> Antoine(180, A=8.95894, B=510.595, C=-15.95)
702271.0518579542

```

Oxygen at 94.91 K , with coefficients from [3] in units of \({ }^{\circ} \mathrm{C}, \mathrm{mmHg}, \log 10\), showing the conversion of coefficients \(\mathrm{A}(\mathrm{mmHg}\) to Pa\()\) and \(\mathrm{C}\left({ }^{\circ} \mathrm{C}\right.\) to K\()\)
```

>>> Antoine(94.91, 6.83706+2.1249, 339.2095, 268.70-273.15)
162978.88655572367

```
n-hexane with Antoine coefficients from the NIST webbook in units of \(K\) and bar, calculating the vapor pressure in Pa at 200 K :
```

>>> Antoine(T=200, A=3.45604+5, B=1044.038, C=-53.893)
20.4329803671

```
chemicals.vapor_pressure. Wagner \((T, T c, P c, a, b, c, d)\)
Calculates vapor pressure using the Wagner equation (2.5, 5 form).
Requires critical temperature and pressure as well as four coefficients specific to each chemical.
\[
\begin{gathered}
\ln P^{s a t}=\ln P_{c}+\frac{a \tau+b \tau^{1.5}+c \tau^{2.5}+d \tau^{5}}{T_{r}} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, \([\mathrm{Pa}]\)
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}

Psat [float] Vapor pressure at T [Pa]

\section*{Notes}

Warning: Pc is often treated as adjustable constant. This is also called the PPDS16 equation [3].

\section*{References}
[1], [2], [3]

\section*{Examples}

Methane, coefficients from [2], at 100 K .
>>> Wagner(100., 190.551, 4599200, -6.02242, 1.26652, -0.5707, -1.366)
34415.004762637
chemicals.vapor_pressure.Wagner_original ( \(T, T c, P c, a, b, c, d\) )
Calculates vapor pressure using the Wagner equation (3, 6 form).
Requires critical temperature and pressure as well as four coefficients specific to each chemical.
\[
\begin{gathered}
\ln P^{s a t}=\ln P_{c}+\frac{a \tau+b \tau^{1.5}+c \tau^{3}+d \tau^{6}}{T_{r}} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, \([\mathrm{K}\) ]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [Pa]
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}

Psat [float] Vapor pressure at T [Pa]

\section*{Notes}

Warning: Pc is often treated as adjustable constant. This is also called the PPDS1 equation [3].

\section*{References}
[1], [2], [3]

\section*{Examples}

Methane, coefficients from [2], at 100 K .
>>> Wagner_original(100.0, 190.53, 4596420., \(\mathrm{a}=-6.00435, \mathrm{~b}=1.1885\),
\(\ldots \mathrm{c}=-0.834082, \mathrm{~d}=-1.22833\) )
34520.44601450499
chemicals.vapor_pressure.TRC_Antoine_extended ( \(T, T c, t o, A, B, C, n, E, F)\)
Calculates vapor pressure of a chemical using the TRC Extended Antoine equation. Parameters are chemical dependent, and said to be from the Thermodynamics Research Center (TRC) at Texas A\&M. Coefficients for various chemicals can be found in [1].
\[
\begin{aligned}
\log _{10} P^{s a t} & =A-\frac{B}{T+C}+0.43429 x^{n}+E x^{8}+F x^{12} \\
x & =\max \left(\frac{T-t_{o}-273.15}{T_{c}}, 0\right)
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
Tc [float] Critical temperature of fluid, [K]
to [float] Fit temperature-transition parameter, [K]
A [float] Antoine A parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
n [float] Fit parameter, [-]
E [float] Fit parameter, [-]
F [float] Fit parameter, [-]

\section*{Returns}

Psat [float] Vapor pressure calculated with coefficients [Pa]

\section*{Notes}

Assumes coefficients are for calculating vapor pressure in Pascal. Coefficients should be consistent with input temperatures in Kelvin;

\section*{References}
[1]

\section*{Examples}

Tetrafluoromethane, coefficients from [1], at 180 K :
>>> TRC_Antoine_extended( \(\mathrm{T}=180.0\), \(\mathrm{Tc}=227.51\), to \(=-120 ., \mathrm{A}=8.95894\),
... \(\mathrm{B}=510.595, \mathrm{C}=-15.95, \mathrm{n}=2.41377, \mathrm{E}=-93.74, \mathrm{~F}=7425.9\) )
706317.0898414153
chemicals.vapor_pressure.Yaws_Psat \((T, A, B, C, D, E)\)
Calculates vapor pressure of a chemical using the Yaws equation for vapor pressure. Parameters \(A, B, C, D\), and \(E\) are chemical-dependent. Parameters can be found in numerous sources; however units of the coefficients used vary.
\[
\log _{10} P^{\mathrm{sat}}=A+\frac{B}{T}+C \log _{10}(T)+D T+E T^{2}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, \([\mathrm{K}\) ]
A [float] \(A\) parameter, [-]
B [float] \(B\) parameter, [K]
C [float] \(C\) parameter, [-]
D [float] \(D\) parameter, [1/K]
\(\mathbf{E}\) [float] \(E\) parameter, [1/K^2]

\section*{Returns}

Psat [float] Vapor pressure calculated with coefficients [Pa]

\section*{Notes}

Assumes coefficients are for calculating vapor pressure in Pascal. Coefficients should be consistent with input temperatures in Kelvin;

\section*{Converting units in input coefficients:}
- mmHg to Pa: Add \(\log 10(101325 / 760)=2.1249\) to A .
- kPa to Pa: Add \(\log _{-}\{10\}(1000)=3\) to A
- bar to Pa: Add \(\log _{-}\{10\}(100000)=5\) to A

\section*{References}
[1], [2]

\section*{Examples}

Acetone, coefficients from [1], at 400 K and with the conversion of \(A\) to obtain a result in Pa :
```

>>> Yaws_Psat(T=400.0, A=28.588 + log10(101325/760), B=-2469, C=-7.351, D=2.8025E-
๑10, E=2.7361E-6)
708657.089106

```

Coefficients for benzene from [2] at 400 K ; that source outputs vapor pressure in kPa . That style of coefficients can be converted to \(P a\) by adding 3 to \(A\).
>> Yaws_Psat \((T=400.0, A=39.7918+3, B=-2965.83, C=-12.073, \mathrm{D}=0.0033269, \mathrm{E}=1.58609 \mathrm{e}-\)
\(\rightarrow 6)\)
352443.191026
chemicals.vapor_pressure.TDE_PVExpansion( \(T, a 1, a 2, a 3, a 4=0.0, a 5=0.0, a 6=0.0, a 7=0.0, a 8=0.0\) )
Calculates vapor pressure or sublimation pressure of a chemical using the PVExpansion equation for vapor pressure or sublimation pressure. Parameters \(a 1, a 2, a 3, a 4, a 5, a 6, a 7\), and \(a 8\) are chemical-dependent. Parameters can be found in various sources; however units of the coefficients used vary.
\[
\log P^{\mathrm{sat}}=a_{1}+\frac{a_{2}}{T}+a_{3} \ln (T)+a_{4} T+a_{5} T^{2}+\frac{a_{6}}{T^{2}}+a_{7} T^{6}+\frac{a_{8}}{T^{4}}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
a1 [float] Regression parameter, [-]
a2 [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]
a5 [float] Regression parameter, [-]
a6 [float] Regression parameter, [-]
a7 [float] Regression parameter, [-]
a8 [float] Regression parameter, [-]

\section*{Returns}

Psat [float] Vapor pressure calculated with coefficients [Pa]

\section*{Notes}

Coefficients in [1] produce a vapor pressure in kPa ; add \(\log (1000)\) to \(a l\) to make them produce vapor pressure in Pa.

\section*{References}

\section*{[1]}

\section*{Examples}

Coefficients for sublimation pressure from [1]:
>> TDE_PVExpansion(T=273.16, \(\mathrm{a} 1=23.7969+\log (1000)\), \(\mathrm{a} 2=-11422, \mathrm{a} 3=0.177978\) )
4.06220657398e-05

\subsection*{1.32.2 Fit Correlation Derivatives}
chemicals.vapor_pressure.dAntoine_dT \((T, A, B, C\), base \(=10.0)\)
Calculates the first temperature derivative of vapor pressure of a chemical using the Antoine equation. Parameters \(A, B\), and \(C\) are chemical-dependent.
\[
\frac{\partial P^{\text {sat }}}{\partial T}=\frac{B \text { base }^{A-\frac{B}{C+T}} \log (\text { base })}{(C+T)^{2}}
\]

\section*{Parameters}

T [float] Temperature of fluid, [K]
A [float] Antoine \(A\) parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
base [float, optional] Optional base of logarithm; 10 by default

\section*{Returns}
dPsat_dT [float] First temperature derivative of vapor pressure calculated with coefficients [ \(\mathrm{Pa} / \mathrm{K}\) ]

\section*{Examples}

Methane at 100 K :
>> dAntoine_dT(100.0, 8.7687, 395.744, -6.469)
3591.4147747481
chemicals.vapor_pressure.d2Antoine_dT2 ( \(T, A, B, C\), base \(=10.0\) )
Calculates the second temperature derivative of vapor pressure of a chemical using the Antoine equation. Parameters \(A, B\), and \(C\) are chemical-dependent.
\[
\frac{\partial^{2} P^{\text {sat }}}{\partial T^{2}}=\frac{B \operatorname{base}^{A-\frac{B}{C+T}}\left(\frac{B \log (\text { base })}{C+T}-2\right) \log (\text { base })}{(C+T)^{3}}
\]

\section*{Parameters}

T [float] Temperature of fluid, [K]
A [float] Antoine \(A\) parameter, [-]

B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
base [float, optional] Optional base of logarithm; 10 by default

\section*{Returns}
d2Psat_dT2 [float] Second temperature derivative of vapor pressure calculated with coefficients \(\left[\mathrm{Pa} / \mathrm{K}^{\wedge} 2\right]\)

\section*{Examples}

Methane at 100 K :
>>> d2Antoine_dT2(100.0, 8.7687, 395.744, -6.469)
297.30093799054
chemicals.vapor_pressure.dWagner_dT (T,Tc, Pc,a,b,c,d)
Calculates the first temperature derivative of vapor pressure using the Wagner equation (2.5, 5 form).
Requires critical temperature and pressure as well as four coefficients specific to each chemical.
\[
\begin{gathered}
\frac{\partial P^{\mathrm{sat}}}{\partial T}=P_{c}\left(\frac{T_{c}\left(-\frac{a}{T_{c}}-\frac{1.5 b \tau^{0.5}}{T_{c}}-\frac{2.5 c \tau^{1.5}}{T_{c}}-\frac{5 d \tau^{4}}{T_{c}}\right)}{T}-\frac{T_{c}\left(a \tau+b \tau^{1.5}+c \tau^{2.5}+d \tau^{5}\right)}{T^{2}}\right) e^{\frac{T_{c}\left(a \tau+b \tau^{1.5}+c \tau^{2.5}+d \tau^{5}\right)}{T}} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, \([\mathrm{K}]\)
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [Pa]
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}
dPsat_dT [float] First temperature derivative of vapor pressure at T \([\mathrm{Pa} / \mathrm{K}]\)

\section*{Examples}

Methane at 100 K .
```

>>> dWagner_dT(100., 190.551, 4599200, -6.02242, 1.26652, -0.5707, -1.366)
3587.2910498076

```
chemicals.vapor_pressure.d2Wagner_dT2 (T, Tc, \(P c, a, b, c, d)\)
Calculates the second temperature derivative of vapor pressure using the Wagner equation (2.5, 5 form).
Requires critical temperature and pressure as well as four coefficients specific to each chemical.
\[
\frac{\partial^{2} P^{\mathrm{sat}}}{\partial T^{2}}=\frac{P_{c}\left(\frac{\frac{0.75 b}{\tau 0.5}+3.75 c \tau^{0.5}+20 d \tau^{3}}{T_{c}}+\frac{2\left(a+1.5 b \tau^{0.5}+2.5 c \tau^{1.5}+5 d \tau^{4}\right)}{T}+\frac{25\left(\frac{a}{5}+0.3 b \tau^{0.5}+0.5 c \tau^{1.5}+d \tau^{4}-\frac{T_{c}\left(-a \tau-b \tau^{1.5}-c \tau^{2.5}-d \tau^{5}\right)}{5 T}\right)^{2}}{T}-\cdots\right.}{T}
\]
\[
\tau=1-\frac{T}{T_{c}}
\]

\section*{Parameters}

T [float] Temperature of fluid, [K]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [Pa]
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}
d2Psat_dT2 [float] Second temperature derivative of vapor pressure at T \(\left[\mathrm{Pa} / \mathrm{K}^{\wedge} 2\right.\) ]

\section*{Notes}

This second derivative is infinity at \(\mathrm{T}==\mathrm{Tc}\).

\section*{Examples}

Methane at 100 K .
>>> d2Wagner_dT2(100., 190.551, 4599200, -6.02242, 1.26652, -0.5707, -1.366) 296.7091513877
chemicals.vapor_pressure.dWagner_original_dT(T, Tc, Pc, \(a, b, c, d)\)
Calculates first temperature derivative of vapor pressure using the Wagner equation ( 3,6 form).
Requires critical temperature and pressure as well as four coefficients specific to each chemical.
\[
\begin{gathered}
\frac{\partial P^{\mathrm{sat}}}{\partial T}=P_{c}\left(\frac{T_{c}\left(-\frac{a}{T_{c}}-\frac{1.5 b \tau^{0.5}}{T_{c}}-\frac{3 c \tau^{2}}{T_{c}}-\frac{6 d \tau^{5}}{T_{c}}\right)}{T}-\frac{T_{c}\left(a \tau+b \tau^{1.5}+c \tau^{3}+d \tau^{6}\right)}{T^{2}}\right) e^{\frac{T_{c}\left(a \tau+b \tau^{1.5}+c \tau^{3}+d \tau^{6}\right)}{T}} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, \([\mathrm{K}\) ]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [Pa]
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}
dPsat_dT [float] First temperature derivative of vapor pressure at T \([\mathrm{Pa} / \mathrm{K}]\)

\section*{Examples}

Methane at 100 K .
```

>>> dWagner_original_dT(100.0, 190.53, 4596420., a=-6.00435, b=1.1885,

```
\(\ldots \mathrm{c}=-0.834082, \mathrm{~d}=-1.22833\) )
3593.70783283
chemicals.vapor_pressure.d2Wagner_original_dT2 (T, Tc, \(P c, a, b, c, d)\)
Calculates second temperature derivative of vapor pressure using the Wagner equation ( 3,6 form).
Requires critical temperature and pressure as well as four coefficients specific to each chemical.
\[
\frac{\partial^{2} P^{\text {sat }}}{\partial T^{2}}=\frac{P_{c}\left(\frac{\frac{0.75 b}{\tau 0.5}+6 c \tau+30 d \tau^{4}}{T_{c}}+\frac{2\left(a+1.5 b \tau^{0.5}+3 c \tau^{2}+6 d \tau^{5}\right)}{T}+\frac{36\left(\frac{a}{6}+0.25 b \tau^{0.5}+\frac{c \tau^{2}}{2}+d \tau^{5}-\frac{T_{c}\left(-a \tau-b \tau^{1.5}-c \tau^{3}-d \tau^{6}\right)}{6 T}\right)^{2}}{T}-\frac{2 T_{c}\left(-a \tau-b \tau^{1}\right.}{T}\right.}{T}
\]
\[
\tau=1-\frac{T}{T_{c}}
\]

\section*{Parameters}

T [float] Temperature of fluid, [K]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [Pa]
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}
d2Psat_dT2 [float] Second temperature derivative of vapor pressure at \(\mathrm{T}\left[\mathrm{Pa} / \mathrm{K}^{\wedge} 2\right.\) ]

\section*{Notes}

This second derivative is infinity at \(\mathrm{T}=\mathrm{Tc}\).

\section*{Examples}

Methane at 100 K .
```

>>> d2Wagner_original_dT2(100.0, 190.53, 4596420., a=-6.00435, b=1.1885,
... c=-0.834082, d=-1.22833)
296.87593368224

```
chemicals.vapor_pressure.dTRC_Antoine_extended_dT( \(T, T c, t o, A, B, C, n, E, F)\)
Calculates the first temperature derivative of vapor pressure of a chemical using the TRC Extended Antoine equation.
\[
\begin{gathered}
\frac{\partial P^{\text {sat }}}{\partial T}=10^{A-\frac{B}{C+T}+\frac{E\left(T-T_{r e f}-t o\right)^{8}}{T_{c}^{8}}+\frac{F\left(T-T_{r e f}-t o\right)^{12}}{T_{c}^{12}}+f\left(\frac{T-T_{r e f}-t o}{T_{c}}\right)^{n}}\left(\frac{B}{(C+T)^{2}}+\frac{8 E\left(T-T_{r e f}-t o\right)^{7}}{T_{c}^{8}}+\frac{12 F\left(T-T_{r e f}-t\right.}{T_{c}^{12}}\right. \\
x=\max \left(\frac{T-t_{o}-273.15}{T_{c}}, 0\right)
\end{gathered}
\]
\[
\begin{gathered}
T_{r e f}=273.15 \mathrm{~K} \\
f=0.43429
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, \([\mathrm{K}\) ]
Tc [float] Critical temperature of fluid, [K]
to [float] Fit temperature-transition parameter, [K]
A [float] Antoine A parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
n [float] Fit parameter, [-]
E [float] Fit parameter, [-]
F [float] Fit parameter, [-]

\section*{Returns}
dPsat_dT [float] First temperature derivative of vapor pressure calculated with coefficients \([\mathrm{Pa} / \mathrm{K}]\)

\section*{Examples}

Tetrafluoromethane at 180 K :
>>> dTRC_Antoine_extended_dT(T=180.0, Tc=227.51, to=-120., A=8.95894,
\(\ldots \mathrm{B}=510.595, \mathrm{C}=-15.95, \mathrm{n}=2.41377, \mathrm{E}=-93.74, \mathrm{~F}=7425.9\) )
31219.6061263
chemicals.vapor_pressure.d2TRC_Antoine_extended_dT2 (T, Tc, to, \(A, B, C, n, E, F)\)
Calculates the second temperature derivative of vapor pressure of a chemical using the TRC Extended Antoine equation.
\[
\begin{gathered}
\frac{\partial^{2} P^{\mathrm{sat}}}{\partial T^{2}}=10^{A-\frac{B}{C+T}+\frac{E\left(-T+T_{r e f}+t o\right)^{8}}{T_{c}^{8}}+\frac{F\left(-T+T_{r e f}+t o\right)^{12}}{T_{c}^{12}}+f\left(-\frac{-T+T_{r e f}+t o}{T_{c}}\right)^{n}}\left(-\frac{2 B}{(C+T)^{3}}+\frac{56 E\left(-T+T_{r e f}+t o\right)^{6}}{T_{c}^{8}}+\frac{132 F(-}{}\right. \\
x=\max \left(\frac{T-t_{o}-273.15}{T_{c}}, 0\right) \\
T_{r e f}=273.15 \mathrm{~K} \\
f=0.43429
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
Tc [float] Critical temperature of fluid, [K]
to [float] Fit temperature-transition parameter, [K]
A [float] Antoine \(A\) parameter, [-]
B [float] Antoine \(B\) parameter, [K]

C [float] Antoine \(C\) parameter, [K]
n [float] Fit parameter, [-]
E [float] Fit parameter, [-]
F [float] Fit parameter, [-]

\section*{Returns}
d2Psat_dT2 [float] Second temperature derivative of vapor pressure calculated with coefficients [ \(\mathrm{Pa} / \mathrm{K}]\)

\section*{Examples}

Tetrafluoromethane at 180 K :
```

>>> d2TRC_Antoine_extended_dT2(T=180.0, Tc=227.51, to=-120., A=8.95894,
... B=510.595, C=-15.95, n=2.41377, E=-93.74, F=7425.9)
1022.550368944

```
chemicals.vapor_pressure.dYaws_Psat_dT ( \(T, A, B, C, D, E\) )
Calculates the first temperature derivative of vapor pressure of a chemical using the Yaws equation for vapor pressure. Parameters \(A, B, C, D\), and \(E\) are chemical-dependent. Parameters can be found in numerous sources; however units of the coefficients used vary.
\[
\frac{\partial P^{\mathrm{sat}}}{\partial T}=10^{A+\frac{B}{T}+\frac{C \log (T)}{\log (10)}+D T+E T^{2}}\left(-\frac{B}{T^{2}}+\frac{C}{T \log (10)}+D+2 E T\right) \log (10)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
A [float] \(A\) parameter, [-]
B [float] \(B\) parameter, [K]
C [float] \(C\) parameter, [-]
D [float] \(D\) parameter, [1/K]
\(\mathbf{E}\) [float] \(E\) parameter, [1/K^2]

\section*{Returns}
dPsat_dT [float] First temperature derivative of vapor pressure calculated with coefficients \([\mathrm{Pa} / \mathrm{K}]\)

\section*{Examples}

Benzene:
```

>>> dYaws_Psat_dT(T=400.0, A=42.7918, B=-2965.83, C=-12.073, D=0.0033269, E=1.
\rightarrow 5 8 6 0 9 e - 6 )
8134.87548930

```
chemicals.vapor_pressure.d2Yaws_Psat_dT2 ( \(T, A, B, C, D, E\) )
Calculates the second temperature derivative of vapor pressure of a chemical using the Yaws equation for vapor pressure. Parameters \(A, B, C, D\), and \(E\) are chemical-dependent. Parameters can be found in numerous sources;
however units of the coefficients used vary.
\[
\frac{\partial^{2} P^{\mathrm{sat}}}{\partial T^{2}}=10^{A+\frac{B}{T}+\frac{C \log (T)}{\log (10)}+D T+E T^{2}}\left(\frac{2 B}{T^{3}}-\frac{C}{T^{2} \log (10)}+2 E+\left(-\frac{B}{T^{2}}+\frac{C}{T \log (10)}+D+2 E T\right)^{2} \log (10)\right) \log (10)
\]

\section*{Parameters}

T [float] Temperature of fluid, [K]
A [float] \(A\) parameter, [-]
B [float] \(B\) parameter, [K]
C [float] \(C\) parameter, [-]
D [float] \(D\) parameter, [1/K]
\(\mathbf{E}\) [float] \(E\) parameter, [1/K^2]

\section*{Returns}
d2Psat_dT2 [float] Second temperature derivative of vapor pressure calculated with coefficients \(\left[\mathrm{Pa} / \mathrm{K}^{\wedge} 2\right]\)

\section*{Examples}

Benzene:
```

>> d2Yaws_Psat_dT2(T=400.0, A=42.7918, B=-2965.83, C=-12.073, D=0.0033269, E=1.
\hookrightarrow5609e-6)
141.7181045862

```

\subsection*{1.32.3 Jacobians (for fitting)}
chemicals.vapor_pressure. Wagner_fitting_jacobian(Ts, \(T c, P c, a, b, c, d\) )
Calculates the jacobian of the Wagner \((2.5,5)\) vapor pressure equation for use in fitting these parameters when experimental values are known.
Requires critical temperature and pressure as well as four coefficients specific to each chemical.

\section*{Parameters}

Ts [list[float]] Temperatures of fluid data points, [K]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, \([\mathrm{Pa}]\)
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}
jac [list[list[float, 4], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.vapor_pressure.Wagner_original_fitting_jacobian (Ts, Tc, Pc, \(a, b, c, d\) )
Calculates the jacobian of the Wagner \((3,6)\) vapor pressure equation for use in fitting these parameters when experimental values are known.

Requires critical temperature and pressure as well as four coefficients specific to each chemical.

\section*{Parameters}

Ts [list[float]] Temperatures of fluid data points, [K]
Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [ Pa ]
\(\mathbf{a}, \mathbf{b}, \mathbf{c}, \mathbf{d}\) [floats] Parameters for wagner equation. Specific to each chemical. [-]

\section*{Returns}
jac [list[list[float, 4], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.vapor_pressure.Antoine_fitting_jacobian (Ts, \(A, B, C\), base=10.0)
Calculates the jacobian of the Antoine vapor pressure equation for use in fitting these parameters when experimental values are known.

Requires three coefficients specific to each chemical.

\section*{Parameters}

Ts [list[float]] Temperatures of fluid data points, [K]
A [float] Antoine A parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
base [float, optional] Optional base of logarithm; 10 by default, [-]

\section*{Returns}
jac [list[list[float, 3], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.vapor_pressure.Yaws_Psat_fitting_jacobian (Ts, \(A, B, C, D, E)\)
Compute and return the Jacobian of the property predicted by the Yaws vapor pressure equation with respect to all the coefficients. This is used in fitting parameters for chemicals.

\section*{Parameters}

Ts [list[float]] Temperatures of the experimental data points, [K]
A [float] \(A\) parameter, [-]
B [float] \(B\) parameter, [K]
C [float] \(C\) parameter, [-]
D [float] \(D\) parameter, [1/K]
\(\mathbf{E}\) [float] \(E\) parameter, [1/K^2]

\section*{Returns}
jac [list[list[float, 5], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.vapor_pressure.TRC_Antoine_extended_fitting_jacobian ( \(T s, T c, t o, A, B, C, n, E, F\) )
Calculates the jacobian of the TRC Antoine extended vapor pressure equation for use in fitting these parameters when experimental values are known.
Requires 7 coefficients specific to each chemical.

\section*{Parameters}

Ts [list[float]] Temperatures of fluid data points, [K]

Tc [float] Critical temperature of fluid, [K]
to [float] Fit temperature-transition parameter, [K]
A [float] Antoine \(A\) parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]
n [float] Fit parameter, [-]
E [float] Fit parameter, [-]
F [float] Fit parameter, [-]

\section*{Returns}
jac [list[list[float, 7], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]

\subsection*{1.32.4 Vapor Pressure Estimation Correlations}
chemicals.vapor_pressure.Lee_Kesler ( \(T, T c, P c\), omega)
Calculates vapor pressure of a fluid at arbitrary temperatures using a CSP relationship by [1]; requires a chemical's critical temperature and acentric factor.

The vapor pressure is given by:
\[
\begin{gathered}
\ln P_{r}^{s a t}=f^{(0)}+\omega f^{(1)} \\
f^{(0)}=5.92714-\frac{6.09648}{T_{r}}-1.28862 \ln T_{r}+0.169347 T_{r}^{6} \\
f^{(1)}=15.2518-\frac{15.6875}{T_{r}}-13.4721 \ln T_{r}+0.43577 T_{r}^{6}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor [-]

\section*{Returns}

Psat [float] Vapor pressure at T [Pa]

\section*{Notes}

This equation appears in [1] in expanded form. The reduced pressure form of the equation ensures predicted vapor pressure cannot surpass the critical pressure.

\section*{References}
[1], [2]

\section*{Examples}

Example from [2]; ethylbenzene at 347.2 K.
>>> Lee_Kesler(347.2, 617.1, 36E5, 0.299)
13078.694162949312
chemicals.vapor_pressure.Ambrose_Walton (T,Tc, Pc, omega)
Calculates vapor pressure of a fluid at arbitrary temperatures using a CSP relationship by [1]; requires a chemical's critical temperature and acentric factor.
The vapor pressure is given by:
\[
\begin{gathered}
\ln P_{r}=f^{(0)}+\omega f^{(1)}+\omega^{2} f^{(2)} \\
f^{(0)}=\frac{-5.97616 \tau+1.29874 \tau^{1.5}-0.60394 \tau^{2.5}-1.06841 \tau^{5}}{T_{r}} \\
f^{(1)}=\frac{-5.03365 \tau+1.11505 \tau^{1.5}-5.41217 \tau^{2.5}-7.46628 \tau^{5}}{T_{r}} \\
f^{(2)}=\frac{-0.64771 \tau+2.41539 \tau^{1.5}-4.26979 \tau^{2.5}+3.25259 \tau^{5}}{T_{r}} \\
\tau=1-T_{r}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor [-]

\section*{Returns}

Psat [float] Vapor pressure at T [Pa]

\section*{Notes}

Somewhat more accurate than the Lee_Kesler formulation.

\section*{References}
[1], [2]

\section*{Examples}

Example from [2]; ethylbenzene at 347.25 K .
>>> Ambrose_Walton(347.25, 617.15, 36.09E5, 0.304)
13278.878504306222
chemicals.vapor_pressure.boiling_critical_relation( \(T, T b, T c, P c\) )
Calculates vapor pressure of a fluid at arbitrary temperatures using a CSP relationship as in [1]; requires a chemical's critical temperature and pressure as well as boiling point.

The vapor pressure is given by:
\[
\begin{aligned}
& \ln P_{r}^{s a t}=h\left(1-\frac{1}{T_{r}}\right) \\
& h=T_{b r} \frac{\ln \left(P_{c} / 101325\right)}{1-T_{b r}}
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tb [float] Boiling temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]

\section*{Returns}

Psat [float] Vapor pressure at T [Pa]

\section*{Notes}

Units are Pa. Formulation makes intuitive sense; a logarithmic form of interpolation.

\section*{References}
[1]

\section*{Examples}

Example as in [1] for ethylbenzene
>>> boiling_critical_relation(347.2, 409.3, 617.1, 36E5)
15209.467273093938
chemicals.vapor_pressure. Sanjari \((T, T c, P c\), omega)
Calculates vapor pressure of a fluid at arbitrary temperatures using a CSP relationship by [1]. Requires a chemical's critical temperature, pressure, and acentric factor. Although developed for refrigerants, this model should have some general predictive ability.

The vapor pressure of a chemical at \(T\) is given by:
\[
P^{s a t}=P_{c} \exp \left(f^{(0)}+\omega f^{(1)}+\omega^{2} f^{(2)}\right)
\]
\[
\begin{gathered}
f^{(0)}=a_{1}+\frac{a_{2}}{T_{r}}+a_{3} \ln T_{r}+a_{4} T_{r}^{1.9} \\
f^{(1)}=a_{5}+\frac{a_{6}}{T_{r}}+a_{7} \ln T_{r}+a_{8} T_{r}^{1.9} \\
f^{(2)}=a_{9}+\frac{a_{10}}{T_{r}}+a_{11} \ln T_{r}+a_{12} T_{r}^{1.9}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor [-]

\section*{Returns}

Psat [float] Vapor pressure, [Pa]

\section*{Notes}
\(\mathrm{a}[1-12]\) are as follows: \(6.83377,-5.76051,0.90654,-1.16906,5.32034,-28.1460,-58.0352,23.57466,18.19967\), 16.33839, 65.6995, -35.9739.

For a claimed fluid not included in the regression, R128, the claimed AARD was \(0.428 \%\). A re-calculation using 200 data points from 125.45 K to 343.90225 K evenly spaced by 1.09775 K as generated by NIST Webbook April 2016 produced an AARD of \(0.644 \%\). It is likely that the author's regression used more precision in its coefficients than was shown here. Nevertheless, the function is reproduced as shown in [1].

For \(\mathrm{Tc}=808 \mathrm{~K}, \mathrm{Pc}=1100000 \mathrm{~Pa}\), omega=1.1571, this function actually declines after 770 K .

\section*{References}
[1]

\section*{Examples}
```

>>> Sanjari(347.2, 617.1, 36E5, 0.299)
13651.916109552523

```
chemicals.vapor_pressure.Edalat ( \(T, T c, P c\), omega)
Calculates vapor pressure of a fluid at arbitrary temperatures using a CSP relationship by [1]. Requires a chemical's critical temperature, pressure, and acentric factor. Claimed to have a higher accuracy than the Lee-Kesler CSP relationship.

The vapor pressure of a chemical at \(T\) is given by:
\[
\begin{gathered}
\ln \left(P^{s a t} / P_{c}\right)=\frac{a \tau+b \tau^{1.5}+c \tau^{3}+d \tau^{6}}{1-\tau} \\
a=-6.1559-4.0855 \omega \\
b=1.5737-1.0540 \omega-4.4365 \times 10^{-3} d \\
c=-0.8747-7.8874 \omega
\end{gathered}
\]
\[
\begin{gathered}
d=\frac{1}{-0.4893-0.9912 \omega+3.1551 \omega^{2}} \\
\tau=1-\frac{T}{T_{c}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor [-]

\section*{Returns}

Psat [float] Vapor pressure, [Pa]

\section*{Notes}
[1] found an average error of \(6.06 \%\) on 94 compounds and 1106 data points.

\section*{References}
[1]

\section*{Examples}
```

>>> Edalat(347.2, 617.1, 36E5, 0.299)
13461.273080743307

```

\subsection*{1.32.5 Sublimation Pressure Estimation Correlations}
chemicals.vapor_pressure.Psub_Clapeyron ( \(T, T t, P t, H s u b \_t\) )
Calculates sublimation pressure of a solid at arbitrary temperatures using an approximate themodynamic identity - the Clapeyron equation as described in [1] and [2]. Requires a chemical's triple temperature, triple pressure, and triple enthalpy of sublimation.
The sublimation pressure of a chemical at \(T\) is given by:
\[
\ln \frac{P}{P_{t p}}=-\frac{\Delta H_{s u b}}{R}\left(\frac{1}{T}-\frac{1}{T_{t p}}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of solid [K]
Tt [float] Triple temperature of solid [K]
Pt [float] Truple pressure of solid [Pa]
Hsub_t [float] Enthalpy of fusion at the triple point of the chemical, [J/mol]

\section*{Returns}

Psub [float] Sublimation pressure, [Pa]

\section*{Notes}

Does not seem to capture the decrease in sublimation pressure quickly enough.

\section*{References}
[1], [2]

\section*{Examples}
>>> Psub_Clapeyron(250, Tt=273.15, Pt=611.0, Hsub_t=51100.0)
76.06457150831804
>>> Psub_Clapeyron(300, Tt=273.15, Pt=611.0, Hsub_t=51100.0)
4577.282832876156

\subsection*{1.32.6 Correlations for Specific Substances}

\section*{chemicals.vapor_pressure.Psat_IAPWS ( \(T\) )}

Calculates vapor pressure of water using the IAPWS explicit equation.
\[
\begin{gathered}
P^{s a t}=10^{6}\left[\frac{2 C}{-B+\sqrt{B^{2}-4 A C}}\right]^{4} \\
A=\nu^{2}+n_{1} \nu+n_{2} \\
B=n_{3} \nu^{2}+n_{4} \nu+n_{5} \\
C=n_{6} \nu^{2}+n_{7} \nu+n_{8} \\
\nu=T+\frac{n_{9}}{T-n_{10}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of water, [K]

\section*{Returns}

Psat [float] Vapor pressure at T [Pa]

\section*{Notes}

This formulation is quite efficient, and can also be solved backward. The range of validity of this equation is 273.15 K < T < 647.096 K, the IAPWS critical point.

Extrapolation to lower temperatures is very poor. The function continues to decrease until a pressure of 5.7 mPa is reached at 159.77353993926621 K ; under that pressure the vapor pressure increases, which is obviously wrong.

\section*{References}
[1]

\section*{Examples}
```

>>> Psat_IAPWS(300.)

```
3536.58941301301
chemicals.vapor_pressure.dPsat_IAPWS_dT(T)
Calculates the first temperature dervative of vapor pressure of water using the IAPWS explicit equation. This was derived with SymPy, using the CSE method.

\section*{Parameters}

T [float] Temperature of water, [K]

\section*{Returns}
dPsat_dT [float] Temperature dervative of vapor pressure at \(\mathrm{T}[\mathrm{Pa} / \mathrm{K}]\)

\section*{Notes}

The derivative of this is useful when solving for water dew point.

\section*{References}
[1]

\section*{Examples}
>>> dPsat_IAPWS_dT(300.)
207.88388134164282

\section*{chemicals.vapor_pressure.Tsat_IAPWS ( \(P\) )}

Calculates the saturation temperature of water using the IAPWS explicit equation.
\[
\begin{gathered}
T_{s}=\frac{n_{10}+D-\left[\left(n_{10}+D\right)^{2}-4\left(n_{9}+n_{10} D\right)\right]^{0.5}}{2} \\
E=\beta^{2}+n_{3} \beta+n_{6} \\
F=n_{1} \beta^{2}+n_{4} \beta+n_{7} \\
G=n_{2} \beta^{2}+n_{5} \beta+n_{8} \\
\beta=\left(P_{\text {sat }}\right)^{0.25}
\end{gathered}
\]

\section*{Parameters}

Psat [float] Vapor pressure at T [Pa]

\section*{Returns}

T [float] Temperature of water along the saturation curve at Psat, [K]

\section*{Notes}

The range of validity of this equation is \(273.15 \mathrm{~K}<\mathrm{T}<647.096 \mathrm{~K}\), the IAPWS critical point.
The coefficients \(n 1\) to \(n 10\) are \((0.11670521452767 \mathrm{E} 4,-0.72421316703206 \mathrm{E} 6,-0.17073846940092 \mathrm{E} 2\), \(0.12020824702470 \mathrm{E} 5, \quad-0.32325550322333 \mathrm{E} 7, \quad 0.14915108613530 \mathrm{E} 2, \quad-0.48232657361591 \mathrm{E} 4\), \(0.40511340542057 \mathrm{E} 6,-0.23855557567849,0.65017534844798 \mathrm{E} 3\) )

\section*{References}
[1]

\section*{Examples}
>>> Tsat_IAPWS(1E5)
372.75591861133773

\subsection*{1.32.7 Analytical Fit Equations}
chemicals.vapor_pressure.Antoine_coeffs_from_point ( \(T\), Psat, dPsat_dT, d2Psat_dT2, base=10.0)
Calculates the antoine coefficients \(A, B\), and \(C\) from a known vapor pressure and its first and second temperature derivative.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid, [K]
Psat [float] Vapor pressure at specified \(T\) [Pa]
dPsat_dT [float] First temperature derivative of vapor pressure at specified \(T[\mathrm{~Pa} / \mathrm{K}]\)
d2Psat_dT2 [float] Second temperature derivative of vapor pressure at specified \(T\left[\mathrm{~Pa} / \mathrm{K}^{\wedge} 2\right.\) ]
Base [float, optional] Base of logarithm; 10 by default

\section*{Returns}

A [float] Antoine \(A\) parameter, [-]
B [float] Antoine \(B\) parameter, [K]
C [float] Antoine \(C\) parameter, [K]

\section*{Notes}

Coefficients are for calculating vapor pressure in Pascal. This is primarily useful for interconverting vapor pressure models, not fitting experimental data.

Derived with SymPy as follows:
```

>>> from sympy import *
>>> base, A, B, C, T = symbols('base, A, B, C, T')
>>> v = base**(A - B/(T + C))
>>> d1, d2 = diff(v, T), diff(v, T, 2)
>>> vk, d1k, d2k = symbols('vk, d1k, d2k')
>> solve([Eq(v, vk), Eq(d1, d1k), Eq(d2, d2k)], [A, B, C])

```

\section*{References}
[1]

\section*{Examples}

Recalculate some coefficients from a calcualted value and its derivative:
```

>>> T = 178.01
>>> A, B, C = (24.0989474955895, 4346.793091137991, -18.96968471040141)
>>> Psat = Antoine(T, A, B, C, base=exp(1))
>>> dPsat_dT, d2Psat_dT2 = (0.006781441203850251, 0.0010801244983894853) \#
\hookrightarrow precomputed
>>> Antoine_coeffs_from_point(T, Psat, dPsat_dT, d2Psat_dT2, base=exp(1))
(24.098947495155, 4346.793090994, -18.969684713118)

```
chemicals.vapor_pressure.Antoine_AB_coeffs_from_point (T, Psat,dPsat_dT, base=10.0)
Calculates the antoine coefficients \(A, B\), with \(C\) set to zero to improve low-temperature or high-temperature extrapolation, from a known vapor pressure and its first temperature derivative.

\section*{Parameters}

T [float] Temperature of fluid, [K]
Psat [float] Vapor pressure at specified \(T\) [Pa]
dPsat_dT [float] First temperature derivative of vapor pressure at specified \(T[\mathrm{~Pa} / \mathrm{K}]\)
Base [float, optional] Base of logarithm; 10 by default

\section*{Returns}

A [float] Antoine \(A\) parameter, [-]
B [float] Antoine \(B\) parameter, [K]

\section*{Notes}

Coefficients are for calculating vapor pressure in Pascal. This is primarily useful for interconverting vapor pressure models, not fitting experimental data.

Derived with SymPy as follows:
```

>>> from sympy import *
>>> base, A, B, T = symbols('base, A, B, T')
>>> v = base**(A - B/T)
>>> d1, d2 = diff(v, T), diff(v, T, 2)
>>> vk, d1k = symbols('vk, d1k')
>>> solve([Eq(v, vk), Eq(d1, d1k)], [A, B])

```

\section*{References}
[1]

\section*{Examples}

Recalculate some coefficients from a calcualted value and its derivative:
```

>> T = 178.01
>>> A, B = (27.358925161569008, 5445.569591293226)
>>> Psat = Antoine(T, A, B, C=0, base=exp(1))
>>> dPsat_dT = B*exp(1)**(A - B/T)* log(exp(1))/T**2
>>> Antoine_AB_coeffs_from_point(T, Psat, dPsat_dT, base=exp(1))
(27.35892516156901, 5445.569591293226)

```
chemicals.vapor_pressure.DIPPR101_ABC_coeffs_from_point ( \(T\), Psat, \(d P s a t\) _ \(d T, d 2 P s a t \_d T 2\) )
Calculates the first three DIPPR101 coefficients \(A, B\), and \(C\) from a known vapor pressure and its first and second temperature derivative.

If the second derivative is infinity as is the case in some vapor pressure models at the critical point, only the \(A\) and \(C\) coefficients are fit, using the first derivative an the actual value of vapor pressure.

\section*{Parameters}

T [float] Temperature of fluid, [K]
Psat [float] Vapor pressure at specified \(T\) [Pa]
dPsat_dT [float] First temperature derivative of vapor pressure at specified \(T[\mathrm{~Pa} / \mathrm{K}]\)
d2Psat_dT2 [float] Second temperature derivative of vapor pressure at specified \(T\left[\mathrm{~Pa} / \mathrm{K}^{\wedge} 2\right]\)

\section*{Returns}

A [float] DIPPR101 \(A\) parameter (same as Antoine \(A\) ), [-]
B [float] DIPPR101 \(B\) parameter (same as Antoine \(B\) ), [K]
C: float DIPPR101 \(C\) parameter (NOT same as Antoine \(C\), multiplied by \(\log (\mathrm{T})\) ), \([-]\)

\section*{Notes}

Coefficients are for calculating vapor pressure in Pascal. This is primarily useful for interconverting vapor pressure models, not fitting experimental data.

Derived with SymPy as follows:
```

>>> from sympy import *
>>> base, A, B, C, T = symbols('base, A, B, C, T')
>>> v = exp(A + B/T + C* log(T))
>>> d1, d2 = diff(v, T), diff(v, T, 2)
>>> vk, d1k, d2k = symbols('vk, d1k, d2k')
>> solve([Eq(v, vk), Eq(d1, d1k), Eq(d2, d2k)], [A, B, C])

```

\section*{Examples}

Calculate the coefficients:
```

>>> T = 178.01
>>> Psat, dPsat_dT, d2Psat_dT2 = (0.03946094565666715, 0.006781441203850251, 0.
๑0010801244983894853)
>>> DIPPR101_ABC_coeffs_from_point(T, Psat, dPsat_dT, d2Psat_dT2)
(72.47169926642, -6744.620564969, -7.2976291987890)

```

\subsection*{1.32.8 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
```

chemicals.vapor_pressure.Psat_data_WagnerMcGarry

```

Coefficients for the Wagner 3,6 original model equation documented in Wagner_original with data for 245 chemicals, from [1].

\section*{chemicals.vapor_pressure.Psat_data_WagnerPoling}

Coefficients for the Wagner 2.5, 5 model equation documented in Wagner in [2], with data for 104 chemicals.

\section*{chemicals.vapor_pressure.Psat_data_AntoinePoling}

Standard Antoine equation coefficients, as documented in the function Antoine and with data for 325 fluids from [2]. Coefficients were altered to be in units of Pa and Celcius.
chemicals.vapor_pressure.Psat_data_AntoineExtended
Data for 97 chemicals in [2] for the TRC extended Antoine model TRC_Antoine_extended.
chemicals.vapor_pressure.Psat_data_Perrys2_8
A collection of 341 coefficient sets for thermo.dippr.EQ101 from the DIPPR database published openly in [4].
chemicals.vapor_pressure.Psat_data_VDI_PPDS_3
Coefficients for the Wagner equation Wagner, published openly in [3].
chemicals.vapor_pressure.Psat_data_Alcock_elements
Coefficients for the DIPPR 101 equation chemicals.dippr.EQ101, published in [5] and converted to provide base SI units (and use the natural logarithm).

The structure of each dataframe is shown below:
```

In [1]: import chemicals
In [2]: chemicals.vapor_pressure.Psat_data_WagnerMcGarry
Out[2]:
Name A ... Tc Tmin
CAS
50-00-0
56-23-5
60-29-7 diethylether -7.29916 ... 466.74 250.0
carbon tetrachloride -7.07139 ... 556.40 250.0
62-53-3 aniline -7.65517 ... 699.00 376.0
64-17-5 ethanol -8.51838 ... 513.92 293.0
7732-18-5
7782-41-4
7782-44-7

| Name | A | $\ldots$ | Tc | Tmin |
| ---: | ---: | :--- | ---: | ---: |
|  |  | $\ldots$ |  |  |
| formaldehyde -7.29343 | $\ldots$ | 408.00 | 184.0 |  |
| carbon    <br> tetrachloride -7.07139 $\ldots$ 556.40 <br> diethylether -7.29916 $\ldots$ 466.74 250.0 <br> aniline -7.65517 $\ldots$ 699.00 376.0 <br> ethanol -8.51838 $\ldots$ 513.92 293.0 <br> $\ldots$ $\ldots$ $\ldots$ $\ldots$ <br> $\ldots$ $\ldots$ 647.35 275.0 <br> water -7.76451 $\ldots$ 144.31 64.0 <br> fluorine -6.18224 $\ldots$ 154.70 54.0 oxygen -6.28275 | $\ldots$ | 154 |  |  |

```

[104 rows x 9 columns]
In [4]: chemicals.vapor_pressure.Psat_data_AntoinePoling
Out [4]:
\begin{tabular}{lrrlrr} 
& Chemical & A & \(\ldots\) & Tmin & Tmax \\
CAS & & \(\ldots\) & & \\
\(56-23-5\) & tetrachloromethane & 9.10445 & \(\ldots\) & 259.00 & 373.76 \\
\(60-29-7\) & diethyl ether & 9.10962 & \(\ldots\) & 229.71 & 328.31 \\
\(62-53-3\) & benzeneamine & 9.40870 & \(\ldots\) & 349.86 & 484.81 \\
\(64-17-5\) & ethanol & 10.33675 & \(\ldots\) & 276.50 & 369.54 \\
\(64-19-7\) & ethanoic acid & 9.54456 & \(\ldots\) & 297.58 & 414.97 \\
\(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) \\
\(14762-55-1\) & helium-3 & 6.39750 & \(\ldots\) & 1.12 & 4.41 \\
\(16747-38-9\) & \(2,3,3,4\)-tetramethylpentane & 8.99105 & \(\ldots\) & 307.81 & 443.27 \\
\(20291-95-6\) & \(2,2,5\)-trimethylheptane & 9.00345 & \(\ldots\) & 318.00 & 452.00 \\
\(800000-51-5\) & hydrogen, normal & 7.94928 & \(\ldots\) & 13.33 & 22.94 \\
\(800000-54-8\) & deuterium, normal & 8.25315 & \(\ldots\) & 17.57 & 26.23
\end{tabular}
```

[325 rows x 6 columns]

```
In [5]: chemicals.vapor_pressure.Psat_data_AntoineExtended
Out[5]:
\begin{tabular}{rrrrr} 
Chemical & A & \(\ldots\) & Tmin & Tmax \\
benzeneamine & 9.40870 & \(\ldots\) & & \\
ethene & 8.91382 & \(\ldots\) & 188.15 & 673.15 \\
methanamine & 9.21300 & \(\ldots\) & 288.15 & 423.15 \\
ethanamine & 8.88560 & \(\ldots\) & 308.15 & 443.15 \\
difluoromethane & 9.29712 & \(\ldots\) & 238.15 & 338.15 \\
\(\ldots\) & \(\ldots\). & \(\ldots\) & \(\ldots\) & \(\ldots\) \\
3-ethyl-3-methylpentane & 8.98950 & \(\ldots\) & 408.15 & 543.15
\end{tabular}
(continued from previous page)
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline 1511-62-2 & \multicolumn{2}{|r|}{bromodifluoromethan} & - 8.40030 & \multicolumn{2}{|r|}{273.1540} & 03.15 \\
\hline 1640-89-7 & \multicolumn{2}{|r|}{ethylcyclopentane} & 9.00408 & \multicolumn{2}{|r|}{408.1556} & 69.52 \\
\hline 1717-00-6 & \multicolumn{2}{|l|}{1,1-dichloro-1-fluoroethane} & 9.03117 & \multicolumn{2}{|r|}{333.1547} & 73.15 \\
\hline 2837-89-0 & \multicolumn{2}{|l|}{1-chloro-1,2,2,2-tetrafluoroethane} & 8.98581 & \multicolumn{2}{|r|}{283.1538} & 383.15 \\
\hline \multicolumn{7}{|l|}{[97 rows x 11 columns]} \\
\hline \multicolumn{7}{|l|}{In [6]: chemicals.vapor_pressure.Psat_data_Perrys2_8} \\
\hline \multicolumn{7}{|l|}{Out[6]:} \\
\hline & Chemical & C1 & 1 C2 & C5 & Tmin & Tmax \\
\hline \multicolumn{7}{|l|}{CAS} \\
\hline 50-00-0 & Formaldehyde & 101.510 & -4917.20 & 1.0 & 181.15 & 408.00 \\
\hline 55-21-0 & Benzamide & 85.474 & -11932.00 & 6.0 & 403.00 & 824.00 \\
\hline 56-23-5 & Carbon tetrachloride & 78.441 & -6128.10 & 2.0 & 250.33 & 556.35 \\
\hline 57-55-6 & 1,2-Propylene glycol & 212.800 & -15420.00 & 2.0 & 213.15 & 626.00 \\
\hline 60-29-7 & Diethyl ether & 136.900 & -6954.30 & 1.0 & 156.85 & 466.70 \\
\hline & & & & & & \\
\hline 10028-15-6 & Ozone & 40.067 & -2204.80 & 6.0 & 80.15 & 261.00 \\
\hline 10035-10-6 & Hydrogen bromide & 29.315 & -2424.50 & 6.0 & 185.15 & 363.15 \\
\hline 10102-43-9 & Nitric oxide & 72.974 & -2650.00 & 6.0 & 109.50 & 180.15 \\
\hline 13511-13-2 & Propenylcyclohexene & 64.268 & -7298.90 & 6.0 & 199.00 & 636.00 \\
\hline 132259-10-0 & Air & 21.662 & \(2-692.39\) & 1.0 & 59.15 & 132.45 \\
\hline \multicolumn{7}{|l|}{[340 rows x 8 columns]} \\
\hline \multicolumn{7}{|l|}{In [7]: chemicals.vapor_pressure.Psat_data_VDI_PPDS_3} \\
\hline \multicolumn{7}{|l|}{Out[7]:} \\
\hline & Chemical & Tm & Tc & B & C & D \\
\hline \multicolumn{7}{|l|}{CAS} \\
\hline 50-00-0 & Formaldehyde & 181.1540 & 408.05 & 1.28290 & -0. 50464 & -4.29089 \\
\hline 56-23-5 & Carbon tetrachloride & 250.2555 & 556.35 & 1.96174 & -2.05900 & -3.26771 \\
\hline 56-81-5 & Glycerol & 291.4585 & 850.05 & -0.33345- & -5.98569 & -1.33011 \\
\hline 60-29-7 & Diethyl ether & 156.7546 & 466.63 & \(2.15613-\) & -3.02766 & -2.37858 \\
\hline 62-53-3 & Aniline & 267.1569 & 699.05 & 1.96206 - & -3.65571 & -2.00622 \\
\hline & & & & & & \\
\hline 10097-32-2 & Bromine & \(265.85 \quad 58\) & 584.15 & 1.50339 & -0.64097 & -3.62166 \\
\hline 10102-43-9 & Nitric oxide & 112.1518 & 180.15 & 0.85755 - & -3.11447 & -8.98765 \\
\hline 10102-44-0 & Nitrogen dioxide & 261.8543 & 431.15 & 2.37620 & 0.67820 & -2.53997 \\
\hline 10544-72-6 & Dinitrogentetroxide & 261.8543 & 431.10 & 3.10196 & 0.59704 & -5.33648 \\
\hline 132259-10-0 & Air & 63.05132 & 132.53 & -0.21537 & 0.93623 & -3.02641 \\
\hline
\end{tabular}
[275 rows x 8 columns]
In [8]: chemicals.vapor_pressure.Psat_data_Alcock_elements
Out [8]:
\begin{tabular}{lrrrrrrr} 
& name & \multicolumn{2}{c}{ A } & B & \(\ldots\) & E & Tmin \\
CAS & & & \(\ldots\) & & & \\
\(7439-93-2 ~\) & lithium & 30.888526 & -19157.507974 & \(\ldots\) & -3.0 & 453.6500 & 1000.0 \\
\(7440-23-5\) & sodium & 30.867803 & -12972.764414 & \(\ldots\) & -3.0 & 370.9440 & 700.0 \\
\(7440-09-7\) & potassium & 30.483272 & -10806.031841 & \(\ldots\) & -3.0 & 336.6500 & 600.0 \\
\(7440-17-7\) & Rubidium & 30.674386 & -9843.551273 & \(\ldots\) & -3.0 & 312.4500 & 550.0 \\
\(7440-46-2\) & Caesium & 30.480969 & -9353.100648 & \(\ldots\) & -3.0 & 301.6500 & 550.0
\end{tabular}
\begin{tabular}{|c|c|c|c|c|c|c|}
\hline \multicolumn{7}{|l|}{} \\
\hline 7429-90-5 & Aluminium & 35.882834 & -39019.606986 & -3.0 & 933.4730 & 1800.0 \\
\hline 7440-55-3 & gallium & 19.870657 & -31842.449251 & -3.0 & 302.9146 & 1600.0 \\
\hline 7440-74-6 & Indium & 34.365430 & -28938.889449 & -3.0 & 429.7500 & 1500.0 \\
\hline 7440-28-0 & Thallium & 31.392793 & -21605.155928 & -3.0 & 577.1500 & 1100.0 \\
\hline 7440-31-5 & Tin & 17.786817 & -34785.153000 & -3.0 & 505.0780 & 1850.0 \\
\hline 7439-92-1 & Lead & 31.171744 & -23239.991344 & -3.0 & 600.6120 & 1200.0 \\
\hline 7440-65-5 & Yttrium & 43.175121 & -51151.927841 & -3.0 & 1795.1500 & 2300.0 \\
\hline 7439-91-0 & Lanthanum & 26.548154 & -50603.912589 & -3.0 & 1193.1500 & 2450.0 \\
\hline 7440-32-6 & Titanium & 49.219406 & -58091.919311 & -3.0 & 1943.1500 & 2400.0 \\
\hline 7440-67-7 & Zirconium & 15.173383 & -66231.557615 & -3.0 & 2127.1500 & 2500.0 \\
\hline 7440-06-4 & Platinum & 60.472140 & -71198.233660 & -3.0 & 2041.3500 & 2500.0 \\
\hline 7440-50-8 & Copper & 37.335765 & -40127.150416 & -3.0 & 1357.7700 & 1850.0 \\
\hline 7440-57-5 & Gold & 35.238110 & -43514.253087 & -3.0 & 1337.3300 & 2050.0 \\
\hline 7440-45-1 & Cerium & 25.394558 & -48994.405609 & -3.0 & 1072.1500 & 2450.0 \\
\hline 7440-10-0 & Praseodymium & 38.965995 & -43042.223143 & -3.0 & 1204.1500 & 2200.0 \\
\hline 7440-00-8 & Neodymium & 40.068933 & -39717.290269 & -3.0 & 1289.1500 & 2000.0 \\
\hline 7440-54-2 & Gadolinium & 35.947306 & -47214.507332 & -3.0 & 1586.1500 & 2250.0 \\
\hline 7440-27-9 & Terbium & 38.703500 & -46171.436285 & -3.0 & 1632.1500 & 2200.0 \\
\hline 7439-94-3 & Lutetium & 54.932120 & -54202.853089 & -3.0 & 1936.1500 & 2350.0 \\
\hline 7440-29-1 & Thorium & 148.700293 & -85151.899324 & -3.0 & 2023.1500 & 2500.0 \\
\hline 7440-13-3 & Protactinium & 35.081534 & -78331.642279 & -3.0 & 1845.1500 & 2500.0 \\
\hline 7439-99-8 & Neptunium & 48.979938 & -55303.488764 & -3.0 & 917.1500 & 2500.0 \\
\hline 7440-07-5 & Plutonium & 41.441274 & -40495.564030 & -3.0 & 913.1500 & 2450.0 \\
\hline 7440-51-9 & Curium & 56.511693 & -49353.608883 & -3.0 & 1618.1500 & 2200.0 \\
\hline 7440-41-7 & Beryllium & 24.848846 & -36221.966098 & -3.0 & 1560.1500 & 1800.0 \\
\hline 7440-39-3 & Barium & 20.752547 & -18796.002114 & -3.0 & 1000.1500 & 1200.0 \\
\hline 7440-20-2 & Scandium & 24.869569 & -40712.007029 & -3.0 & 1814.1500 & 2000.0 \\
\hline 7440-62-2 & Vanadium & 27.480701 & -57589.955761 & -3.0 & 2183.1500 & 2500.0 \\
\hline 7439-89-6 & Iron & 26.140596 & -45070.800610 & -3.0 & 1811.1500 & 2100.0 \\
\hline 7440-48-4 & Cobalt & 26.465261 & -47382. 596044 & -3.0 & 1768.1500 & 2150.0 \\
\hline 7440-02-0 & Nickel & 26.875121 & -47813.179456 & -3.0 & 1728.1500 & 2150.0 \\
\hline 7440-05-3 & Palladium & 24.019915 & -41213.970580 & -3.0 & 1827.9500 & 2100.0 \\
\hline 7440-22-4 & Silver & 24.770558 & -31837.844081 & -3.0 & 1234.9300 & 1600.0 \\
\hline 7440-66-6 & Zinc & 23.909391 & -14474.049895 & -3.0 & 692.6770 & 750.0 \\
\hline 7440-43-9 & Cadmium & 23.596240 & -12415.538821 & -3.0 & 594.2190 & 650.0 \\
\hline 7439-97-6 & Mercury & 23.306114 & -7345.246447 & -3.0 & 298.0000 & 400.0 \\
\hline 7440-52-0 & Erbium & 22.320607 & -33111.173637 & -3.0 & 1802.1500 & 1900.0 \\
\hline 7440-61-1 & Uranium & 59.270190 & -66259.188636 & -3.0 & 1408.1500 & 2500.0 \\
\hline
\end{tabular}
[43 rows x 8 columns]

\subsection*{1.33 Support for Numpy Arrays (chemicals.vectorized)}

Basic module which wraps all chemicals functions with numpy's np.vectorize function.
All other object - dicts, classes, etc - are not wrapped. Supports star imports; so the same objects exported when importing from the main library will be imported from here.
```

>>> from chemicals.vectorized import *
>>> Antoine(np.linspace(100, 200, 5), A=8.95894, B=510.595, C=-15.95)

```
(continues on next page)
```

array([7.65674361e+02, 1.89116754e+04, 1.41237759e+05, 5.60609191e+05,
1.53010431e+06])

```

Inputs do not need to be numpy arrays; they can be any iterable:
```

>>> import chemicals.vectorized
>>> chemicals.vectorized.Tc(['108-88-3', '7732-18-5'])
array([591.75 , 647.096])

```

Warning: This module does not replace the functions in the chemicals module; it copies all the functions into the chemicals.vectorized module and makes them vectorized there.

For example by importing chemicals.vectorized, chemicals.Antoine won't become vectorized, but chemicals.vectorized.Antoine will become available and is vectorized.

Warning: np.vectorize does not use NumPy to accelerate any computations; it is a convenience wrapper. If you are working on a problem large enough for speed to be an issue and Numba is compatible with your version of Python, an interface to that library is available at chemicals . numba which does accelerate NumPy array computations and is normally faster than using numpy directly.

\subsection*{1.34 Virial Coefficients (chemicals.virial)}

This module contains four estimation methods for second \(B\) virial coefficients, two utility covnersions for when only \(B\) is considered, and two methods to calculate \(Z\) from higher order virial expansions.

For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Utilities
- Second Virial Correlations
- Third Virial Correlations
- Cross-Parameters
- Second Virial Correlations Dense Implementations
- Third Virial Correlations Dense Implementations

\subsection*{1.34.1 Utilities}
chemicals.virial.B_to_Z \((B, T, P)\)
Calculates the compressibility factor of a gas, given its second virial coefficient.
\[
Z=\frac{P V}{R T}=1+\frac{B P}{R T}
\]

\section*{Parameters}

B [float] Second virial coefficient, [m^3/mol]

T [float] Temperature, [K]
\(\mathbf{P}\) [float] Pressure [Pa]

\section*{Returns}
\(\mathbf{Z}\) [float] Compressibility factor, [-]

Notes
Other forms of the virial coefficient exist.

\section*{References}
[1]

\section*{Examples}
>>> B_to_Z (-0.0015, 300, 1E5)
0.939863822478637
chemicals.virial.B_from_Z(Z,T, \(P\) )
Calculates the second virial coefficient of a pure species, given the compressibility factor of the gas.
\[
B=\frac{R T(Z-1)}{P}
\]

\section*{Parameters}

Z [float] Compressibility factor, [-]
T [float] Temperature, [K]
\(\mathbf{P}\) [float] Pressure [Pa]

\section*{Returns}

B [float] Second virial coefficient, [m^3/mol]

Notes
Other forms of the virial coefficient exist.

References
[1]

\section*{Examples}
>> B_from_Z(0.94, 300, 1E5)
-0.0014966032712675846

\section*{chemicals.virial.Z_from_virial_density_form ( \(T, P\), *args)}

Calculates the compressibility factor of a gas given its temperature, pressure, and molar density-form virial coefficients. Any number of coefficients is supported.
\[
Z=\frac{P V}{R T}=1+\frac{B}{V}+\frac{C}{V^{2}}+\frac{D}{V^{3}}+\frac{E}{V^{4}} \ldots
\]

\section*{Parameters}

T [float] Temperature, [K]
\(\mathbf{P}\) [float] Pressure, [Pa]
B to \(\mathbf{Z}\) [float, optional] Virial coefficients, [various]

\section*{Returns}
\(\mathbf{Z}\) [float] Compressibility factor at T, P , and with given virial coefficients, [-]

\section*{Notes}

For use with B or with B and C or with B and C and D, optimized equations are used to obtain the compressibility factor directly. If more coefficients are provided, uses numpy's roots function to solve this equation. This takes substantially longer as the solution is numerical.

If no virial coefficients are given, returns 1 , as per the ideal gas law.
The units of each virial coefficient are as follows, where for \(\mathrm{B}, \mathrm{n}=1\), and \(\mathrm{C}, \mathrm{n}=2\), and so on.
\[
\left(\frac{\mathrm{m}^{3}}{\mathrm{~mol}}\right)^{n}
\]

\section*{References}
[1], [2]

\section*{Examples}
>>> Z_from_virial_density_form(300, 122057.233762653, 1E-4, 1E-5, 1E-6, 1E-7) 1.28434940526
chemicals.virial.Z_from_virial_pressure_form ( \(P\), *args)
Calculates the compressibility factor of a gas given its pressure, and pressure-form virial coefficients. Any number of coefficients is supported.
\[
Z=\frac{P v}{R T}=1+B^{\prime} P+C^{\prime} P^{2}+D^{\prime} P^{3}+E^{\prime} P^{4} \ldots
\]

\section*{Parameters}
\(\mathbf{P}\) [float] Pressure, [Pa]
B to Z [float, optional] Pressure form Virial coefficients, [various]

\section*{Returns}

Z [float] Compressibility factor at P , and with given virial coefficients, [-]

\section*{Notes}

Note that although this function does not require a temperature input, it is still dependent on it because the coefficients themselves normally are regressed in terms of temperature.
The use of this form is less common than the density form. Its coefficients are normally indicated with the """ suffix.
If no virial coefficients are given, returns 1 , as per the ideal gas law.
The units of each virial coefficient are as follows, where for \(\mathrm{B}, \mathrm{n}=1\), and \(\mathrm{C}, \mathrm{n}=2\), and so on.
\[
\left(\frac{1}{\mathrm{~Pa}}\right)^{n}
\]

\section*{References}
[1], [2]

\section*{Examples}
>>> Z_from_virial_pressure_form(102919.99946855308, 4.032286555169439e-09, 1. \(\rightarrow 6197059494442215 \mathrm{e}-13,6.483855042486911 \mathrm{e}-19)\)
1.00283753944

\section*{chemicals.virial.BVirial_mixture(zs, Bijs)}

Calculate the \(B\) second virial coefficient from a matrix of virial cross-coefficients. The diagonal is virial coefficients of the pure components.
\[
B=\sum_{i} \sum_{j} y_{i} y_{j} B(T)
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Bijs [list[list[ffoat]]] Second virial coefficient in density form [m^3/mol]

\section*{Returns}

B [float] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{References}
[1]

\section*{Examples}
```

>>> Bijs = [[-6.24e-06, -2.013e-05, -3.9e-05], [-2.01e-05, -4.391e-05, -6.46e-05],,
[-3.99e-05, -6.46e-05, -0.00012]]
>>> zs = [.5, .3, .2]
>>> BVirial_mixture(zs=zs, Bijs=Bijs)
-3.19884e-05

```
chemicals.virial.dBVirial_mixture_dzs(zs, Bijs, \(\left.d B \_d z s=N o n e\right)\)
Calculate first mole fraction derivative of the \(B\) second virial coefficient from a matrix of virial cross-coefficients.
\[
\frac{\partial B}{\partial x_{i}}=\sum_{j} z_{j}\left(B_{i, j}+B_{j, i}\right)
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Bijs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dzs [list[float], optional] Array for first mole fraction derivatives of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Returns}
dB_dzs [list[float]] First mole fraction derivatives of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Examples}
```

>>> Bijs = [[-6.24e-06, -2.013e-05, -3.9e-05], [-2.01e-05, -4.391e-05, -6.46e-05],, 七
\rightarrow [ - 3 . 9 9 e - 0 5 , ~ - 6 . 4 6 e - 0 5 , ~ - 0 . 0 0 0 1 2 ] ] ~
>>> zs = [.5, .3, .2]
>>> dBVirial_mixture_dzs(zs=zs, Bijs=Bijs)
[-3.4089e-05, -7.2301e-05, -0.00012621]

```

\section*{chemicals.virial.d2BVirial_mixture_dzizjs(zs, Bijs, d2B_dzizjj=None)}

Calculate second mole fraction derivative of the \(B\) second virial coefficient from a matrix of virial crosscoefficients.
\[
\frac{\partial^{2} B}{\partial x_{i} \partial x_{j}}=B_{i, j}+B_{j, i}
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Bijs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
d2B_dzizjs [list[list[float]], optional] Array for First mole fraction derivatives of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Returns}
d2B_dzizjs [list[list[float]]] First mole fraction derivatives of second virial coefficient in density form [m^3/mol]

\section*{Examples}
```

>>> Bijs = [[-6.24e-06, -2.013e-05, -3.9e-05], [-2.01e-05, -4.391e-05, -6.46e-05],,
[-3.99e-05, -6.46e-05, -0.00012]]
>>> zs = [.5, .3, .2]
>>> d2BVirial_mixture_dzizjs(zs=zs, Bijs=Bijs)
[[-1.248e-05, -4.023e-05, -7.89e-05], [-4.023e-05, -8.782e-05, -0.0001292], [-7.89e-
->05, -0.0001292, -0.00024]]

```
chemicals.virial.d3BVirial_mixture_dzizjzks(zs, Bijs,d3B_dzizjzks=None)
Calculate third mole fraction derivative of the \(B\) third virial coefficient from a matrix of virial cross-coefficients.
\[
\frac{\partial^{3} B}{\partial x_{i} \partial x_{j} \partial x_{k}}=0
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Bijs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
d3B_dzizjzks [list[list[list[float]]]] Array for third mole fraction derivatives of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
d3B_dzizjzks [list[list[list[float]]]] Third mole fraction derivatives of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Examples}
```

>>> Bijs = [[-6.24e-06, -2.013e-05, -3.9e-05], [-2.01e-05, -4.391e-05, -6.46e-05],,
\leftrightarrow[-3.99e-05, -6.46e-05, -0.00012]]
>>> zs = [.5, .3, .2]
>>> d3BVirial_mixture_dzizjzks(zs=zs, Bijs=Bijs)
[[[0.0, 0.0, 0.0], [0.0, 0.0, 0.0], [0.0, 0.0, 0.0]], [[0.0, 0.0, 0.0], [0.0, 0.0, ь
\rightarrow 0 . 0 ] , ~ [ 0 . 0 , ~ 0 . 0 , ~ 0 . 0 ] ] , ~ [ [ 0 . 0 , ~ 0 . 0 , ~ 0 . 0 ] , ~ [ 0 . 0 , ~ 0 . 0 , ~ 0 . 0 ] , ~ [ 0 . 0 , ~ 0 . 0 , ~ 0 . 0 ] ] ] ~ ]

```
chemicals.virial.CVirial_mixture_Orentlicher_Prausnitz (zs, Cijs)
Calculate the \(C\) third virial coefficient from a matrix of virial cross-coefficients. The diagonal is virial coefficients of the pure components.
\[
\begin{gathered}
C=\sum_{i} \sum_{j} \sum_{k} y_{i} y_{j} y_{k} C_{i j k}(T) \\
C_{i j k}=\left(C_{i j} C_{j k} C_{i k}\right)^{1 / 3}
\end{gathered}
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Cijs [list[list[float]]] Third virial binary interaction coefficients in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2\) ]

\section*{Returns}
\(\mathbf{C}\) [float] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]

\section*{References}
[1]

\section*{Examples}
>>> Cijs \(=[[1.46 e-09,1.831 e-09,2.12 e-09], \quad[1.831 e-09,2.46 e-09,2.996 e-09]\), [2.
\(\rightarrow 12 \mathrm{e}-09,2.996 \mathrm{e}-09,4.927 \mathrm{e}-09]]\)
>>> zs = [.5, .3, .2]
>>> CVirial_mixture_Orentlicher_Prausnitz(zs, Cijs)
\(2.0790440095 \mathrm{e}-09\)
chemicals.virial.dCVirial_mixture_dT_Orentlicher_Prausnitz(zs, Cijs, dCij_dTs)
Calculate the first temperature derivative of the \(C\) third virial coefficient from matrices of virial cross-coefficients and their first temperature derivatives.
\(\frac{\partial C}{\partial T}=\sum_{i} \sum_{j} \sum_{k} \frac{z i z j z k \sqrt[3]{\operatorname{Cij}(T) \operatorname{Cik}(T) \operatorname{Cjk}(T)}\left(\frac{\operatorname{Cij}(T) \operatorname{Cik}(T) \frac{d}{d T} \operatorname{Cjk}(T)}{3}+\frac{\operatorname{Cij}(T) \operatorname{Cjk}(T) \frac{d}{d T} \operatorname{Cik}(T)}{3}+\frac{\operatorname{Cik}(T) \operatorname{Cjk}(T) \frac{d}{d T} \operatorname{Cij}(T}{3}\right.}{\operatorname{Cij}(T) \operatorname{Cik}(T) \operatorname{Cjk}(T)}\)

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Cijs [list[list[float]]] Third virial binary interaction coefficients in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dCij_dTs [list[list[float]]] First temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)

\section*{Returns}
dC_dT [float] First temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge}{ }^{\wedge} / \mathrm{K}\right]\)

\section*{References}
[1]

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
->12e-09, 2.996e-09, 4.927e-09]]
>>> dCij_dTs = [[-2.212e-12, -4.137e-12, -1.079e-11], [-4.137e-12, -7.669e-12, -1.
\rightarrow 8 0 9 e - 1 1 ] , ~ [ - 1 . 0 7 9 e - 1 1 , ~ - 1 . 8 0 9 e - 1 1 , ~ - 2 . 0 1 0 e - 1 1 ] ] ~ ]
>>> zs = [.5, .3, .2]
>>> dCVirial_mixture_dT_Orentlicher_Prausnitz(zs, Cijs, dCij_dTs)
-7.2751517e-12

```
chemicals.virial.d2CVirial_mixture_dT2_Orentlicher_Prausnitz(zs, Cijs,dCij_dTs,d2Cij_dT2s)
Calculate the second temperature derivative of the \(C\) third virial coefficient from matrices of virial crosscoefficients and their first and second temperature derivatives.
\[
\frac{\partial^{2} C}{\partial T^{2}}=\sum_{i} \sum_{j} \sum_{k} z_{i} z_{j} z_{k} \frac{\sqrt[3]{\operatorname{Cij}(T) \operatorname{Cik}(T) \operatorname{Cjk}(T)}\left(\frac{\left(\operatorname{Cij}(T) \operatorname{Cik}(T) \frac{d}{d T} \operatorname{Cjk}(T)+\operatorname{Cij}(T) \operatorname{Cjk}(T) \frac{d}{d T} \operatorname{Cik}(T)+\operatorname{Cik}(T) \operatorname{Cjk}(T) \frac{d}{d T} \operatorname{Cij}(T)\right)^{2}}{\operatorname{Cij}(T) \operatorname{Cik}(T) \operatorname{Cjk}(T)}\right.}{\text { ? }}
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Cijs [list[list[float]]] Third virial binary interaction coefficients in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2\) ]
dCij_dTs [list[list[float]]] First temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge}{ }^{\wedge} / \mathrm{K}\right]\)
d2Cij_dT2s [list[list[float]]] Second temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)

\section*{Returns}
d2C_dT2 [float] Second temperature derivative of third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\) ]

\section*{References}
[1]

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
42e-09, 2.996e-09, 4.927e-09]]
>>> dCij_dTs = [[-2.212e-12, -4.137e-12, -1.079e-11], [-4.137e-12, -7.669e-12, -1.
409e-11], [-1.079e-11, -1.809e-11, -2.010e-11]]
>>> d2Cij_dT2s = [[ 2.6469e-14, 5.0512e-14, 1.1509e-13], [ 5.0512e-14, 9.3272e-
\leftrightarrow14, 1.7836e-13], [ 1.1509e-13, 1.7836e-13, -1.4906e-13]]
>>> zs = [.5, .3, .2]
>>> d2CVirial_mixture_dT2_Orentlicher_Prausnitz(zs, Cijs, dCij_dTs, d2Cij_dT2s)
6.7237107787e-14

```
chemicals.virial.d3CVirial_mixture_dT3_Orentlicher_Prausnitz(zs, \(C_{i j s,} d C i j \_d T s, d 2 C i j \_d T 2 s\), d3Cij_dT3s)
Calculate the third temperature derivative of the \(C\) third virial coefficient from matrices of virial cross-coefficients and their first, second, and third temperature derivatives.
The expression is quite lengthy and not shown here [1].
\[
\frac{\partial^{3} C}{\partial T^{3}}
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Cijs [list[[list[float]]] Third virial binary interaction coefficients in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dCij_dTs [list[list[float]]] First temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2Cij_dT2s [list[list[float]]] Second temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3Cij_dT3s [list[list[float]]] Third temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2^{\wedge} 2\right]\)

\section*{Returns}
d3C_dT3 [float] Third temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{References}
[1]

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
->12e-09, 2.996e-09, 4.927e-09]]
>>> dCij_dTs = [[-2.212e-12, -4.137e-12, -1.079e-11], [-4.137e-12, -7.669e-12, -1.
\leftrightarrows09e-11], [-1.079e-11, -1.809e-11, -2.010e-11]]
>>> d2Cij_dT2s = [[ 2.6469e-14, 5.0512e-14, 1.1509e-13], [ 5.0512e-14, 9.3272e-
44, 1.7836e-13], [ 1.1509e-13, 1.7836e-13, -1.4906e-13]]
>>> d3Cij_dT3s = [[-4.2300e-16, -7.9727e-16, -1.6962e-15], [-7.9727e-16, -1.3826e-
->15, -1.4525e-15], [-1.6962e-15, -1.4525e-15, 1.9786e-14]]
>>> zs = [.5, .3, .2]
>>> d3CVirial_mixture_dT3_Orentlicher_Prausnitz(zs, Cijs, dCij_dTs, d2Cij_dT2s,_
\&3Cij_dT3s)
-3.7358368e-16

```

\section*{chemicals.virial.dCVirial_mixture_Orentlicher_Prausnitz_dzs(zs,Cijs,dCs=None)}

Calculate the first mole fraction derivatives of the \(C\) third virial coefficient from a matrix of virial crosscoefficients.
\[
\frac{\partial C}{\partial z_{m}}=\sum_{\substack{0 \leq i \leq n c \\ 0 \leq j \leq n c \\ 0 \leq k \leq n c}} \sqrt[3]{C s_{i, j} C s_{i, k} C s_{j, k}}\left(\delta_{i m} z s_{j} z s_{k}+\delta_{j m} z s_{i} z s_{k}+\delta_{k m} z s_{i} z s_{j}\right)
\]

\section*{Parameters}
zs [list[float] Mole fractions of each species, [-]
Cijs [list[list[float]]] Third virial binary interaction coefficients in density form [m^6/mol \({ }^{\wedge} 2\) ]
dCs [list[float], optional] First derivatives of C with respect to mole fraction, [m^6/mol^2]

\section*{Returns}
dC_dzs [list[float]] First derivatives of \(C\) with respect to mole fraction, \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\right.\) ]

\section*{Notes}

This equation can be derived with SymPy, as follows
```

>>> from sympy import *
>>> i, j, k, m, n, o = symbols("i, j, k, m, n, o", cls=Idx)
>>> zs = IndexedBase('zs')
>>> Cs = IndexedBase('Cs')
>>> nc = symbols('nc')
>>> C_expr = Sum(zs[i]*zs[j]*zs[k]*Cbrt(Cs[i,j]*Cs[i,k]*Cs[j,k]),[i,0,nc],[j,0,nc],
\hookrightarrowk,0,nc])

```
```

>>> diff(C_expr, zs[m])
Sum((Cs[i, j]*Cs[i, k]*Cs[j, k])**(1/3)*KroneckerDelta(i,m)*zs[j]*zs[k] + (Cs[i,七
\hookrightarrowj]*Cs[i,k]*Cs[j, k])**(1/3)*KroneckerDelta(j, m)*zs[i]*zs[k] + (Cs[i, j]*Cs[i,七
\hookrightarrowk]*Cs[j, k])**(1/3)*KroneckerDelta(k, m)*zs[i]*zs[j], (i, 0, nc), (j, 0, nc), (k,七
@, nc))

```

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
412e-09, 2.996e-09, 4.927e-09]]
>>> zs = [.5, .3, .2]
>>> dCVirial_mixture_Orentlicher_Prausnitz_dzs(zs, Cijs)
[5.44450470e-09, 6.54968776e-09, 7.74986672e-09]

```
chemicals．virial．d2CVirial＿mixture＿Orentlicher＿Prausnitz＿dzizjs（zs，Cijs，d2Cs＝None）
Calculate the second mole fraction derivatives of the \(C\) third virial coefficient from a matrix of virial cross－ coefficients．
\[
\frac{\partial^{2} C}{\partial z_{m} \partial z_{n}}=\sum_{\substack{0 \leq i \leq n c \\ 0 \leq j \leq n c \\ 0 \leq k \leq n c}} \sqrt[3]{C s_{i, j} C s_{i, k} C s_{j, k}}\left(\delta_{i m} \delta_{j n} z s_{k}+\delta_{i m} \delta_{k n} z s_{j}+\delta_{i n} \delta_{j m} z s_{k}+\delta_{i n} \delta_{k m} z s_{j}+\delta_{j m} \delta_{k n} z s_{i}+\delta_{j n} \delta_{k m} z s_{i}\right)
\]

\section*{Parameters}
zs［list［float］］Mole fractions of each species，［－］
Cijs［list［list［float］］］Third virial binary interaction coefficients in density form［m＾6／mol \({ }^{\wedge} 2\) ］
d2Cs［list［list［float］］，optional］Second derivatives of C with respect to mole fraction， ［ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\right]\)

\section*{Returns}
d2Cs［list［list［float］］］Second derivatives of \(C\) with respect to mole fraction，\(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\right.\) ］

\section*{Notes}

This equation can be derived with SymPy，as follows
```

>>> from sympy import *
>>> i, j, k, m, n, o = symbols("i, j, k, m, n, o", cls=Idx)
>>> zs = IndexedBase('zs')
>>> Cs = IndexedBase('Cs')
>>> nc = symbols('nc')
>>> C_expr = Sum(zs[i]*zs[j]*zs[k]*\operatorname{cbrt(Cs[i,j]*Cs[i,k]*Cs[j,k]),[i,0,nc],[j,0,nc],}
\rightarrow [ k , 0 , n c ] )
>>> diff(C_expr, zs[m], zs[n])
Sum((Cs[i, j]*Cs[i, k]*Cs[j, k])**(1/3)*(KroneckerDelta(i, m)*KroneckerDelta(j, ь
n)*zs[k] + KroneckerDelta(i, m)*KroneckerDelta(k, n)*zs[j] + KroneckerDelta(i,u
๑n)*KroneckerDelta(j, m)*zs[k] + KroneckerDelta(i, n)*KroneckerDelta(k, m)*zs[j] +ь
↔KroneckerDelta(j, m)*KroneckerDelta(k, n)*zs[i] + KroneckerDelta(j,七
|n)*KroneckerDelta(k, m)*zs[i]), (i, 0, nc), (j, 0, nc), (k, 0, nc))

```

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
\mapsto12e-09, 2.996e-09, 4.927e-09]]
>>> zs = [.5, .3, .2]
>>> d2CVirial_mixture_Orentlicher_Prausnitz_dzizjs(zs, Cijs)
[[9.6827886655e-09, 1.1449146725e-08, 1.3064355337e-08], [1.1449146725e-08, 1.
\hookrightarrow38557674294e-08, 1.60903596751e-08], [1.3064355337e-08, 1.60903596751e-08, 2.
๑0702239403e-08]]

```
chemicals．virial．d3CVirial＿mixture＿Orentlicher＿Prausnitz＿dzizjzks（zs，Cijs，d3Cs＝None）
Calculate the third mole fraction derivatives of the \(C\) third virial coefficient from a matrix of virial cross－ coefficients．
\[
\frac{\partial^{3} C}{\partial z_{m} \partial z_{n} \partial z_{o}}=\sum_{\substack{0 \leq i \leq n c \\ 0 \leq \leq \leq n c \\ 0 \leq k \leq n c}} \sqrt[3]{C s_{i, j} C s_{i, k} C s_{j, k}}\left(\delta_{i m} \delta_{j n} \delta_{k o}+\delta_{i m} \delta_{j o} \delta_{k n}+\delta_{i n} \delta_{j m} \delta_{k o}+\delta_{i n} \delta_{j o} \delta_{k m}+\delta_{i o} \delta_{j m} \delta_{k n}+\delta_{i o} \delta_{j n} \delta_{k m}\right)
\]

\section*{Parameters}
zs［list［float］］Mole fractions of each species，［－］
Cijs［list［list［float］］］Third virial binary interaction coefficients in density form［ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2\right]\)
d3Cs［list［list［list［float］］］，optional］Third derivatives of C with respect to mole fraction， ［ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ］

\section*{Returns}
d3Cs［list［list［list［float］］］］Third derivatives of C with respect to mole fraction，\(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2\right]\)

\section*{Notes}

This equation can be derived with SymPy，as follows
```

>>> from sympy import *
>> i, j, k, m, n, o = symbols("i, j, k, m, n, o", cls=Idx)
>>> zs = IndexedBase('zs')
>> Cs = IndexedBase('Cs')
>>> nc = symbols('nc')
>>> C_expr = Sum(zs[i]*zs[j]*zs[k]*\operatorname{cbrt(Cs[i,j]*Cs[i,k]*Cs[j,k]),[i,0,nc],[j,0,nc],}
\leftrightarrow[k,0,nc])
>>> diff(C_expr, zs[m], zs[n], zs[o])
Sum((Cs[i, j]*Cs[i, k]*Cs[j, k])**(1/3)*(KroneckerDelta(i, m)*KroneckerDelta(j,ь
๑n)*KroneckerDelta(k, o) + KroneckerDelta(i, m)*KroneckerDelta(j,七
\rightarrow 0 ) * K r o n e c k e r D e l t a ( k , ~ n ) ~ + ~ K r o n e c k e r D e l t a ( i , ~ n ) * K r o n e c k e r D e l t a ( j , 七
\rightarrow \mathrm { m } ) * K r o n e c k e r D e l t a ( k , ~ o ) ~ + ~ K r o n e c k e r D e l t a ( i , ~ n ) * K r o n e c k e r D e l t a ( j , , ~
\rightarrow 0 ) * K r o n e c k e r D e l t a ( k , ~ m ) ~ + ~ K r o n e c k e r D e l t a ( i , ~ o ) * K r o n e c k e r D e l t a ( j , ь
\leftrightarrowm)*KroneckerDelta(k, n) + KroneckerDelta(i, o)*KroneckerDelta(j,七
n)*KroneckerDelta(k, m)), (i, 0, nc), (j, 0, nc), (k, 0, nc))

```

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
412e-09, 2.996e-09, 4.927e-09]]
>>> zs = [.5, .3, .2]
>>> d3CVirial_mixture_Orentlicher_Prausnitz_dzizjzks(zs, Cijs)
[[[8.760000000e-09, 1.0187346981e-08, 1.12329228549e-08], [1.01873469818e-08, 1.
\hookrightarrow21223973593e-08, 1.35937701316e-08], [1.12329228549e-08, 1.35937701316e-08, 1.
๑68488143533e-08]], [[1.01873469818e-08, 1.21223973593e-08, 1.35937701316e-08], [1.
\rightarrow 2 1 2 2 3 9 7 3 5 9 e - 0 8 , ~ 1 . 4 7 6 0 0 0 0 0 0 0 0 e - 0 8 , ~ 1 . 6 8 3 2 8 4 3 7 4 9 1 e - 0 8 ] , ~ [ 1 . 3 5 9 3 7 7 0 1 3 1 6 e - 0 8 , ~ 1 . ~
๑68328437491e-08, 2.12181074230e-08]], [[1.12329228549e-08, 1.35937701316e-08, 1.
๑68488143533e-08], [1.35937701316e-08, 1.68328437491e-08, 2.12181074230e-08], [1.
\leftrightarrows68488143533e-08, 2.12181074230e-08, 2.9562000000e-08]]]

```
chemicals.virial.d2CVirial_mixture_Orentlicher_Prausnitz_dTdzs(zs, Cijs, dCij_dTs, \(d 2 C \_d T d z s=\) None \()\)
Calculate the first mole fraction derivatives of the \(C\) third virial coefficient from a matrix of virial crosscoefficients.
\[
\frac{\partial^{2} C}{\partial T \partial z_{m}}
\]

\section*{Parameters}
zs [list[float]] Mole fractions of each species, [-]
Cijs [list[list[float]]] Third virial binary interaction coefficients in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dCij_dTs [list[list[float]]] First temperature derivative of third virial binary interaction coefficients in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dTdzs [list[float], optional] Array for second derivatives of C with respect to mole fraction and temperature, \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)

\section*{Returns}
d2C_dTdzs [list[float]] Second derivatives of C with respect to mole fraction and temperature, \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)

\section*{Notes}

This equation can be derived with SymPy, as follows
```

>>> from sympy import *
>>> from sympy import *
>>> i, j, k, m, n, o, T = symbols("i, j, k, m, n, o, T", cls=Idx)
>>> zs = IndexedBase('zs')
>>> Cs = IndexedBase('Cs')
>>> dC_dTs = IndexedBase('dC_dTs')
>>> nc = symbols('nc')
>>> C_expr = Sum(zs[i]*zs[j]*zs[k]/3*Cbrt(Cs[i,j]*Cs[i,k]*Cs[j,k])/CCs[i,j]*Cs[i,
\leftrightarrowk]*Cs[j,k])*(Cs[i,j]*Cs[i,k]*dC_dTs[j,k] + Cs[i,j]*dC_dTs[i,k]*Cs[j,k] + dC_dTs[i,
->j]*Cs[i,k]*Cs[j,k]),[i,0,nc],[j,0,nc],[k,0,nc])
>>> diff(C_expr, zs[m])
Sum(CCs[i, j]*Cs[i, k]*Cs[j, k])**(1/3)*(Cs[i, j]*Cs[i, k]*dC_dTs[j, k] + Cs[i,,
\hookrightarrowj]*s[j, k]*dC_dTs[i, k] + Cs[i, k]*Cs[j, k]*dC_dTs[i, j])*KroneckerDelta(i,u
๑m)*zs[j]*zs[k]/(3*Cs[i, j]*Cs[i, k]*Cs[j, k]) + (Cs[i, j]*Cs[i, k]*Cs[j, k])**(1/
G3)*(Cs[i, j]*Cs[i, k]*dC_dTs[j, k] + Cs[i, j]*Cs[j, k]*dC_dTs[i, k] (eortig|\&s,qn next page)
->k]*Cs[j, k]*dC_dTs[i, j])*KroneckerDelta(j, m)*zs[i]*zs[k]/(3*Cs[i, j]*Cs[i,七

```

```

$\rightarrow j]) * K r o n e c k e r D e l t a(k, m) * z s[i] * z s[j] /(3 * C s[i, j] * C s[i, k] * C s[j, k]),(i, 0, n c)$, ,
$\rightarrow(j, 0, n c),(k, 0, n c))$

```

\section*{Examples}
```

>>> Cijs = [[1.46e-09, 1.831e-09, 2.12e-09], [1.831e-09, 2.46e-09, 2.996e-09], [2.
@12e-09, 2.996e-09, 4.927e-09]]
>>> dCij_dTs = [[-2.212e-12, -4.137e-12, -1.079e-11], [-4.137e-12, -7.669e-12, -1.
๑09e-11], [-1.079e-11, -1.809e-11, -2.010e-11]]
>> zs = [.5, .3, .2]
>>> d2CVirial_mixture_Orentlicher_Prausnitz_dTdzs(zs, Cijs, dCij_dTs)
[-1.5740994103e-11, -2.27267309501e-11, -3.56846953115e-11]

```
chemicals.virial.dV_dzs_virial ( \(\left.B, C, V, d B \_d z s, d C \_d z s, d V \_d z s=N o n e\right)\)
Calculates first mole fraction derivative of volume for the virial equation of state.
\[
\frac{\partial V}{\partial z_{i}}=\frac{V\left(V \frac{\partial B}{\partial z_{i}}+\frac{\partial C}{\partial z_{i}}\right)}{2 B V+3 C+V^{2}}
\]

\section*{Parameters}

B [float] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
C [float] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
\(\mathbf{V}\) [float] Molar volume from virial equation, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dzs [list[float]] First mole fraction derivatives of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)
dC_dzs [list[float]] First derivatives of C with respect to mole fraction, \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\right.\) ]
dV_dzs [list[float], optional] Array for first derivatives of molar volume with respect to mole fraction, \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Returns}
dV_dzs [list[float]] First derivatives of molar volume with respect to mole fraction, [m^3/mol]

\section*{Notes}

This expression was derived with SymPy as follows:
```

>>> from sympy import *
>>> Z, R, T, P, z1 = symbols('Z, R, T, P, z1')
>>> B, C, V = symbols('B, C, V', cls=Function)
>>> base =Eq(P*V(z1)/(R*T), 1 + B(z1)/V(z1) + C(z1)/V(z1)**2)
>>> P_sln = solve(base, P) [0]
>>> solve(diff(P_sln, z1), Derivative(V(z1), z1))
[(V(z1)*Derivative(B(z1), z1) + Derivative(C(z1), z1))*V(z1)/(2*B(z1)*V(z1) +
->3*C(z1) + V(z1)**2)]

```

\section*{Examples}
```

>>> dV_dzs_virial(B=-5.130920247359858e-05, C=2.6627784284381213e-09, V=0.
๑024892080086430797, dB_dzs=[-4.457911131778849e-05, -9.174964457681726e-05, -0.
๑0001594258679841028], dC_dzs=[6.270599057032657e-09, 7.766612052069565e-09, 9.
403031492910165e-09])
[-4.4510120473455416e-05, -9.181495962913208e-05, -0.00015970040988493522]

```
chemicals.virial.d2V_dzizjs_virial( \(B, C, V, d B \_d z s, d C \_d z s, d V \_d z s, d 2 B \_d z i z j s, d 2 C \_d z i z j s\), \(d 2 V \_d z i z j s=\) None \()\)
Calculates second mole fraction derivative of volume for the virial equation of state.
\[
\frac{\partial^{2} V}{\partial z_{i} \partial z_{j}}
\]

\section*{Parameters}

B [float] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
C [float] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
\(\mathbf{V}\) [float] Molar volume from virial equation, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dzs [list[float]] First mole fraction derivatives of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)
dC_dzs [list[float]] First derivatives of \(C\) with respect to mole fraction, \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\right.\) ]
dV_dzs [list[float]] First derivatives of molar volume with respect to mole fraction, [m^3/mol]
d2B_dzizjs [list[list[float]]] Second mole fraction derivatives of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)
d2C_dzizjs [list[list[float]]] Second derivatives of \(C\) with respect to mole fraction, \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2\right]\)
d2V_dzizjs [list[list[float]], optional] Array for second derivatives of molar volume with respect to mole fraction, [m^3/mol]

\section*{Returns}
d2V_dzizjs [list[list[float]]] Second derivatives of molar volume with respect to mole fraction, [m^3/mol]

\section*{Notes}

This expression was derived with SymPy as follows:
```

>>> from sympy import *
>>> Z, R, T, P, z1 = symbols('Z, R, T, P, z1')
>>> B, C, V = symbols('B, C, V', cls=Function)
>>> base =Eq(P*V(z1)/(R*T), 1 + B(z1)/V(z1) + C(z1)/V(z1)**2)
>>> P_sln = solve(base, P)[0]
>>> solve(diff(P_sln, z1), Derivative(V(z1), z1))
[(V(z1)*Derivative(B(z1), z1) + Derivative(C(z1), z1))*V(z1)/(2*B(z1)*V(z1) +
->3*C(z1) + V(z1)**2)]

```

\section*{Examples}
```

>>> d2C_dzizjs = [[1.0287075724127612e-08, 1.2388277824773021e-08, 1.
\leftrightarrow4298813522844275e-08], [1.2388277824773021e-08, 1.514162073913238e-08, 1.
๑8282527232061114e-08], [1.4298813522844275e-08, 1.8282527232061114e-08, 2.
\hookrightarrow3350122217403063e-08]]
>>> d2B_dzizjs = [[-1.0639357784985337e-05, -3.966321845899801e-05, -7.
\hookrightarrow5987684376414e-05], [-3.966321845899801e-05, -8.286257232134107e-05, -0.
\hookrightarrow00014128571574782375], [-7.53987684376414e-05, -0.00014128571574782375, -0.
๑00024567752140887547]]
>>> dB_dzs = [-4.457911131778849e-05, -9.174964457681726e-05, -0.
@001594258679841028]
>>> dC_dzs = [6.270599057032657e-09, 7.766612052069565e-09, 9.503031492910165e-09]
>>> dV_dzs = [-4.4510120473455416e-05, -9.181495962913208e-05, -0.
๑00015970040988493522]
>>> d2V_dzizjs_virial(B=-5.130920247359858e-05, C=2.6627784284381213e-09, V=0.
\leftrightarrows024892080086430797, dB_dzs=dB_dzs, dC_dzs=dC_dzs, dV_dzs=dV_dzs, d2B_dzizjs=d2B_
\hookrightarrowdzizjs, d2C_dzizjs=d2C_dzizjs)
[[-1.04268917389e-05, -3.9654694588e-05, -7.570310078e-05], [-3.9654694588e-05, -8.
\leftrightarrows3270116767e-05, -0.0001423083584], [-7.5703100789e-05, -0.000142308358, -0.
@0024779788]]

```

\subsection*{1.34.2 Second Virial Correlations}
chemicals.virial.BVirial_Pitzer_Curl( \(T, T c, P c\), omega, order=0)
Calculates the second virial coefficient using the model in [1]. Designed for simple calculations.
\[
\begin{gathered}
B_{r}=B^{(0)}+\omega B^{(1)} \\
B^{(0)}=0.1445-0.33 / T_{r}-0.1385 / T_{r}^{2}-0.0121 / T_{r}^{3} \\
B^{(1)}=0.073+0.46 / T_{r}-0.5 / T_{r}^{2}-0.097 / T_{r}^{3}-0.0073 / T_{r}^{8}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]
order [int, optional] Order of the calculation. 0 for the calculation of B itself; for \(1 / 2 / 3\), the first/second/third derivative of B with respect to temperature; and for \(-1 /-2\), the first/second indefinite integral of B with respect to temperature. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

\section*{Returns}

B [float] Second virial coefficient in density form or its integral/derivative if specified, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) or \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge}\) order]

\section*{Notes}

Analytical models for derivatives and integrals are available for orders \(-2,-1,1,2\), and 3, all obtained with SymPy. For first temperature derivative of B:
\[
\begin{gathered}
\frac{d B^{(0)}}{d T}=\frac{33 T c}{100 T^{2}}+\frac{277 T c^{2}}{1000 T^{3}}+\frac{363 T c^{3}}{10000 T^{4}} \\
\frac{d B^{(1)}}{d T}=-\frac{23 T c}{50 T^{2}}+\frac{T c^{2}}{T^{3}}+\frac{291 T c^{3}}{1000 T^{4}}+\frac{73 T c^{8}}{1250 T^{9}}
\end{gathered}
\]

For the second temperature derivative of \(B\) :
\[
\begin{aligned}
\frac{d^{2} B^{(0)}}{d T^{2}} & =-\frac{3 T c}{5000 T^{3}}\left(1100+\frac{1385 T c}{T}+\frac{242 T c^{2}}{T^{2}}\right) \\
\frac{d^{2} B^{(1)}}{d T^{2}} & =\frac{T c}{T^{3}}\left(\frac{23}{25}-\frac{3 T c}{T}-\frac{291 T c^{2}}{250 T^{2}}-\frac{657 T c^{7}}{1250 T^{7}}\right)
\end{aligned}
\]

For the third temperature derivative of B :
\[
\begin{gathered}
\frac{d^{3} B^{(0)}}{d T^{3}}=\frac{3 T c}{500 T^{4}}\left(330+\frac{554 T c}{T}+\frac{121 T c^{2}}{T^{2}}\right) \\
\frac{d^{3} B^{(1)}}{d T^{3}}=\frac{3 T c}{T^{4}}\left(-\frac{23}{25}+\frac{4 T c}{T}+\frac{97 T c^{2}}{50 T^{2}}+\frac{219 T c^{7}}{125 T^{7}}\right)
\end{gathered}
\]

For the first indefinite integral of B:
\[
\begin{gathered}
\int B^{(0)} d T=\frac{289 T}{2000}-\frac{33 T c}{100} \ln (T)+\frac{1}{20000 T^{2}}\left(2770 T T c^{2}+121 T c^{3}\right) \\
\int B^{(1)} d T=\frac{73 T}{1000}+\frac{23 T c}{50} \ln (T)+\frac{1}{70000 T^{7}}\left(35000 T^{6} T c^{2}+3395 T^{5} T c^{3}+73 T c^{8}\right)
\end{gathered}
\]

For the second indefinite integral of B :
\[
\begin{gathered}
\iint B^{(0)} d T d T=\frac{289 T^{2}}{4000}-\frac{33 T}{100} T c \ln (T)+\frac{33 T}{100} T c+\frac{277 T c^{2}}{2000} \ln (T)-\frac{121 T c^{3}}{20000 T} \\
\iint B^{(1)} d T d T=\frac{73 T^{2}}{2000}+\frac{23 T}{50} T c \ln (T)-\frac{23 T}{50} T c+\frac{T c^{2}}{2} \ln (T)-\frac{1}{420000 T^{6}}\left(20370 T^{5} T c^{3}+73 T c^{8}\right)
\end{gathered}
\]

\section*{References}
[1]

\section*{Examples}

Example matching that in BVirial_Abbott, for isobutane.
```

>>> BVirial_Pitzer_Curl(510., 425.2, 38E5, 0.193)
-0.00020845362479301725

```
chemicals.virial.BVirial_Abbott ( \(T, T c, P c\), omega, order \(=0\) )
Calculates the second virial coefficient using the model in [1]. Simple fit to the Lee-Kesler equation.
\[
\begin{aligned}
B_{r} & =B^{(0)}+\omega B^{(1)} \\
B^{(0)} & =0.083+\frac{0.422}{T_{r}^{1.6}} \\
B^{(1)} & =0.139-\frac{0.172}{T_{r}^{4.2}}
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]
order [int, optional] Order of the calculation. 0 for the calculation of B itself; for \(1 / 2 / 3\), the first/second/third derivative of \(B\) with respect to temperature; and for \(-1 /-2\), the first/second indefinite integral of B with respect to temperature. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

\section*{Returns}

B [float] Second virial coefficient in density form or its integral/derivative if specified, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) or \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge}\) order]

\section*{Notes}

Analytical models for derivatives and integrals are available for orders \(-2,-1,1,2\), and 3, all obtained with SymPy.
For first temperature derivative of B :
\[
\begin{aligned}
\frac{d B^{(0)}}{d T} & =\frac{0.6752}{T\left(\frac{T}{T c}\right)^{1.6}} \\
\frac{d B^{(1)}}{d T} & =\frac{0.7224}{T\left(\frac{T}{T c}\right)^{4.2}}
\end{aligned}
\]

For the second temperature derivative of B:
\[
\begin{aligned}
\frac{d^{2} B^{(0)}}{d T^{2}} & =-\frac{1.75552}{T^{2}\left(\frac{T}{T c}\right)^{1.6}} \\
\frac{d^{2} B^{(1)}}{d T^{2}} & =-\frac{3.75648}{T^{2}\left(\frac{T}{T c}\right)^{4.2}}
\end{aligned}
\]

For the third temperature derivative of B:
\[
\begin{aligned}
\frac{d^{3} B^{(0)}}{d T^{3}} & =\frac{6.319872}{T^{3}\left(\frac{T}{T c}\right)^{1.6}} \\
\frac{d^{3} B^{(1)}}{d T^{3}} & =\frac{23.290176}{T^{3}\left(\frac{T}{T c}\right)^{4.2}}
\end{aligned}
\]

For the first indefinite integral of B:
\[
\begin{gathered}
\int B^{(0)} d T=0.083 T+\frac{\frac{211}{300} T c}{\left(\frac{T}{T c}\right)^{0.6}} \\
\int B^{(1)} d T=0.139 T+\frac{0.05375 T c}{\left(\frac{T}{T c}\right)^{3.2}}
\end{gathered}
\]

For the second indefinite integral of B :
\[
\begin{gathered}
\iint B^{(0)} d T d T=0.0415 T^{2}+\frac{211}{120} T c^{2}\left(\frac{T}{T c}\right)^{0.4} \\
\iint B^{(1)} d T d T=0.0695 T^{2}-\frac{\frac{43}{1760} T c^{2}}{\left(\frac{T}{T c}\right)^{2.2}}
\end{gathered}
\]

\section*{References}
[1]

\section*{Examples}

Example is from [1], p. 93, and matches the result exactly, for isobutane.
```

>>> BVirial_Abbott(510., 425.2, 38E5, 0.193)
-0.000205701850095

```
chemicals.virial.BVirial_Tsonopoulos(T, Tc, Pc, omega, order=0)
Calculates the second virial coefficient using the model in [1].
\[
\begin{gathered}
B_{r}=B^{(0)}+\omega B^{(1)} \\
B^{(0)}=0.1445-0.330 / T_{r}-0.1385 / T_{r}^{2}-0.0121 / T_{r}^{3}-0.000607 / T_{r}^{8} \\
B^{(1)}=0.0637+0.331 / T_{r}^{2}-0.423 / T_{r}^{3}-0.423 / T_{r}^{3}-0.008 / T_{r}^{8}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]
order [int, optional] Order of the calculation. 0 for the calculation of B itself; for \(1 / 2 / 3\), the first/second/third derivative of B with respect to temperature; and for \(-1 /-2\), the first/second indefinite integral of B with respect to temperature. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

\section*{Returns}

B [float] Second virial coefficient in density form or its integral/derivative if specified, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) or \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge}\) order]

\section*{Notes}

A more complete expression is also available, in BVirial_Tsonopoulos_extended.
Analytical models for derivatives and integrals are available for orders \(-2,-1,1,2\), and 3, all obtained with SymPy.
For first temperature derivative of B:
\[
\begin{gathered}
\frac{d B^{(0)}}{d T}=\frac{33 T c}{100 T^{2}}+\frac{277 T c^{2}}{1000 T^{3}}+\frac{363 T c^{3}}{10000 T^{4}}+\frac{607 T c^{8}}{125000 T^{9}} \\
\frac{d B^{(1)}}{d T}=-\frac{331 T c^{2}}{500 T^{3}}+\frac{1269 T c^{3}}{1000 T^{4}}+\frac{8 T c^{8}}{125 T^{9}}
\end{gathered}
\]

For the second temperature derivative of B:
\[
\begin{gathered}
\frac{d^{2} B^{(0)}}{d T^{2}}=-\frac{3 T c}{125000 T^{3}}\left(27500+\frac{34625 T c}{T}+\frac{6050 T c^{2}}{T^{2}}+\frac{1821 T c^{7}}{T^{7}}\right) \\
\frac{d^{2} B^{(1)}}{d T^{2}}=\frac{3 T c^{2}}{500 T^{4}}\left(331-\frac{846 T c}{T}-\frac{96 T c^{6}}{T^{6}}\right)
\end{gathered}
\]

For the third temperature derivative of B :
\[
\begin{gathered}
\frac{d^{3} B^{(0)}}{d T^{3}}=\frac{3 T c}{12500 T^{4}}\left(8250+\frac{13850 T c}{T}+\frac{3025 T c^{2}}{T^{2}}+\frac{1821 T c^{7}}{T^{7}}\right) \\
\frac{d^{3} B^{(1)}}{d T^{3}}=\frac{3 T c^{2}}{250 T^{5}}\left(-662+\frac{2115 T c}{T}+\frac{480 T c^{6}}{T^{6}}\right)
\end{gathered}
\]

For the first indefinite integral of B:
\[
\begin{gathered}
\int B^{(0)} d T=\frac{289 T}{2000}-\frac{33 T c}{100} \ln (T)+\frac{1}{7000000 T^{7}}\left(969500 T^{6} T c^{2}+42350 T^{5} T c^{3}+607 T c^{8}\right) \\
\int B^{(1)} d T=\frac{637 T}{10000}-\frac{1}{70000 T^{7}}\left(23170 T^{6} T c^{2}-14805 T^{5} T c^{3}-80 T c^{8}\right)
\end{gathered}
\]

For the second indefinite integral of B :
\[
\begin{gathered}
\iint B^{(0)} d T d T=\frac{289 T^{2}}{4000}-\frac{33 T}{100} T c \ln (T)+\frac{33 T}{100} T c+\frac{277 T c^{2}}{2000} \ln (T)-\frac{1}{42000000 T^{6}}\left(254100 T^{5} T c^{3}+607 T c^{8}\right) \\
\iint B^{(1)} d T d T=\frac{637 T^{2}}{20000}-\frac{331 T c^{2}}{1000} \ln (T)-\frac{1}{210000 T^{6}}\left(44415 T^{5} T c^{3}+40 T c^{8}\right)
\end{gathered}
\]

\section*{References}
[1]

\section*{Examples}

Example matching that in BVirial_Abbott, for isobutane.
```

>>> BVirial_Tsonopoulos(510., 425.2, 38E5, 0.193)
-0.0002093529540

```
chemicals.virial.BVirial_Tsonopoulos_extended \((T, T c, P c\), omega, \(a=0, b=0\), species_type=", dipole \(=0\), order=0)
Calculates the second virial coefficient using the comprehensive model in [1]. See the notes for the calculation of \(a\) and \(b\).
\[
\begin{gathered}
\frac{B P_{c}}{R T_{c}}=B^{(0)}+\omega B^{(1)}+a B^{(2)}+b B^{(3)} \\
B^{(0)}=0.1445-0.33 / T_{r}-0.1385 / T_{r}^{2}-0.0121 / T_{r}^{3} \\
B^{(1)}=0.0637+0.331 / T_{r}^{2}-0.423 / T_{r}^{3}-0.423 / T_{r}^{3}-0.008 / T_{r}^{8} \\
B^{(2)}=1 / T_{r}^{6} \\
B^{(3)}=-1 / T_{r}^{8}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]
a [float, optional] Fit parameter, calculated based on species_type if a is not given and species_type matches on of the supported chemical classes.
b [float, optional] Fit parameter, calculated based on species_type if a is not given and species_type matches on of the supported chemical classes.
species_type [str, optional] One of .
dipole [float] dipole moment, optional, [Debye]
order [int, optional] Order of the calculation. 0 for the calculation of B itself; for \(1 / 2 / 3\), the first/second/third derivative of \(B\) with respect to temperature; and for \(-1 /-2\), the first/second indefinite integral of B with respect to temperature. No other integrals or derivatives are implemented, and an exception will be raised if any other order is given.

\section*{Returns}

B [float] Second virial coefficient in density form or its integral/derivative if specified, \([\mathrm{m} \wedge 3 / \mathrm{mol}\) or \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge}\) order]

\section*{Notes}

Analytical models for derivatives and integrals are available for orders \(-2,-1,1,2\), and 3, all obtained with SymPy.
To calculate \(a\) or \(b\), the following rules are used:
For 'simple' or 'normal' fluids:
\[
\begin{aligned}
& a=0 \\
& b=0
\end{aligned}
\]

For 'ketone', 'aldehyde', 'alkyl nitrile', 'ether', 'carboxylic acid', or 'ester' types of chemicals:
\[
\begin{gathered}
a=-2.14 \times 10^{-4} \mu_{r}-4.308 \times 10^{-21}\left(\mu_{r}\right)^{8} \\
b=0
\end{gathered}
\]

For 'alkyl halide', 'mercaptan', 'sulfide', or 'disulfide' types of chemicals:
\[
\begin{gathered}
a=-2.188 \times 10^{-4}\left(\mu_{r}\right)^{4}-7.831 \times 10^{-21}\left(\mu_{r}\right)^{8} \\
b=0
\end{gathered}
\]

For 'alkanol' types of chemicals (except methanol):
\[
\begin{gathered}
a=0.0878 \\
b=0.00908+0.0006957 \mu_{r}
\end{gathered}
\]

For methanol:
\[
\begin{aligned}
& a=0.0878 \\
& b=0.0525
\end{aligned}
\]

For water:
\[
\begin{gathered}
a=-0.0109 \\
b=0
\end{gathered}
\]

If required, the form of dipole moment used in the calculation of some types of \(a\) and \(b\) values is as follows:
\[
\mu_{r}=100000 \frac{\mu^{2}(P c / 101325.0)}{T c^{2}}
\]

For first temperature derivative of B :
\[
\begin{gathered}
\frac{d B^{(0)}}{d T}=\frac{33 T c}{100 T^{2}}+\frac{277 T c^{2}}{1000 T^{3}}+\frac{363 T c^{3}}{10000 T^{4}}+\frac{607 T c^{8}}{125000 T^{9}} \\
\frac{d B^{(1)}}{d T}=-\frac{331 T c^{2}}{500 T^{3}}+\frac{1269 T c^{3}}{1000 T^{4}}+\frac{8 T c^{8}}{125 T^{9}} \\
\frac{d B^{(2)}}{d T}=-\frac{6 T c^{6}}{T^{7}} \\
\frac{d B^{(3)}}{d T}=\frac{8 T c^{8}}{T^{9}}
\end{gathered}
\]

For the second temperature derivative of B:
\[
\begin{aligned}
& \frac{d^{2} B^{(0)}}{d T^{2}}=-\frac{3 T c}{125000 T^{3}}\left(27500+\frac{34625 T c}{T}+\frac{6050 T c^{2}}{T^{2}}+\frac{1821 T c^{7}}{T^{7}}\right) \\
& \frac{d^{2} B^{(1)}}{d T^{2}}=\frac{3 T c^{2}}{500 T^{4}}\left(331-\frac{846 T c}{T}-\frac{96 T c^{6}}{T^{6}}\right) \\
& \frac{d^{2} B^{(2)}}{d T^{2}}=\frac{42 T c^{6}}{T^{8}} \\
& \frac{d^{2} B^{(3)}}{d T^{2}}=-\frac{72 T c^{8}}{T^{10}}
\end{aligned}
\]

For the third temperature derivative of B :
\[
\frac{d^{3} B^{(0)}}{d T^{3}}=\frac{3 T c}{12500 T^{4}}\left(8250+\frac{13850 T c}{T}+\frac{3025 T c^{2}}{T^{2}}+\frac{1821 T c^{7}}{T^{7}}\right)
\]
\[
\begin{gathered}
\frac{d^{3} B^{(1)}}{d T^{3}}=\frac{3 T c^{2}}{250 T^{5}}\left(-662+\frac{2115 T c}{T}+\frac{480 T c^{6}}{T^{6}}\right) \\
\frac{d^{3} B^{(2)}}{d T^{3}}=-\frac{336 T c^{6}}{T^{9}} \\
\frac{d^{3} B^{(3)}}{d T^{3}}=\frac{720 T c^{8}}{T^{11}}
\end{gathered}
\]

For the first indefinite integral of B :
\[
\begin{gathered}
\int B^{(0)} d T=\frac{289 T}{2000}-\frac{33 T c}{100} \ln (T)+\frac{1}{7000000 T^{7}}\left(969500 T^{6} T c^{2}+42350 T^{5} T c^{3}+607 T c^{8}\right) \\
\int B^{(1)} d T=\frac{637 T}{10000}-\frac{1}{70000 T^{7}}\left(23170 T^{6} T c^{2}-14805 T^{5} T c^{3}-80 T c^{8}\right) \\
\int B^{(2)} d T=-\frac{T c^{6}}{5 T^{5}} \\
\int B^{(3)} d T=\frac{T c^{8}}{7 T^{7}}
\end{gathered}
\]

For the second indefinite integral of B:
\[
\begin{gathered}
\iint B^{(0)} d T d T=\frac{289 T^{2}}{4000}-\frac{33 T}{100} T c \ln (T)+\frac{33 T}{100} T c+\frac{277 T c^{2}}{2000} \ln (T)-\frac{1}{42000000 T^{6}}\left(254100 T^{5} T c^{3}+607 T c^{8}\right) \\
\iint B^{(1)} d T d T=\frac{637 T^{2}}{20000}-\frac{331 T c^{2}}{1000} \ln (T)-\frac{1}{210000 T^{6}}\left(44415 T^{5} T c^{3}+40 T c^{8}\right) \\
\iint B^{(2)} d T d T=\frac{T c^{6}}{20 T^{4}} \\
\iint B^{(3)} d T d T=-\frac{T c^{8}}{42 T^{6}}
\end{gathered}
\]

\section*{References}
[1], [2]

\section*{Examples}

Example from Perry's Handbook, 8E, p2-499. Matches to a decimal place.
```

>>> BVirial_Tsonopoulos_extended(430., 405.65, 11.28E6, 0.252608, a=0, b=0, species_
->type='ketone', dipole=1.469)
-9.679718337596e-05

```

New implementations, returning the derivatives as well
chemicals.virial.BVirial_Pitzer_Curl_fast(T, Tc, Pc, omega)
Implementation of BVirial_Pitzer_Curl in the interface which calculates virial coefficients and their derivatives at the same time.

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]

Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

B [float] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\) ]
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Examples}
>>> BVirial_Pitzer_Curl_fast(510., 425.2, 38E5, 0.193)
(-0.000208453624, 1.065377516e-06, -5.7957101e-09, 4.513533043e-11)

\section*{chemicals.virial.BVirial_Abbott_fast( \(T, T c, P c\), omega)}

Implementation of BVirial_Abbott in the interface which calculates virial coefficients and their derivatives at the same time.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

B [float] Second virial coefficient in density form [m^3/mol]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Examples}
>>> BVirial_Abbott_fast(510., 425.2, 38E5, 0.193)
(-0.0002057018500, 1.039249294e-06, -5.902233639e-09, 4.78222764e-11)

\section*{chemicals.virial.BVirial_Tsonopoulos_fast( \(T, T c, P c\), omega)}

Implementation of BVirial_Tsonopoulos in the interface which calculates virial coefficients and their derivatives at the same time.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]

Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

B [float] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\) ]
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Examples}
>>> BVirial_Tsonopoulos_fast(510., 425.2, 38E5, 0.193)
(-0.0002093529540, 9.95742355e-07, -5.54234465e-09, 4.57035160e-11)
chemicals.virial.BVirial_Tsonopoulos_extended_fast (T, Tc, Pc, omega, \(a=0.0, b=0.0\) )
Implementation of BVirial_Tsonopoulos_extended in the interface which calculates virial coefficients and their derivatives at the same time.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]
a [float, optional] Fit parameter [-]
b [float, optional] Fit parameter [-]

\section*{Returns}

B [float] Second virial coefficient in density form [m^3/mol]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Examples}
>>> BVirial_Tsonopoulos_extended_fast(510., 425.2, 38E5, 0.193)
(-0.0002093529540, 9.9574235e-07, -5.54234465e-09, 4.5703516e-11)

\section*{chemicals.virial.BVirial_Oconnell_Prausnitz(T,Tc, Pc, omega)}

Calculates the second virial coefficient using the model in [1].
\[
\begin{gathered}
B_{r}=B^{(0)}+\omega B^{(1)} \\
B^{(0)}=c 0+\frac{c 1}{T_{r}}+\frac{c 2}{T_{r}^{2}}+\frac{c 3}{T_{r}^{3}} \\
B^{(1)}=d 0+\frac{d 1}{T_{r}^{2}}+\frac{d 2}{T_{r}^{3}}+\frac{d 3}{T_{r}^{8}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

B [float] Second virial coefficient in density form [m^3/mol]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Notes}

The coefficients are as follows:
\(\mathrm{c} 0=0.1445 \mathrm{c} 1=-0.330 \mathrm{c} 2=-0.1385 \mathrm{c} 3=-0.0121\)
\(\mathrm{d} 0=0.073 \mathrm{~d} 1=0.46 \mathrm{~d} 2=-0.50 \mathrm{~d} 3=-0.097 \mathrm{~d} 4=-0.0073\)

\section*{References}
[1]

\section*{Examples}
>>> BVirial_Oconnell_Prausnitz(510., 425.2, 38E5, 0.193)
(-0.000203193781, 1.036185972e-06, -6.53679132e-09, 6.59478287e-11)
chemicals.virial.BVirial_Xiang ( \(T, T c, P c, V c\), omega)
Calculates the second virial coefficient using the model in [1].
\[
\begin{gathered}
B={\frac{\left.\left(-b_{0} T_{r}^{-3 / 4} \exp \left(b_{1} T_{r}^{-3}\right)+b_{2} T_{r}^{-1 / 2}\right)\right)}{V}}_{c} \\
b_{0}=b_{00}+b_{01} \omega+b_{02} \theta \\
b_{1}=b_{10}+b_{11} \omega+b_{12} \theta \\
b_{2}=b_{20}+b_{21} \omega+b_{22} \theta \\
\theta=\left(Z_{c}-0.29\right)^{2}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
Vc [float] Critical volume of the fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

B [float] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\) ]

\section*{References}
[1]

\section*{Examples}
>>> BVirial_Xiang(388.26, 647.1, 22050000.0, 5.543076e-05, 0.344)
(-0.0004799570, 4.6778266e-06, -7.0157656e-08, 1.4137862e-09)
chemicals.virial.BVirial_Meng( \(T, T c, P c, V c\), omega, \(a=0.0\) )
Calculates the second virial coefficient using the model in [1].
\[
B=\frac{R T_{c}}{P_{c}}\left(f_{0}+\omega f_{1}+f_{2}\right)
\]
\[
\begin{gathered}
f_{0}=c_{0}+c_{1} / T_{r}+c_{2} / T_{r}^{2}+c_{3} / T_{r}^{3}+c_{4} / T_{r}^{8} \\
f_{1}=d_{0}+d_{1} / T_{r}+d_{2} / T_{r}^{2}+d_{3} / T_{r}^{3}+d_{4} / T_{r}^{8} \\
f_{2}=\frac{a}{T_{r}^{6}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
Vc [float] Critical volume of the fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omega [float] Acentric factor for fluid, [-]
a [float] Polar parameter that can be estimated by chemicals.virial.Meng_virial_a

\section*{Returns}

B [float] Second virial coefficient in density form [m^3/mol]
dB_dT [float] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2 [float] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3 [float] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{References}
[1]

\section*{Examples}
>>> BVirial_Meng(388.26, 647.1, 22050000.0, 5.543076e-05, 0.344)
(-0.00032436028, 2.47004e-06, -3.132e-08, 5.8e-10)
chemicals.virial.Meng_virial_a(Tc, Pc, dipole \(=0.0\), haloalkane=False)
Calculate the \(a\) parameter which is used in the Meng \(B\) second virial coefficient for polar components. There are two correlations implemented - one for haloalkanes, and another for other polar molecules. If the dipole moment is not provided, a value of 0.0 will be returned.

If the compound is a haloalkane
\[
a=-1.1524 \times 10^{-6} \mu_{r}^{2}+7.2238 \times 10^{-11} \mu_{r}^{4}-1.8701 \times 10^{-15} \mu_{r}^{6}
\]

Otherwise
\[
a=-3.0309 \times 10^{-6} \mu_{r}^{2}+9.503 \times 10^{-11} \mu_{r}^{4}-1.2469 \times 10^{-15} \mu_{r}^{6}
\]

\section*{Parameters}

Tc [float] Critical temperature, [K]
Pc [float] Critical pressure, [Pa]
dipole [float] Dipole moment, [debye]
haloalkane [bool] Whether or not the compound is a haloalkane, [-]

\section*{Returns}
a [float] Coefficient [-]

\section*{References}

\section*{[1]}

\section*{Examples}

Ethanol
```

>>> Meng_virial_a(514.0, 6137000.0, 1.44, haloalkane=False)
-0.00637841

```

R-41 Fluoromethane
```

>>> Meng_virial_a(317.4, 5870000.0, 1.85, haloalkane=True)

```
-0.04493829

\subsection*{1.34.3 Third Virial Correlations}
chemicals.virial.CVirial_Orbey_Vera (T, Tc, Pc, omega)
Calculates the third virial coefficient using the model in [1].
\[
\begin{gathered}
C=\left(R T_{c} / P_{c}\right)^{2}\left(f C_{T r}^{(0)}+\omega f C_{T r}^{(1)}\right) \\
f C_{T r}^{(0)}=0.01407+0.02432 T_{r}^{-2.8}-0.00313 T_{r}^{-10.5} \\
f C_{T r}^{(1)}=-0.02676+0.01770 T_{r}^{-2.8}+0.040 T_{r}^{-3}-0.003 T_{r}^{-6}-0.00228 T_{r}^{-10.5}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
\(\mathbf{C}\) [float] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dC_dT [float] First temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2 [float] Second temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3 [float] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{References}
[1]

\section*{Examples}
n-octane
>>> CVirial_Orbey_Vera(T=300, Tc=568.7, Pc=2490000.0, omega=0.394)
( \(-1.1107124 \mathrm{e}-05,4.1326808 \mathrm{e}-07,-1.6041435 \mathrm{e}-08,6.7035158 \mathrm{e}-10\) )
chemicals.virial.CVirial_Liu_Xiang ( \(T, T c, P c, V c\), omega)
Calculates the third virial coefficient using the model in [1].
\[
\begin{gathered}
C=V_{c}^{2}\left(f_{T_{r}}^{(0)}+\omega f_{T_{r}}^{(1)}+\theta f_{T_{r}}^{(2)}\right) \\
f_{T_{r}}^{(0)}=a_{00}+a_{10} T_{r}^{-3}+a_{20} T_{r}^{-6}+a_{30} T_{r}^{-11} \\
f_{T_{r}}^{(1)}=a_{01}+a_{11} T_{r}^{-3}+a_{21} T_{r}^{-6}+a_{31} T_{r}^{-11} \\
f_{T_{r}}^{(2)}=a_{02}+a_{12} T_{r}^{-3}+a_{22} T_{r}^{-6}+a_{32} T_{r}^{-11} \\
\theta=\left(Z_{c}-0.29\right)^{2}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
Vc [float] Critical volume of the fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}
\(C\) [float] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dC_dT [float] First temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2 [float] Second temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3 [float] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{References}
[1]

\section*{Examples}

Water at \(\mathrm{Tr}=0.6\)
>>> CVirial_Liu_Xiang(388.26, 647.1, 22050000.0, 5.543076923076923e-05, 0.344)
(-1.4779977e-07, 4.9949901e-09, -1.652899e-10, 5.720067e-12)

\subsection*{1.34.4 Cross-Parameters}
chemicals.virial.Tarakad_Danner_virial_CSP_kijs(Vcs)
Calculates a binary interaction parameter for the calculation of Bij binary virial coefficient as shown in [1] and [2].

This equation for kij is:
\[
k_{i j}=1-\frac{8 \sqrt{v_{c i} v_{c j}}}{\left(V_{c i}^{1 / 3}+V_{c i}^{1 / 3}\right)^{3}}
\]

The equation this kij is used in is
\[
T_{c i j}=\sqrt{T_{c i} T_{c j}}\left(1-k_{i j}\right)
\]

\section*{Parameters}

Ves [list[float]] Critical volumes for each species, [m^3/mol]

\section*{Returns}
kijs [list[list[float]]] Binary interaction parameters, [-]

\section*{References}
[1], [2]

\section*{Examples}
>>> Tarakad_Danner_virial_CSP_kijs(Vcs=[0.000168, 0.000316])
[[0.0, 0.01646332091], [0.0164633209, 0.0]]

\section*{chemicals.virial.Tarakad_Danner_virial_CSP_Tcijs(Tcs, kijs)}

Calculates the corresponding states critical temperature for the calculation of Bij binary virial coefficient as shown in [1] and [2].
\[
T_{c i j}=\sqrt{T_{c i} T_{c j}}\left(1-k_{i j}\right)
\]

\section*{Parameters}

Tcs [list[float]] Critical temperatures for each species, [K]
kijs [list[list[float]]] Binary interaction parameters, [-]

\section*{Returns}

Tcijs [list[list[float]]] CSP Critical temperatures for each pair of species, [K]

\section*{References}
[1], [2]

\section*{Examples}
>>> kijs = Tarakad_Danner_virial_CSP_kijs(Vcs=[0.000168, 0.000316])
>>> Tarakad_Danner_virial_CSP_Tcijs(Tcs=[514.0, 591.75], kijs=kijs) [[514.0, 542.42694], [542.42694, 591.75000]]

\section*{chemicals.virial.Tarakad_Danner_virial_CSP_Pcijs(Tcs, Pcs, Vcs, Tcijs)}

Calculates the corresponding states critical pressure for the calculation of Bij binary virial coefficient as shown in [1] and [2].
\[
P_{c i j}=\frac{4 T_{c i j}\left(\frac{P_{c i} V_{c i}}{T_{c i}}+\frac{P_{c j} V_{c j}}{T_{c j}}\right)}{\left(V_{c i}^{1 / 3}+V_{c i}^{1 / 3}\right)^{3}}
\]

\section*{Parameters}

Tcs [list[float]] Critical temperatures for each species, [K]
Pcs [list[float]] Critical pressures for each species, [Pa]
Ves [list[float]] Critical volumes for each species, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
Tcijs [list[list[float]]] CSP Critical temperatures for each pair of species, [K]

\section*{Returns}

Pcijs [list[list[float]]] CSP Critical pressures for each pair of species, [Pa]

\section*{References}
[1], [2]

\section*{Examples}
```

>>> kijs = Tarakad_Danner_virial_CSP_kijs(Vcs=[0.000168, 0.000316])
>>> Tcijs = Tarakad_Danner_virial_CSP_Tcijs(Tcs=[514.0, 591.75], kijs=kijs)
>>> Tarakad_Danner_virial_CSP_Pcijs(Tcs=[514.0, 591.75], Pcs=[6137000.0, 4108000.0],
Vcs=[0.000168, 0.000316], Tcijs=Tcijs)
[[6136999.9, 4861936.4], [4861936.4, 4107999.9]]

```

\section*{chemicals.virial.Tarakad_Danner_virial_CSP_omegaijs(omegas)}

Calculates the corresponding states acentric factor for the calculation of Bij binary virial coefficient as shown in [1] and [2].
\[
\omega_{i j}=0.5\left(\omega_{i}+\omega_{j}\right)
\]

\section*{Parameters}
omegas [list[float]] Acentric factor for each species, [-]

\section*{Returns}
omegaijs [list[list[float]]] CSP acentric factors for each pair of species, [-]

\section*{References}
[1], [2]

\section*{Examples}
>>> Tarakad_Danner_virial_CSP_omegaijs([0.635, 0.257])
[[0.635, 0.446], [0.446, 0.257]]

\section*{chemicals.virial.Lee_Kesler_virial_CSP_Vcijs(Vcs)}

Calculates the corresponding states critical volumes for the calculation of Vcijs binary virial coefficient as shown in [1] and [2].
\[
V_{c i j}=\frac{1}{8}\left(V_{c, i}^{1 / 3}+V_{c, j}^{1 / 3}\right)^{3}
\]

\section*{Parameters}

Vcs [list[float]] Critical volume of the fluids [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}

Vcijs [list[list[float]]] CSP critical volumes for each pair of species, [m^3/mol]

\section*{Notes}
[1] cites this as Lee-Kesler rules.

\section*{References}
[1], [2]

\section*{Examples}
>>> Lee_Kesler_virial_CSP_Vcijs(Vcs=[0.000168, 0.000316])
[[0.000168, 0.00023426], [0.000234265, 0.000316]]

\section*{chemicals.virial.Meng_Duan_2005_virial_CSP_kijs(CASs, atomss)}

Calculates a binary interaction parameter for the calculation of Bij binary virial coefficient as shown in [1]. This implements a correlation of alkane-alkane, CO2-alkane, and N2-alkane.
The equation this kij is used in is
\[
T_{c i j}=\sqrt{T_{c i} T_{c j}}\left(1-k_{i j}\right)
\]

\section*{Parameters}

CASs [list[str]] CAS registration numbers for each component, [-]
atomss [list[dict]] Breakdown of each component into its elements and their counts, as a dict, [-]

\section*{Returns}
kijs [list[list[float]]] Binary interaction parameters, [-]

\section*{References}
[1]

\section*{Examples}
```

>>> CASs = ['74-82-8', '74-84-0', '124-38-9', '7727-37-9', '7439-89-6']
>> atomss = [{'C': 1, 'H': 4}, {'C': 2, 'H': 6}, {'C': 1, 'O': 2}, {'N': 2}, {'Fe':
-> 1}]
>>> kijs = Meng_Duan_2005_virial_CSP_kijs(CASs=CASs, atomss=atomss)

```

\subsection*{1.34.5 Second Virial Correlations Dense Implementations}
chemicals.virial.BVirial_Xiang_vec \(\left(T, T c s, P c s, V c s\right.\), omegas, \(B s=N o n e, d B \_d T s=N o n e, d 2 B \_d T 2 s=N o n e\), \(d 3 B \_d T 3 s=\) None \()\)
Perform a vectorized calculation of the Xiang B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
Ves [list[float]] Critical volume of the fluids [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omegas [list[float]] Acentric factor for fluids, [-]
Bs [list[float], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\mathrm{m} \wedge 3 / \mathrm{mol} / \mathrm{K}\) ]
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\) ]
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Xiang_mat( \(T, T c s, P c s, V c s\), omegas, \(B s=N o n e, d B \_d T s=N o n e, d 2 B \_d T 2 s=N o n e\), \(d 3 B \_d T 3 s=\) None)
Perform a matrix calculation of the Xiang B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]

Tes [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
Ves [list[list[float]]] Critical volume of the fluids [m^3/mol]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form [m^3/mol/K^3]

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Pitzer_Curl_vec(T,Tcs, Pcs,omegas, \(B s=N o n e, d B \_d T s=N o n e\), \(d 2 B \_d T 2 s=\) None, \(d 3 B \_d T 3 s=\) None \()\)
Perform a vectorized calculation of the Pitzer-Curl B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
omegas [list[float]] Acentric factor for fluids, [-]
Bs [list[float], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\) ]
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\) ]
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Pitzer_Curl_mat(T,Tcs, Pcs,omegas, Bs=None, \(d B \_d T s=N o n e\), \(d 2 B \_d T 2 s=\) None, \(d 3 B \_d T 3 s=\) None \()\)
Perform a matrix calculation of the Pitzer-Curl B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form [m^3/mol/K^3]

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Abbott_vec \(\left(T, T c s, P c s\right.\), omegas, \(B s=N o n e, d B \_d T s=N o n e, d 2 B \_d T 2 s=N o n e\), \(d 3 B \_d T 3 s=\) None)
Perform a vectorized calculation of the Abbott B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
omegas [list[float]] Acentric factor for fluids, [-]
Bs [list[float], optional] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\) ]
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Abbott_mat(T,Tcs, Pcs, omegas, \(B s=N o n e, d B \_d T s=N o n e, d 2 B \_d T 2 s=N o n e\), \(d 3 B \_d T 3 s=\) None)
Perform a matrix calculation of the Abbott B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\) ]
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Tsonopoulos_vec (T, Tcs, Pcs, omegas, \(B s=N o n e, d B \_d T s=\) None, \(d 2 B \_d T 2 s=\) None, \(d 3 B \_d T 3 s=\) None \()\)
Perform a vectorized calculation of the Tsonopoulos B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
omegas [list[float]] Acentric factor for fluids, [-]
Bs [list[float], optional] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
\[
\begin{array}{r}
\text { chemicals.virial.BVirial_Tsonopoulos_mat }\left(T, T c s, P c s, \text { omegas, } B s=N o n e, d B \_d T s=N o n e,\right. \\
\left.\qquad d 2 B \_d T 2 s=N o n e, d 3 B \_d T 3 s=N o n e\right)
\end{array}
\]

Perform a matrix calculation of the Tsonopoulos B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Meng_vec ( \(T, T c s, P c s, V c s\), omegas, ais, \(B s=N o n e, d B \_d T s=\) None, \(d 2 B \_d T 2 s=\) None,\(d 3 B \_d T 3 s=\) None \()\)
Perform a vectorized calculation of the Meng B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
Ves [list[float]] Critical volume of the fluids [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omegas [list[float]] Acentric factor for fluids, [-]
ais [list[float]] Polar parameters that can be estimated by chemicals.virial. Meng_virial_a

Bs [list[float], optional] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\) ]
chemicals.virial.BVirial_Meng_mat ( \(T, T c s, P c s, V c s\), omegas, ais, Bs=None, \(d B \_d T s=\) None, \(d 2 B \_d T 2 s=\) None, \(d 3 B \_d T 3 s=\) None)
Perform a matrix calculation of the Meng B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
Ves [list[list[float]]] Critical volume of the fluids [m^3/mol]
omegas [list[list[float]]] Acentric factor for fluids, [-]
ais [list[float]] Polar parameters that can be estimated as the average of the pure component values predicted by chemicals.virial.Meng_virial_a

Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Oconnell_Prausnitz_vec (T,Tcs, Pcs, omegas, Bs=None, \(d B \_d T s=N o n e\), \(d 2 B \_d T 2 s=\) None, \(d 3 B \_d T 3 s=\) None \()\)
Perform a vectorized calculation of the O'connell Prausnitz B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
omegas [list[float]] Acentric factor for fluids, [-]
Bs [list[float], optional] Second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\) ]
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\) ]
chemicals.virial.BVirial_Oconnell_Prausnitz_mat(T,Tcs, Pcs, omegas, Bs=None, \(d B \_d T s=N o n e\), \(d 2 B \_d T 2 s=\) None,\(d 3 B \_d T 3 s=\) None \()\)
Perform a matrix calculation of the Oconnell_Prausnitz B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]

Tes [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Tsonopoulos_extended_vec(T, Tcs, Pcs, omegas, ais, \(b s, B s=N o n e\), \(d B \_d T s=\) None, \(d 2 B \_d T 2 s=\) None, \(d 3 B \_d T 3 s=\) None)
Perform a vectorized calculation of the Tsonopoulos (extended) B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
omegas [list[float]] Acentric factor for fluids, [-]
ais [list[float]] Fit parameters, [-]
bs [list[float]] Fit parameters, [-]
Bs [list[float], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[float]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[float]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[float]] Second temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[float]] Third temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.BVirial_Tsonopoulos_extended_mat (T, Tcs, Pcs,omegas, ais, bs, Bs=None, \(d B \_d T s=N o n e, d 2 B \_d T 2 s=N o n e\), \(d 3 B \_d T 3 s=\) None \()\)
Perform a matrix calculation of the Tsonopoulos (extended) B virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
omegas [list[list[float]]] Acentric factor for fluids, [-]
ais [list[list[float]]] Fit parameters, [-]
bs [list[list[float]]] Fit parameters, [-]
Bs [list[list[float]], optional] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]], optional] First temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]], optional] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]], optional] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Bs [list[list[float]]] Second virial coefficient in density form [m^3/mol]
dB_dTs [list[list[float]]] First temperature derivative of second virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}\right]\)
d2B_dT2s [list[list[float]]] Second temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 2\right]\)
d3B_dT3s [list[list[float]]] Third temperature derivative of second virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol} / \mathrm{K}^{\wedge} 3\right]\)

\subsection*{1.34.6 Third Virial Correlations Dense Implementations}
chemicals.virial.CVirial_Liu_Xiang_vec (T,Tcs, Pcs, Vcs, omegas, Cs=None, \(d C \_d T s=\) None, \(d 2 C \_d T 2 s=\) None, \(d 3 C \_d T 3 s=\) None)
Perform a vectorized calculation of the Xiang C virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
Ves [list[float]] Critical volume of the fluids [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omegas [list[float]] Acentric factor for fluids, [-]
Cs [list[float], optional] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}{ }^{\wedge} 2\) ]
dC_dTs [list[float], optional] First temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[float], optional] Second temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[float], optional] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Cs [list[float]] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dC_dTs [list[float]] First temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[float]] Second temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[float]] Third temperature derivative of third virial coefficient in density form [m^6/mol^2/K^3]
chemicals.virial.CVirial_Orbey_Vera_vec (T, Tcs, Pcs, omegas, \(C s=\) None, \(d C \_d T s=\) None, \(d 2 C_{-} d T 2 s=\) None, \(d 3 C \_d T 3 s=\) None)
Perform a vectorized calculation of the Orbey-Vera C virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[float]] Critical temperature of fluids [K]
Pcs [list[float]] Critical pressure of the fluids [Pa]
omegas [list[float]] Acentric factor for fluids, [-]
Cs [list[float], optional] Third virial coefficient in density form [m^6/mol^2]
dC_dTs [list[float], optional] First temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[float], optional] Second temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[float], optional] Third temperature derivative of third virial coefficient in density form \(\left[m^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Cs [list[float]] Third virial coefficient in density form [m^6/mol \(\left.{ }^{\wedge} 2\right]\)
dC_dTs [list[float]] First temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[float]] Second temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[float]] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)
chemicals.virial.CVirial_Liu_Xiang_mat( \(T, T c s, P c s, V c s\), omegas, \(C s=N o n e, d C \_d T s=N o n e\), \(d 2 C \_d T 2 s=\) None, \(d 3 C \_d T 3 s=\) None \()\)
Perform a matrix calculation of the Xiang \(C\) virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tcs [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
Ves [list[list[float]]] Critical volume of the fluids [m^3/mol]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Cs [list[list[float]], optional] Third virial coefficient in density form [m^6/mol^2]
dC_dTs [list[list[float]], optional] First temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[list[float]], optional] Second temperature derivative of third virial coefficient in density form \(\left[m^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[list[float]], optional] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Cs [list[list[float]]] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) 2]
dC_dTs [list[list[float]]] First temperature derivative of third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\) ]
d2C_dT2s [list[list[float]]] Second temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[list[float]]] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)
```

chemicals.virial.CVirial_Orbey_Vera_mat(T,Tcs, Pcs, omegas, Cs=None,dC_dTs=None,
d2C_dT2s=None, d3C_dT3s=None)

```

Perform a matrix calculation of the Orbey-Vera \(C\) virial coefficient model and its first three temperature derivatives.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list[list[float]]] Critical temperature of fluids [K]
Pcs [list[list[float]]] Critical pressure of the fluids [Pa]
omegas [list[list[float]]] Acentric factor for fluids, [-]
Cs [list[list[float]], optional] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dC_dTs [list[list[float]], optional] First temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[list[float]], optional] Second temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[list[float]], optional] Third temperature derivative of third virial coefficient in density form \(\left[m^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\section*{Returns}

Cs [list[list[float]]] Third virial coefficient in density form [ \(\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2\) ]
dC_dTs [list[list[float]]] First temperature derivative of third virial coefficient in density form [ \(\left.\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}\right]\)
d2C_dT2s [list[list[float]]] Second temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 2\right]\)
d3C_dT3s [list[list[float]]] Third temperature derivative of third virial coefficient in density form \(\left[\mathrm{m}^{\wedge} 6 / \mathrm{mol}^{\wedge} 2 / \mathrm{K}^{\wedge} 3\right]\)

\subsection*{1.35 Viscosity (chemicals.viscosity)}

This module contains various viscosity estimation routines, dataframes of fit coefficients, and mixing rules.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Pure Low Pressure Liquid Correlations
- Pure High Pressure Liquid Correlations
- Liquid Mixing Rules
- Pure Low Pressure Gas Correlations
- Pure High Pressure Gas Correlations
- Gas Mixing Rules
- Correlations for Specific Substances
- Petroleum Correlations
- Fit Correlations
- Conversion functions
- Fit Coefficients

\subsection*{1.35.1 Pure Low Pressure Liquid Correlations}
chemicals.viscosity.Letsou_Stiel ( \(T, M W, T c, P c\), omega)
Calculates the viscosity of a liquid using an emperical model developed in [1]. However. the fitting parameters for tabulated values in the original article are found in ChemSep.
\[
\begin{gathered}
\xi=\frac{2173.424 T_{c}^{1 / 6}}{\sqrt{M W} P_{c}^{2 / 3}} \\
\xi^{(0)}=\left(1.5174-2.135 T_{r}+0.75 T_{r}^{2}\right) \cdot 10^{-5} \\
\xi^{(1)}=\left(4.2552-7.674 T_{r}+3.4 T_{r}^{2}\right) \cdot 10^{-5} \\
\mu=\left(\xi^{(0)}+\omega \xi^{(1)}\right) / \xi
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
MW [float] Molwcular weight of fluid [ \(\mathrm{g} / \mathrm{mol}\) ]

Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor of compound

\section*{Returns}
mu_l [float] Viscosity of liquid, [ \(\mathrm{Pa}^{*}\) s]

\section*{Notes}

The form of this equation is a polynomial fit to tabulated data. The fitting was performed by the DIPPR. This is DIPPR Procedure 8G: Method for the viscosity of pure, nonhydrocarbon liquids at high temperatures internal units are SI standard. [1]'s units were different. DIPPR test value for ethanol is used.

Average error \(34 \%\). Range of applicability is \(0.76<\mathrm{Tr}<0.98\).

\section*{References}
[1]

\section*{Examples}
```

>>> Letsou_Stiel(400., 46.07, 516.25, 6.383E6, 0.6371)
0.0002036150875308

```
chemicals.viscosity.Przedziecki_Sridhar( \(T, T m, T c, P c, V c, V m\), omega, \(M W\) )
Calculates the viscosity of a liquid using an emperical formula developed in [1].
\[
\begin{gathered}
\mu=\frac{V_{o}}{E\left(V-V_{o}\right)} \\
E=-1.12+\frac{V_{c}}{12.94+0.10 M W-0.23 P_{c}+0.0424 T_{m}-11.58\left(T_{m} / T_{c}\right)} \\
V_{o}=0.0085 \omega T_{c}-2.02+\frac{V_{m}}{0.342\left(T_{m} / T_{c}\right)+0.894}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
Tm [float] Melting point of fluid [K]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
Vc [float] Critical volume of the fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
Vm [float] Molar volume of the fluid at temperature [K]
omega [float] Acentric factor of compound
MW [float] Molwcular weight of fluid [g/mol]

\section*{Returns}
mu_l [float] Viscosity of liquid, [Pa*s]

\section*{Notes}

A test by Reid (1983) is used, but only mostly correct. This function is not recommended. Internal units are bar and \(\mathrm{mL} / \mathrm{mol}\).

\section*{References}
[1]

\section*{Examples}
```

>>> Przedziecki_Sridhar(383., 178., 591.8, 41E5, 316E-6, 95E-6, .263, 92.14)

```
0.00021981479956033846

\subsection*{1.35.2 Pure High Pressure Liquid Correlations}
chemicals.viscosity.Lucas \(\left(T, P, T c, P c\right.\), omega, \(\left.P s a t, m u \_l\right)\)
Adjustes for pressure the viscosity of a liquid using an emperical formula developed in [1], but as discussed in [2] as the original source is in German.
\[
\begin{gathered}
\frac{\mu}{\mu_{s a t}}=\frac{1+D\left(\Delta P_{r} / 2.118\right)^{A}}{1+C \omega \Delta P_{r}} \\
\Delta P_{r}=\frac{P-P^{s a t}}{P_{c}} \\
A=0.9991-\frac{4.674 \times 10^{-4}}{1.0523 T_{r}^{-0.03877}-1.0513} \\
D=\frac{0.3257}{\left(1.0039-T_{r}^{2.573}\right)^{0.2906}}-0.2086 \\
C=-0.07921+2.1616 T_{r}-13.4040 T_{r}^{2}+44.1706 T_{r}^{3}-84.8291 T_{r}^{4}+96.1209 T_{r}^{5}-59.8127 T_{r}^{6}+15.6719 T_{r}^{7}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
\(\mathbf{P}\) [float] Pressure of fluid [Pa]
Tc: float Critical point of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
omega [float] Acentric factor of compound
Psat [float] Saturation pressure of the fluid [Pa]
mu_l [float] Viscosity of liquid at 1 atm or saturation, \([\mathrm{Pa}\) ss]

\section*{Returns}
mu_l_dense [float] Viscosity of liquid, \(\left[\mathrm{Pa}^{*} \mathrm{~s}\right]\)

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The example is from Reid (1987); all results agree. Above several thousand bar, this equation does not represent true behavior. If Psat is larger than P, the fluid may not be liquid; dPr is set to 0 .

\section*{References}
[1], [2]

Examples
```

>>> Lucas(300., 500E5, 572.2, 34.7E5, 0.236, 0, 0.00068) \# methylcyclohexane

```
0.0010683738499316494

\subsection*{1.35.3 Liquid Mixing Rules}

No specific correlations are implemented but chemicals.utils.mixing_logarithmic with weight fractions is the recommended form.

\subsection*{1.35.4 Pure Low Pressure Gas Correlations}

\section*{chemicals.viscosity.Yoon_Thodos( \(T, T c, P c, M W\) )}

Calculates the viscosity of a gas using an emperical formula developed in [1].
\[
\begin{gathered}
\eta \xi \times 10^{8}=46.10 T_{r}^{0.618}-20.40 \exp \left(-0.449 T_{r}\right)+19.40 \exp \left(-4.058 T_{r}\right)+1 \\
\xi=2173.424 T_{c}^{1 / 6} M W^{-1 / 2} P_{c}^{-2 / 3}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
MW [float] Molwcular weight of fluid [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
mu_g [float] Viscosity of gas, [Pa*s]

\section*{Notes}

This equation has been tested. The equation uses SI units only internally. The constant 2173.424 is an adjustment factor for units. Average deviation within \(3 \%\) for most compounds. Greatest accuracy with dipole moments close to 0 . Hydrogen and helium have different coefficients, not implemented. This is DIPPR Procedure 8B: Method for the Viscosity of Pure, non hydrocarbon, nonpolar gases at low pressures

\section*{References}
[1]

\section*{Examples}
```

>>> Yoon_Thodos(300., 556.35, 4.5596E6, 153.8)

```
1.019488572777e-05
chemicals.viscosity.Stiel_Thodos( \(T, T c, P c, M W\) )
Calculates the viscosity of a gas using an emperical formula developed in [1].
if \(T_{r}>1.5\) :
\[
\mu_{g}=17.78 \times 10^{-5}\left(4.58 T_{r}-1.67\right)^{0.625} / \xi
\]
else:
\[
\begin{gathered}
\mu_{g}=34 \times 10^{-5} T_{r}^{0.94} / \xi \\
\xi=\frac{T_{c}^{(1 / 6)}}{\sqrt{M W} P_{c}^{2 / 3}}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
MW [float] Molwcular weight of fluid [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
mu_g [float] Viscosity of gas, [Pa*s]

\section*{Notes}

Claimed applicability from 0.2 to 5 atm . Developed with data from 52 nonpolar, and 53 polar gases. internal units are poise and atm. Seems to give reasonable results.

\section*{References}
[1]

\section*{Examples}
```

>>> Stiel_Thodos(300., 556.35, 4.5596E6, 153.8) \#CCl4
1.040892622360e-05

```
chemicals.viscosity.Lucas_gas \((T, T c, P c, Z c, M W\), dipole \(=0.0, C A S R N=\) None \()\)
Estimate the viscosity of a gas using an emperical formula developed in several sources, but as discussed in [1] as the original sources are in German or merely personal communications with the authors of [1].
\[
\begin{gathered}
\eta=\left[0.807 T_{r}^{0.618}-0.357 \exp \left(-0.449 T_{r}\right)+0.340 \exp \left(-4.058 T_{r}\right)+0.018\right] F_{p}^{\circ} F_{Q}^{\circ} / \xi \\
F_{p}^{\circ}=1,0 \leq \mu_{r}<0.022 \\
F_{p}^{\circ}=1+30.55\left(0.292-Z_{c}\right)^{1.72}, 0.022 \leq \mu_{r}<0.075 \\
F_{p}^{\circ}=1+30.55\left(0.292-Z_{c}\right)^{1.72}\left|0.96+0.1\left(T_{r}-0.7\right)\right| 0.075<\mu_{r} \\
F_{Q}^{\circ}=1.22 Q^{0.15}\left\{1+0.00385\left[\left(T_{r}-12\right)^{2}\right]^{1 / M} \operatorname{sign}\left(T_{r}-12\right)\right\} \\
\mu_{r}=52.46 \frac{\mu^{2} P_{c}}{T_{c}^{2}} \\
\xi=0.176\left(\frac{T_{c}}{M W^{3} P_{c}^{4}}\right)^{1 / 6}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc: float Critical point of fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
Zc [float] Critical compressibility of the fluid [Pa]
dipole [float] Dipole moment of fluid [debye]
CASRN [str, optional] CAS of the fluid

\section*{Returns}
mu_g [float] Viscosity of gas, [ Pa *s]

\section*{Notes}

The example is from [1]; all results agree. Viscosity is calculated in micropoise, and converted to SI internally (1E-7). Q for \(\mathrm{He}=1.38 ; \mathrm{Q}\) for \(\mathrm{H} 2=0.76 ; \mathrm{Q}\) for \(\mathrm{D} 2=0.52\).

\section*{References}
[1]

\section*{Examples}
```

>>> Lucas_gas(T=550., Tc=512.6, Pc=80.9E5, Zc=0.224, MW=32.042, dipole=1.7)

```
\(1.7822676912698925 \mathrm{e}-05\)
chemicals.viscosity.viscosity_gas_Gharagheizi ( \(T, T c, P c, M W\) )
Calculates the viscosity of a gas using an emperical formula developed in [1].
\[
\mu=10^{-7}\left|10^{-5} P_{c} T_{r}+\left(0.091-\frac{0.477}{M}\right) T+M\left(10^{-5} P_{c}-\frac{8 M^{2}}{T^{2}}\right)\left(\frac{10.7639}{T_{c}}-\frac{4.1929}{T}\right)\right|
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
Tc [float] Critical temperature of the fluid [K]
Pc [float] Critical pressure of the fluid [Pa]
MW [float] Molwcular weight of fluid [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
mu_g [float] Viscosity of gas, [ \(\mathrm{Pa}^{*}\) s]

\section*{Notes}

Example is first point in supporting information of article, for methane. This is the prefered function for gas viscosity. 7\% average relative deviation. Deviation should never be above 30\%. Developed with the DIPPR database. It is believed theoretically predicted values are included in the correlation.
Under 0.2 Tc , this correlation has been modified to provide values at the limit.

\section*{References}
[1]

Examples
```

>>> viscosity_gas_Gharagheizi(120., 190.564, 45.99E5, 16.04246)
5.215761625399613e-06

```

\subsection*{1.35.5 Pure High Pressure Gas Correlations}

No correlations are implemented yet.

\subsection*{1.35.6 Gas Mixing Rules}
chemicals.viscosity.Herning_Zipperer (zs, mus, MWs, MW_roots=None)
Calculates viscosity of a gas mixture according to mixing rules in [1].
\[
\mu=\frac{\sum x_{i} \mu_{i} \sqrt{M W_{i}}}{\sum x_{i} \sqrt{M W_{i}}}
\]

\section*{Parameters}
zs [float] Mole fractions of components, [-]
mus [float] Gas viscosities of all components, [ \(\mathrm{Pa} * \mathrm{~s}\) ]
MWs [float] Molecular weights of all components, [ \(\mathrm{g} / \mathrm{mol}\) ]
MW_roots [float, optional] Square roots of molecular weights of all components, [ \(\mathrm{g}^{\wedge} 0.5 / \mathrm{mol}^{\wedge} 0.5\) ]

\section*{Returns}
mug [float] Viscosity of gas mixture, [ \(\mathrm{Pa}^{*} \mathrm{~s}\) ]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The original source has not been reviewed. Adding the square roots can speed up the calculation.

\section*{References}
[1]

\section*{Examples}
>> Herning_Zipperer([0.5, 0.25, 0.25], [1.78e-05, 1.12e-05, 9.35e-06], [28.0134, \(\rightarrow 16.043\), 30.07])
\(1.4174908599465168 \mathrm{e}-05\)
chemicals.viscosity.Brokaw (T, ys, mus, MWs, molecular_diameters, Stockmayers)
Calculates viscosity of a gas mixture according to mixing rules in [1].
\[
\begin{gathered}
\eta_{m i x}=\sum_{i=1}^{n} \frac{y_{i} \eta_{i}}{\sum_{j=1}^{n} y_{j} \phi_{i j}} \\
\phi_{i j}=\left(\frac{\eta_{i}}{\eta_{j}}\right)^{0.5} S_{i j} A_{i j} \\
A_{i j}=m_{i j} M_{i j}^{-0.5}\left[1+\frac{M_{i j}-M_{i j}^{0.45}}{2\left(1+M_{i j}\right)+\frac{\left(1+M_{i j}^{0.45}\right) m_{i j}^{-0.5}}{1+m_{i j}}}\right] \\
m_{i j}=\left[\frac{4}{\left(1+M_{i j}^{-1}\right)\left(1+M_{i j}\right)}\right]^{0.25} \\
S_{i j}=\frac{M_{i j}}{\left[1+T_{i}^{*}+\left(\delta_{i}^{2} / 4\right)\right]^{0.5}\left[1+T_{j}^{*}+\left(\delta_{j}^{2} / 4\right)\right]^{0.5}} \\
T^{*}=k T / \epsilon
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of fluid, [K]
ys [float] Mole fractions of gas components, [-]
mus [float] Gas viscosities of all components, \(\left[\mathrm{Pa}^{*} \mathrm{~s}\right.\) ]
MWs [float] Molecular weights of all components, [ \(\mathrm{g} / \mathrm{mol}\) ]
molecular_diameters [float] L-J molecular diameter of all components, [angstroms]
Stockmayers [float] L-J Stockmayer energy parameters of all components, []

\section*{Returns}
mug [float] Viscosity of gas mixture, [Pa*s]

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The original source has not been reviewed.
This is DIPPR Procedure 8D: Method for the Viscosity of Nonhydrocarbon Vapor Mixtures at Low Pressure (Polar and Nonpolar)

\section*{References}
[1], [2], [3]

\section*{Examples}
>>> Brokaw(308.2, [0.05, 0.95], [1.34E-5, 9.5029E-6], [64.06, 46.07], [0.42, 0.19], 七 \(\rightarrow\) [347, 432])
\(9.699085099801568 \mathrm{e}-06\)
chemicals.viscosity.Wilke ( \(y s\), mus, \(M W s\) )
Calculates viscosity of a gas mixture according to mixing rules in [1].
\[
\begin{gathered}
\eta_{m i x}=\sum_{i=1}^{n} \frac{y_{i} \eta_{i}}{\sum_{j=1}^{n} y_{j} \phi_{i j}} \\
\phi_{i j}=\frac{\left(1+\sqrt{\eta_{i} / \eta_{j}}\left(M W_{j} / M W_{i}\right)^{0.25}\right)^{2}}{\sqrt{8\left(1+M W_{i} / M W_{j}\right)}}
\end{gathered}
\]

\section*{Parameters}
ys [float] Mole fractions of gas components, [-]
mus [float] Gas viscosities of all components, [Pa*s]
MWs [float] Molecular weights of all components, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
mug [float] Viscosity of gas mixture, [ \(\mathrm{Pa}^{*}\) s]

\section*{See also:}

Wilke_prefactors
Wilke_prefactored
Wilke_large

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel. The original source has not been reviewed or found.

\section*{References}
[1]

\section*{Examples}
>>> Wilke([0.05, 0.95], [1.34E-5, 9.5029E-6], [64.06, 46.07])
9.701614885866193e-06

\section*{chemicals.viscosity.Wilke_prefactors(MWs)}

The Wilke gas viscosity method can be sped up by precomputing several matrices. The memory used is proportional to \(\mathrm{N}^{\wedge} 2\), so it can be significant, but is still a substantial performance increase even when they are so large they cannot fit into cached memory. These matrices are functions of molecular weights only. These are used by the Wilke_prefactored function.
\[
\begin{aligned}
t 0_{i, j} & =\frac{\sqrt{\frac{M W_{j}}{M W_{i}}}}{\sqrt{\frac{8 M W_{i}}{M W_{j}}+8}} \\
t 1_{i, j} & =\frac{2 \sqrt[4]{\frac{M W_{j}}{M W_{i}}}}{\sqrt{\frac{8 M W_{i}}{M W_{j}}+8}} \\
t 2_{i, j} & =\frac{1}{\sqrt{\frac{8 M W_{i}}{M W_{j}}+8}}
\end{aligned}
\]

\section*{Parameters}

MWs [list[float]] Molecular weights of all components, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
t0s [list[list[float]]] First terms, [-]
t1s [list[list[float]]] Second terms, [-]
t2s [list[list[float]]] Third terms, [-]

\section*{Notes}

These terms are derived as follows using SymPy. The viscosity terms are not known before hand so they are not included in the factors, but otherwise these parameters simplify the computation of the \(\phi_{i j}\) term to the following:
\[
\phi_{i j}=\frac{\mu_{i}}{\mu_{j}} t 0_{i, j}+\sqrt{\frac{\mu_{i}}{\mu_{j}}} t 1_{i, j}+t 2_{i, j}
\]
```

>>> from sympy import *
>>> MWi, MWj, mui, muj = symbols('MW_i, MW_j, mu_i, mu_j')
>>> f = (1 + sqrt(mui/muj)*(MWj/MWi)**Rational (1,4))**2
>>> denom = sqrt(8*(1+MWi/MWj))
>>> (expand(simplify(expand(f))/denom))
mu_i*sqrt(MW_j/MW_i)/(mu_j*sqrt(8*MW_i/MW_j + 8)) + 2*(MW_j/MW_i)**(1/4)*sqrt(mu_i/
๑mu_j)/sqrt(8*MW_i/MW_j + 8) + 1/sqrt(8*MW_i/MW_j + 8)

```

\section*{Examples}
>>> Wilke_prefactors([64.06, 46.07])
([[0.25, 0.19392193320396522], [0.3179655106303118, 0.25]], [[0.5, 0.
\(\rightarrow 421161930934918],[0.5856226024677849,0.5]],[[0.25,0.22867110638055677]\), [0. \(\rightarrow 2696470380083788,0.25]])\)
>> Wilke_prefactored([0.05, 0.95], [1.34E-5, 9.5029E-6], *Wilke_prefactors([64.06, \(\hookrightarrow 46.07]\) ))
\(9.701614885866193 e-06\)
chemicals.viscosity.Wilke_prefactored (ys, mus, \(t 0 s, t 1 s, t 2 s\) )
Calculates viscosity of a gas mixture according to mixing rules in [1], using precomputed parameters.
\[
\begin{gathered}
\eta_{m i x}=\sum_{i=1}^{n} \frac{y_{i} \eta_{i}}{\sum_{j=1}^{n} y_{j} \phi_{i j}} \\
\phi_{i j}=\frac{\mu_{i}}{\mu_{j}} t 0_{i, j}+\sqrt{\frac{\mu_{i}}{\mu_{j}}} t 1_{i, j}+t 2_{i, j}
\end{gathered}
\]

\section*{Parameters}
ys [float] Mole fractions of gas components, [-]
mus [float] Gas viscosities of all components, [ \(\mathrm{Pa} * \mathrm{~s}\) ]
t0s [list[list[float]]] First terms, [-]
t1s [list[list[float]]] Second terms, [-]
t2s [list[list[float]]] Third terms, [-]

\section*{Returns}
mug [float] Viscosity of gas mixture, \(\left[\mathrm{Pa}{ }^{*}\right.\) s]
See also:
Wilke_prefactors
Wilke
Wilke_large

\section*{Notes}

This equation is entirely dimensionless; all dimensions cancel.

\section*{References}
[1]

\section*{Examples}
>> Wilke_prefactored([0.05, 0.95], [1.34E-5, 9.5029E-6], *Wilke_prefactors([64.06, \(\rightarrow 46.07])\) )
9.701614885866193e-06

\section*{chemicals.viscosity.Wilke_large (ys, mus, MWs)}

Calculates viscosity of a gas mixture according to mixing rules in [1].
This function is a slightly faster version of Wilke. It achieves its extra speed by avoiding some checks, some powers, and by allocating less memory during the computation. For very large component vectors, this function should be called instead.

\section*{Parameters}
ys [float] Mole fractions of gas components, [-]
mus [float] Gas viscosities of all components, \(\left[\mathrm{Pa}^{*} \mathrm{~s}\right]\)
MWs [float] Molecular weights of all components, [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}
mug [float] Viscosity of gas mixture, [ \(\mathrm{Pa}^{*} \mathrm{~s}\) ]

\section*{See also:}

Wilke_prefactors
Wilke_prefactored
Wilke

\section*{References}
[1]

\section*{Examples}
>>> Wilke_large([0.05, 0.95], [1.34E-5, 9.5029E-6], [64.06, 46.07])
9.701614885866193e-06

\subsection*{1.35.7 Correlations for Specific Substances}
chemicals.viscosity.mu_IAPWS \(\left(T, r h o, d r h o \_d P=N o n e, d r h o \_d P \_T r=N o n e\right)\)
Calculates and returns the viscosity of water according to the IAPWS (2008) release.
Viscosity is calculated as a function of three terms; the first is the dilute-gas limit; the second is the contribution due to finite density; and the third and most complex is a critical enhancement term.
\[
\begin{gathered}
\mu=\mu_{0} \cdot \mu_{1}(T, \rho) \cdot \mu_{2}(T, \rho) \\
\mu_{0}(T)=\frac{100 \sqrt{T}}{\sum_{i=0}^{3} \frac{H_{i}}{T^{\imath}}}
\end{gathered}
\]
\[
\begin{gathered}
\mu_{1}(T, \rho)=\exp \left[\rho \sum_{i=0}^{5}\left(\left(\frac{1}{T}-1\right)^{i} \sum_{j=0}^{6} H_{i j}(\rho-1)^{j}\right)\right] \\
\text { if } \xi<0.3817016416 \mathrm{~nm}: \\
Y=0.2 q_{c} \xi\left(q_{D} \xi\right)^{5}\left(1-q_{c} \xi+\left(q_{c} \xi\right)^{2}-\frac{765}{504}\left(q_{D} \xi\right)^{2}\right) \\
\text { else: } \\
Y=\frac{1}{12} \sin \left(3 \psi_{D}\right)-\frac{1}{4 q_{c} \xi} \sin \left(2 \psi_{D}\right)+\frac{1}{\left(q_{c} \xi\right)^{2}}\left[1-1.25\left(q_{c} \xi\right)^{2}\right] \sin \left(\psi_{D}\right)-\frac{1}{\left(q_{c} \xi\right)^{3}}\left\{\left[1-1.5\left(q_{c} \xi\right)^{2}\right] \psi_{D}-\left|\left(q_{c} \xi\right)^{2}-1\right|^{1.5} L(w)\right. \\
w=\left|\frac{q_{c} \xi-1}{q_{c} \xi+1}\right|^{0.5} \tan \left(\frac{\psi_{D}}{2}\right) \\
L(w)=\ln \frac{1+w}{1-w} \text { if } q_{c} \xi>1 \\
L(w)=2 \arctan |w| \text { if } q_{c} \xi \leq 1 \\
\psi_{D}=\arccos \left[\left(1+q_{D}^{2} \xi^{2}\right)^{-0.5}\right] \\
\Delta \bar{\chi}(\bar{T}, \bar{\rho})=\bar{\rho}\left[\zeta(\bar{T}, \bar{\rho})-\zeta\left(\bar{T}_{R}, \bar{\rho}\right) \frac{\bar{T}_{R}}{\bar{T}}\right] \\
\xi=\xi_{0}\left(\frac{\Delta \bar{\chi}}{\Gamma_{0}}\right)^{\nu / \gamma} \\
\zeta=\left(\frac{\partial \bar{\rho}}{\partial \bar{p}}\right)_{\bar{T}}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of water [K]
rho [float] Density of water [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
drho_dP [float, optional] Partial derivative of density with respect to pressure at constant temperature (at the temperature and density of water), \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3 / \mathrm{Pa}\right]\)
drho_dP_Tr [float, optional] Partial derivative of density with respect to pressure at constant temperature (at the reference temperature ( 970.644 K ) and the actual density of water), \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3 / \mathrm{Pa}\right]\)

\section*{Returns}
mu [float] Viscosity, [Pa*s]

\section*{Notes}

There are three ways to use this formulation.
1) Compute the Industrial formulation value which does not include the critical enhacement, by leaving \(d r h o \_d P\) and \(d r h o \_d P \_T r\) None.
2) Compute the Scientific formulation value by accurately computing and providing \(d r h o \_d P\) and \(d r h o \_d P \_T r\), both with IAPWS-95.
3) Get a non-standard but 8 decimal place matching result by providing \(d r h o \_d P\) computed with either IAPWS-95 or IAPWS-97, but not providing drho_dP_Tr; which is calculated internally. There is a formulation for that term in the thermal conductivity IAPWS equation which is used.
\(\mathrm{xmu}=0.068\)
\(\mathrm{qc}=(1.9 \mathrm{E}-9)^{* *-1}\)
\(\mathrm{qd}=(1.1 \mathrm{E}-9) * *-1\)
\(\mathrm{nu}=0.630\)
gamma \(=1.239\)
\(\mathrm{xi} 0=0.13 \mathrm{E}-9\)
Gamma0 \(=0.06\)
\(\mathrm{TRC}=1.5\)
This forulation is highly optimized, spending most of its time in the logarithm, power, and square root.

\section*{References}
[1]

\section*{Examples}
```

>>> mu_IAPWS(298.15, 998.)
0.000889735100149808

```
```

>>> mu_IAPWS(1173.15, 400.)

```
>>> mu_IAPWS(1173.15, 400.)
6.415460784836147e-05
```

6.415460784836147e-05

```

Point 4 of formulation, compared with MPEI and IAPWS, matches.
```

>>> mu_IAPWS(T=647.35, rho=322., drho_dP=1.213641949033E-2)
4.2961578738287e-05

```

Full scientific calculation:
```

>>> from chemicals.iapws import iapws95_properties, iapws95_P, iapws95_Tc
>>> T, P = 298.15, 1e5
>>> rho, _, _, _, _, _, _, _, _, _, drho_dP = iapws95_properties(T, P)
>>> P_ref = iapws95_P(1.5*iapws95_Tc, rho)
>>> _, _, _, _, _, _, _, _, _, _, drho_dP_Tr = iapws95_properties(1.5*iapws95_Tc, P_
ref)
>>> mu_IAPWS(T, rho, drho_dP, drho_dP_Tr)
0.00089002267377

```
chemicals.viscosity.mu_air_lemmon ( \(T\), rho)

Calculates and returns the viscosity of air according to Lemmon and Jacobsen (2003) [1].
Viscosity is calculated as a function of two terms; the first is the dilute-gas limit; the second is the contribution due to finite density.
\[
\begin{gathered}
\mu=\mu^{0}(T)+\mu^{r}(T, \rho) \\
\mu^{0}(T)=\frac{0.9266958 \sqrt{M T}}{\sigma^{2} \Omega\left(T^{*}\right)}
\end{gathered}
\]
\[
\begin{aligned}
& \Omega\left(T^{*}\right)=\exp \left(\sum_{i=0}^{4} b_{i}\left[\ln \left(T^{*}\right)\right]^{i}\right) \\
& \mu^{r}=\sum_{i=1}^{n} N_{i} \tau^{t_{i}} \delta^{d_{i}} \exp \left(-\gamma_{i} \delta^{l_{i}}\right)
\end{aligned}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of air [K]
rho [float] Molar density of air [ \(\mathrm{mol} / \mathrm{m}^{\wedge} 3\) ]

\section*{Returns}
mu [float] Viscosity of air, [ \(\mathrm{Pa}^{*}\) s]

\section*{Notes}

The coefficients are:
\(\mathrm{Ni}=[10.72,1.122,0.002019,-8.876,-0.02916]\)
\(\mathrm{ti}=[0.2,0.05,2.4,0.6,3.6]\)
\(\mathrm{di}=[1,4,9,1,8]\)
gammai \(=\mathrm{Ii}=[0,0,0,1,1]\)
\(\mathrm{bi}=[.431,-0.4623,0.08406,0.005341,-0.00331]\)
The reducing parameters are \(T_{c}=132.6312 \mathrm{~K}\) and \(\rho_{c}=10447.7 \mathrm{~mol} / \mathrm{m}^{\wedge} 3\). Additional parameters used are \(\sigma=0.36 \mathrm{~nm}, M=28.9586 \mathrm{~g} / \mathrm{mol}\) and \(\frac{e}{k}=103.3 \mathrm{~K}\).
This is an implementation optimized for speed, spending its time in the calclulation of \(1 \log ; 2 \mathrm{exp} ; 1\) power; and 2 divisions.

\section*{References}
[1]

\section*{Examples}

Viscosity at 300 K and 1 bar:
```

>>> mu_air_lemmon(300.0, 40.10292351061862)
1.85371518556e-05

```

Calculate the density in-place:
```

>>> from chemicals.air import lemmon2000_rho
>>> mu_air_lemmon(300.0, lemmon2000_rho(300.0, 1e5))
1.85371518556e-05

```

\subsection*{1.35.8 Petroleum Correlations}

\section*{chemicals.viscosity.Twu_1985(T, Tb, rho)}

Calculate the viscosity of a petroleum liquid using the Twu (1985) correlation developed in [1]. Based on a fit to \(n\)-alkanes that used as a reference. Requires the boiling point and density of the system.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tb [float] Normal boiling point, [K]
rho [float] Liquid density liquid as measured at \(60 \operatorname{deg} \mathrm{~F},\left[\mathrm{~kg} / \mathrm{m}^{\wedge} 3\right]\)

\section*{Returns}
mu [float] Liquid viscosity, [Pa*s]

\section*{Notes}

The formulas are as follows:
\[
\begin{gathered}
T_{c}^{\circ}=T_{b}\left(0.533272+0.191017 \times 10^{-3} T_{b}+0.779681 \times 10^{-7} T_{b}^{2}-0.284376 \times 10^{-10} T_{b}^{3}+0.959468 \times 10^{28} / T_{b}^{13}\right)^{-1} \\
\alpha=1-T_{b} / T_{c}^{\circ} \\
\ln \left(\nu_{2}^{\circ}+1.5\right)=4.73227-27.0975 \alpha+49.4491 \alpha^{2}-50.4706 \alpha^{4} \\
\ln \left(\nu_{1}^{\circ}\right)=0.801621+1.37179 \ln \left(\nu_{2}^{\circ}\right) \\
S G^{\circ}=0.843593-0.128624 \alpha-3.36159 \alpha^{3}-13749.5 \alpha^{12} \\
\Delta S G=S G-S G^{\circ} \\
|x|=\left|1.99873-56.7394 / \sqrt{T_{b}}\right| \\
f_{1}=1.33932|x| \Delta S G-21.1141 \Delta S G^{2} / \sqrt{T_{b}} \\
f_{2}=|x| \Delta S G-21.1141 \Delta S G^{2} / \sqrt{T_{b}} \\
\ln \left(\nu_{1}+\frac{450}{T_{b}}\right)=\ln \left(\nu_{1}^{\circ}+\frac{450}{T_{b}}\right)\left(\frac{1+2 f_{1}}{1-2 f_{1}}\right)^{2} \\
\ln \left(\nu_{2}+\frac{450}{T_{b}}\right)=\ln \left(\nu_{2}^{\circ}+\frac{450}{T_{b}}\right)\left(\frac{1+2 f_{2}}{1-2 f_{2}}\right)^{2} \\
Z=\nu+0.7+\exp \left(-1.47-1.84 \nu-0.51 \nu^{2}\right) \\
B=\frac{\ln \ln Z_{1}-\ln \ln Z_{2}}{\ln T_{1}-\ln T_{2}} \\
\left.\left.\nu=(Z-0.7)-\exp (-0.7487-3.295 Z-0.7)+0.6119 Z-0.7)^{2}-0.3193 Z-0.7\right)^{3}\right)
\end{gathered}
\]

\section*{References}
[1]

\section*{Examples}

Sample point from article:
>>> Twu_1985 ( \(\mathrm{T}=338.7055\), \(\mathrm{Tb}=672.3166\), rho=895.5189)
0.008235009644854494

\section*{chemicals.viscosity.Lorentz_Bray_Clarke( \(T, P, V m, z s, M W s, T c s, P c s, V c s)\)}

Calculates the viscosity of a gas or a liquid using the method of Lorentz, Bray, and Clarke [1]. This method is not quite the same as the original, but rather the form commonly presented and used today. The original had a different formula for pressure correction for gases which was tabular and not presented entirely in [1]. However using that distinction introduces a discontinuity between the liquid and gas viscosity, so it is not normally used.
\[
\begin{gathered}
\mu[\text { centipoise }]=\mu_{\text {Plow, Stiel-hThodos }}[\text { centipoise }]+\frac{\text { poly }^{4}-0.0001}{\xi} \\
\text { poly }=\left(0.1023+0.023364 \rho_{r}+0.058533 \rho_{r}^{2}-0.040758 \rho_{r}^{3}+0.0093724 \rho_{r}^{4}\right) \\
\xi=T_{c}^{1 / 6} M W^{-1 / 2}\left(P_{c}[\text { atm }]\right)^{-2 / 3}
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of the fluid [K]
\(\mathbf{P}\) [float] Pressure of the fluid [Pa]
\(\mathbf{V m}\) [float] Molar volume of the fluid at the actual conditions, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
zs [list[float]] Mole fractions of chemicals in the fluid, [-]
MWs [list[float]] Molwcular weights of chemicals in the fluid [g/mol]
Tcs [float] Critical temperatures of chemicals in the fluid [K]
Pcs [float] Critical pressures of chemicals in the fluid [Pa]
Vcs [float] Critical molar volumes of chemicals in the fluid; these are often used as tuning parameters, fit to match a pure component experimental viscosity value [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}
\(\mathbf{m u}\) [float] Viscosity of phase at actual conditions, \([\mathrm{Pa} * \mathrm{~s}]\)

\section*{Notes}

An example from [2] was implemented and checked for validation. Somewhat different rounding is used in [2]. The mixing of the pure component Stiel-Thodos viscosities happens with the Herning-Zipperer mixing rule:
\[
\mu=\frac{\sum x_{i} \mu_{i} \sqrt{M W_{i}}}{\sum x_{i} \sqrt{M W_{i}}}
\]

\section*{References}
[1], [2]

\section*{Examples}
>>> Lorentz_Bray_Clarke(T=300.0, \(\mathrm{P}=1 \mathrm{e} 6, \mathrm{Vm}=0.0023025, \mathrm{zs}=[.4, .3, .3]\),
... MWs \(=[16.04246,30.06904,44.09562], \mathrm{Tcs}=[190.564,305.32,369.83]\),
... Pcs=[4599000.0, 4872000.0, 4248000.0], Vcs=[9.86e-05, 0.0001455, 0.0002])
\(9.925488160761484 e-06\)

\subsection*{1.35.9 Fit Correlations}
chemicals.viscosity. \(\operatorname{PPDS} 9(T, A, B, C, D, E)\)
Calculate the viscosity of a liquid using the 5 -term exponential power fit developed by the PPDS and named PPDS equation 9 .
\[
\mu=E \exp \left[A\left(\frac{C-T}{T-D}\right)^{1 / 3}+B\left(\frac{C-T}{T-D}\right)^{4 / 3}\right]
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [-]
C [float] Coefficient, [K]
D [float] Coefficient, [K]
E [float] Coefficient, [ Pa *s]

\section*{Returns}
mu [float] Liquid viscosity, [ Pa *s]

\section*{Notes}

No other source for these coefficients has been found.
There can be a singularity in this equation when \(T\) approaches \(C\) or \(D\); it may be helpful to take as a limit to this equation \(D+5 \mathrm{~K}\).

\section*{References}
[1]

\section*{Examples}
\(\gg \operatorname{PPDS} 9(400.0,1.74793,1.33728,482.347,41.78,9.963 \mathrm{e}-05)\)
0.00035091137378230684
chemicals.viscosity.dPPDS9_dT \((T, A, B, C, D, E)\)
Calculate the temperature derivative of viscosity of a liquid using the 5 -term exponential power fit developed by the PPDS and named PPDS equation 9 .
Normally, the temperature derivative is:
\[
\frac{\partial \mu}{\partial T}=E\left(\frac{A \sqrt[3]{\frac{C-T}{-D+T}}(-D+T)\left(-\frac{C-T}{3(-D+T)^{2}}-\frac{1}{3(-D+T)}\right)}{C-T}-\frac{B \sqrt[3]{\frac{C-T}{-D+T}}(C-T)}{(-D+T)^{2}}+B \sqrt[3]{\frac{C-T}{-D+T}}\left(-\frac{C-T}{3(-D+T)^{2}}-\frac{}{3}\right)\right.
\]

For the low-temperature region:
\[
\frac{\partial \mu}{\partial T}=E\left(-\frac{A \sqrt[3]{\frac{-C+T}{-D+T}}(-D+T)\left(-\frac{-C+T}{3(-D+T)^{2}}+\frac{1}{3(-D+T)}\right)}{-C+T}+\frac{B \sqrt[3]{\frac{-C+T}{-D+T}}(C-T)}{(-D+T)^{2}}+\frac{B \sqrt[3]{\frac{-C+T}{-D+T}}}{-D+T}-\frac{B \sqrt[3]{\frac{-C+T}{-D+T}}(C-T)}{-}\right.
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [-]
C [float] Coefficient, [K]
D [float] Coefficient, [K]
E [float] Coefficient, [ \(\mathrm{Pa}^{*}\) s]

\section*{Returns}
dmu_dT [float] First temperature derivative of liquid viscosity, [ \(\mathrm{Pa} * \mathrm{~s}\) ]
\(\mathbf{m u}\) [float] Liquid viscosity, [Pa*s]

\section*{References}
[1]

\section*{Examples}
>>> dPPDS9_dT(400.0, 1.74793, 1.33728, 482.347, 41.78, 9.963e-05)
(-3.186540635882627e-06, 0.00035091137378230684)

\section*{chemicals.viscosity.PPDS5( \(T, T c, a 0, a 1, a 2\) )}

Calculate the viscosity of a low-pressure gas using the 3-term exponential power fit developed by the PPDS and named PPDS equation 5 .
\[
\mu=\frac{a_{0} T_{r}}{\left(1+a_{1} T_{r}^{a_{2}}\left(T_{r}-1\right)\right)^{1 / 6}}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
a0 [float] Coefficient, [-]
a1 [float] Coefficient, [-]
a2 [float] Coefficient, [-]

\section*{Returns}
mu [float] Low pressure gas viscosity, [ \(\mathrm{Pa} * \mathrm{~s}\) ]

\section*{References}
[1]

\section*{Examples}

Sample coefficients for n-pentane in [1], at 350 K :
>> PPDS5 (T=350.0, Tc=470.008, \(\mathrm{a} 0=1.08003 \mathrm{e}-5, \mathrm{a} 1=0.19583, \mathrm{a} 2=0.811897\) )
8.096643275836e-06
chemicals.viscosity.Viswanath_Natarajan_2 \((T, A, B)\)
Calculate the viscosity of a liquid using the 2-term form representation developed in [1]. Requires input coefficients. The \(A\) coefficient is assumed to yield coefficients in Pa *s; if it yields values in \(1 \mathrm{E}-3 \mathrm{~Pa}\) *s, remove \(\log (100)\) for A.
\[
\mu=\exp \left(A+\frac{B}{T}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [K]

\section*{Returns}
mu [float] Liquid viscosity, [ Pa *s]

\section*{Notes}

No other source for these coefficients than [1] has been found.

\section*{References}
[1]

\section*{Examples}

DDBST has 0.0004580 as a value at this temperature for 1-Butanol.
>>> Viswanath_Natarajan_2(348.15, -5.9719-log(100), 1007.0)
0.000459836869568295

\section*{chemicals.viscosity.Viswanath_Natarajan_2_exponential \((T, C, D)\)}

Calculate the viscosity of a liquid using the 2-term exponential form representation developed in [1]. Requires input coefficients. The \(A\) coefficient is assumed to yield coefficients in Pa*s, as all coefficients found so far have been.
\[
\mu=C T^{D}
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
C [float] Linear coefficient, [ Pa *s]
D [float] Exponential coefficient, [-]

\section*{Returns}
\(\mathbf{m u}\) [float] Liquid viscosity, [Pa*s]

\section*{Notes}

No other source for these coefficients has been found.

\section*{References}
[1]

\section*{Examples}
```

>>> Ts = [283.15, 288.15, 303.15, 349.65]
>>> mus = [2.2173, 2.1530, 1.741, 1.0091] \# in cP
>>> Viswanath_Natarajan_2_exponential(288.15, 4900800, -3.8075)
0.002114798866203873

```

Calculation of the AARD of the fit ( \(1 \%\) is the value stated in [1].:
```

>>> mu_calc = [Viswanath_Natarajan_2_exponential(T, 4900800, -3.8075) for T in Ts]
>>> np.mean([abs((mu - mu_i*1000)/mu) for mu, mu_i in zip(mus, mu_calc)])
0.010467928813061298

```
chemicals.viscosity.Viswanath_Natarajan_3( \(T, A, B, C\) )
Calculate the viscosity of a liquid using the 3-term Antoine form representation developed in [1]. Requires input coefficients. If the coefficients do not yield viscosity in \(\mathrm{Pa}^{*} \mathrm{~s}\), but rather cP , remove \(\log 10(1000)\) from \(A\).
\[
\log _{10} \mu=A+B /(T+C)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [K]
C [float] Coefficient, [K]

\section*{Returns}
mu [float] Liquid viscosity, \(\left[\mathrm{Pa}^{*} \mathrm{~s}\right]\)

\section*{Notes}

No other source for these coefficients has been found.

\section*{References}
[1]

\section*{Examples}
>>> from math import log10
>>> Viswanath_Natarajan_3(298.15, -2.7173-log10(1000), -1071.18, -129.51)
0.0006129806445142113
chemicals.viscosity.mu_Yaws \((T, A, B, C=0.0, D=0.0)\)
Calculate the viscosity of a liquid using the 4-term Yaws polynomial form. Requires input coefficients. If the coefficients do not yield viscosity in \(\mathrm{Pa}^{*}\) s, but rather cP , remove \(\log 10(1000)\) from \(A\); this is required for the coefficients in [1].
\[
\log _{10} \mu=A+B / T+C T+D T^{2}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [K]
C [float] Coefficient, [1/K]
D [float] Coefficient, [1/K^2]

\section*{Returns}
mu [float] Liquid viscosity, \(\left[\mathrm{Pa}^{*} \mathrm{~s}\right]\)

\section*{References}
[1]

\section*{Examples}
>>> from math import log10
>>> mu_Yaws(300.0, -6.4406-log10(1000), 1117.6, 0.0137, -0.000015465)
0.0010066612081
chemicals.viscosity.dmu_Yaws_dT \((T, A, B, C=0.0, D=0.0)\)
Calculate the temperature derivative of the viscosity of a liquid using the 4-term Yaws polynomial form. Requires input coefficients.
\[
\frac{\partial \mu}{\partial T}=10^{A+\frac{B}{T}+T(C+D T)}\left(-\frac{B}{T^{2}}+C+2 D T\right) \log (10)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [K]
C [float] Coefficient, [1/K]
D [float] Coefficient, [1/K^2]

\section*{Returns}
dmu_dT [float] First temperature derivative of liquid viscosity, \([\mathrm{Pa} * \mathrm{~s} / \mathrm{K}]\)

\section*{Examples}
```

>>> dmu_Yaws_dT(300.0, -9.4406, 1117.6, 0.0137, -0.000015465)

```
-1.853591586963e-05
chemicals.viscosity.mu_Yaws_fitting_jacobian (Ts, \(A, B, C, D)\)
Compute and return the Jacobian of the property predicted by the Yaws viscosity equation with respect to all the coefficients. This is used in fitting parameters for chemicals.

\section*{Parameters}

Ts [list[float]] Temperatures of the experimental data points, [K]
A [float] Coefficient, [-]
B [float] Coefficient, [K]
C [float] Coefficient, [1/K]
D [float] Coefficient, [1/K^2]

\section*{Returns}
jac [list[list[float, 4], len(Ts)]] Matrix of derivatives of the equation with respect to the fitting parameters, [various]
chemicals.viscosity.mu_TDE \((T, A, B, C, D)\)
Calculate the viscosity of a liquid using the 4-term exponential inverse-temperature fit equation used in NIST's TDE.
\[
\mu=\exp \left[A+\frac{B}{T}+\frac{C}{T^{2}}+\frac{D}{T^{3}}\right]
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
A [float] Coefficient, [-]
B [float] Coefficient, [K]
C [float] Coefficient, [K^2]
D [float] Coefficient, [ \(K^{\wedge} 3\) ]

\section*{Returns}
mu [float] Liquid viscosity, [ Pa *s]

\section*{References}
[1]

\section*{Examples}

Coefficients for isooctane at 400 K , as shown in [1].
```

>>> mu_TDE(400.0, -14.0878, 3500.26, -678132.0, 6.17706e7)
0.0001822175281438

```

\subsection*{1.35.10 Conversion functions}

\section*{chemicals.viscosity.viscosity_converter (val, old_scale, new_scale, extrapolate=False)}

Converts kinematic viscosity values from different scales which have historically been used. Though they may not be in use much, some standards still specify values in these scales.

\section*{Parameters}
val [float] Viscosity value in the specified scale; [m^2/s] if 'kinematic viscosity'; [degrees] if Engler or Barbey; [s] for the other scales.
old_scale [str] String representing the scale that val is in originally.
new_scale [str] String representing the scale that val should be converted to.
extrapolate [bool] If True, a conversion will be performed even if outside the limits of either scale; if False, and either value is outside a limit, an exception will be raised.

\section*{Returns}
result [float] Viscosity value in the specified scale; [m^2/s] if 'kinematic viscosity'; [degrees] if Engler or Barbey; [s] for the other scales

\section*{Notes}

The valid scales for this function are any of the following:
['a\&w b', 'a\&w crucible', 'american can', 'astm 0.07', 'astm 0.10', 'astm 0.15', 'astm 0.20', 'astm 0.25 ', 'barbey', 'caspers tin plate', 'continental can', 'crown cork and seal', 'demmier \#1', 'demmier \#10', 'engler', 'ford cup \#3', 'ford cup \#4', 'kinematic viscosity', 'mac michael', 'murphy varnish', 'parlin cup \#10', 'parlin cup \#15', 'parlin cup \#20', 'parlin cup \#25', 'parlin cup \#30', 'parlin cup \#7', 'pratt lambert a', 'pratt lambert b', 'pratt lambert c', 'pratt lambert d', 'pratt lambert e', 'pratt lambert f', 'pratt lambert g', 'pratt lambert h', 'pratt lambert i', 'redwood admiralty', 'redwood standard', 'saybolt furol', 'saybolt universal', 'scott', 'stormer 100 g load', 'westinghouse', 'zahn cup \#1', 'zahn cup \#2', 'zahn cup \#3', 'zahn cup \#4', 'zahn cup \#5']
Some of those scales are converted linearly; the rest use tabulated data and splines.
Because the conversion is performed by spline functions, a re-conversion of a value will not yield exactly the original value. However, it is quite close.
The method 'Saybolt universal' has a special formula implemented for its conversion, from [4]. It is designed for maximum backwards compatibility with prior experimental data. It is solved by newton's method when kinematic viscosity is desired as an output.
\[
S U S_{e q}=4.6324 \nu_{t}+\frac{\left[1.0+0.03264 \nu_{t}\right]}{\left.\left[\left(3930.2+262.7 \nu_{t}+23.97 \nu_{t}^{2}+1.646 \nu_{t}^{3}\right) \times 10^{-5}\right)\right]}
\]

\section*{References}
[1], [2], [3], [4], [5]

\section*{Examples}
```

>>> viscosity_converter(8.79, 'engler', 'parlin cup \#7')
52.5
>>> viscosity_converter(700, 'Saybolt Universal Seconds', 'kinematic viscosity')
0.00015108914751515542

```
chemicals.viscosity.viscosity_index(nu_40, nu_100, rounding=False)
Calculates the viscosity index of a liquid. Requires dynamic viscosity of a liquid at \(40^{\circ} \mathrm{C}\) and \(100^{\circ} \mathrm{C}\). Value may either be returned with or without rounding. Rounding is performed per the standard.
if nu_100 < 70:
\[
L, H=\operatorname{interp}\left(n u_{1} 00\right)
\]
else:
\[
\begin{aligned}
& L=0.8353 \nu_{100}^{2}+14.67 \nu_{100}-216 \\
& H=0.1684 \nu_{100}^{2}+11.85 \nu_{100}-97
\end{aligned}
\]
if nu_40 > H:
\[
V I=\frac{L-n u_{40}}{L-H} \cdot 100
\]
else:
\[
N=\frac{\ln (H)-\ln \left(\nu_{40}\right)}{\ln \left(\nu_{100}\right)}
\]
\[
V I=\frac{10^{N}-1}{0.00715}+100
\]

\section*{Parameters}
nu_40 [float] Dynamic viscosity of fluid at \(40^{\circ} \mathrm{C},\left[\mathrm{m}^{\wedge} 2 / \mathrm{s}\right.\) ]
nu_100 [float] Dynamic viscosity of fluid at \(100^{\circ} \mathrm{C},\left[\mathrm{m}^{\wedge} 2 / \mathrm{s}\right.\) ]
rounding [bool, optional] Whether to round the value or not.

\section*{Returns}

VI: float Viscosity index [-]

\section*{Notes}

VI is undefined for nu_100 under \(2 \mathrm{~mm}^{\wedge} 2 / \mathrm{s}\). None is returned if this is the case. Internal units are \(\mathrm{mm}^{\wedge} 2 / \mathrm{s}\). Higher values of viscosity index suggest a lesser decrease in kinematic viscosity as temperature increases.
Note that viscosity is a pressure-dependent property, and that the viscosity index is defined for a fluid at whatever pressure it is at. The viscosity index is thus also a function of pressure.

\section*{References}
[1]

Examples
```

>>> viscosity_index(73.3E-6, 8.86E-6, rounding=True)

```

92

\subsection*{1.35.11 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.viscosity.mu_data_Dutt_Prasad
Coefficient sfor chemicals.viscosity. Viswanath_Natarajan_3 from [1] for 100 fluids.
chemicals.viscosity.mu_data_VN3
Coefficients for chemicals.viscosity.Viswanath_Natarajan_3 from [1] with data for 432 fluids.
chemicals.viscosity.mu_data_VN2
Coefficients for chemicals.viscosity.Viswanath_Natarajan_2 from [1] with data for 135 fluids.
chemicals.viscosity.mu_data_VN2E
Coefficients for chemicals.viscosity.Viswanath_Natarajan_2_exponential from [1] with data for 14 fluids.
chemicals.viscosity.mu_data_Perrys_8E_2_313
A collection of 337 coefficient sets for chemicals.dippr.EQ101 from the DIPPR database published openly in [3].
chemicals.viscosity.mu_data_Perrys_8E_2_312
A collection of 345 coefficient sets for chemicals.dippr. EQ102 from the DIPPR database published openly in [3].
chemicals.viscosity.mu_data_VDI_PPDS_7
Coefficients for the model equation PPDS9, published openly in [2]. Provides no temperature limits, but has been designed for extrapolation. Extrapolated to low temperatures it provides a smooth exponential increase. However, for some chemicals such as glycerol, extrapolated to higher temperatures viscosity is predicted to increase above a certain point.
chemicals.viscosity.mu_data_VDI_PPDS_8
Coefficients for a tempereture polynomial ( T in Kelvin) developed by the PPDS, published openly in [2]. \(\mu=\) \(A+B T+C T^{2}+D T^{3}+E T^{4}\).

The structure of each dataframe is shown below:
```

In [1]: import chemicals
In [2]: chemicals.viscosity.mu_data_Dutt_Prasad
Out[2]:

|  | Chemical | A | B | C | Tmin | Tmax |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| CAS |  |  |  |  |  |  |
| $56-23-5$ | Carbon tetrachloride | -1.4708 | -324.45 | 71.19 | 273.0 | 373.0 |
| $60-29-7$ | Ethyl ether | -4.4735 | -3623.26 | -648.55 | 273.0 | 373.0 |
| $62-53-3$ | Aniline | -1.1835 | -224.31 | 170.82 | 268.0 | 393.0 |
| $64-17-5$ | Ethyl alcohol | -2.8857 | -1032.53 | -55.95 | 248.0 | 348.0 |
| $64-18-6$ | Formic acid | -1.4150 | -297.43 | 114.74 | 281.0 | 373.0 |
| $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ | $\ldots$ |
| $629-59-4$ | Tetra decane | -1.4424 | -350.81 | 100.18 | 283.0 | 373.0 |
| $629-62-9$ | Penta decane | -1.4073 | -348.84 | 105.48 | 293.0 | 373.0 |
| $629-78-7$ | Hepta decane | -1.7847 | -577.32 | 51.72 | 303.0 | 553.0 |
| $693-02-7$ | 1 - Hexyne | -3.0941 | -1404.92 | -233.99 | 293.0 | 333.0 |
| $3744-21-6$ | $2,2-$ Dimethyl propane | -0.9128 | -30.15 | 202.98 | 258.0 | 283.0 |

[100 rows x 6 columns]
In [3]: chemicals.viscosity.mu_data_VN3
Out[3]:
CAS
57-10-3 Palmitic acid ... 370.0
57-50-1 Sucrose ... 330.0
60-12-8 Phenethyl alcohol ... 380.0
60-35-5 Acetamide ... 500.0
62-53-3 Aniline ... 460.0
...
66538-96-3 1,2,3,4 - Tetrahydro -6 - butyl -hexyl naphtha... ... 380.0
87077-20-1 2-Methyl - 7 -heptanol ... 380.0
99332-99-7 Hexyl thiohexanoate ... 370.0
101433-18-5 Ethyl tetra decanol ... 380.0
109309-32-2 2,2-Di - p - toly butane ... 480.0

```
[432 rows x 7 columns]

In [4]: chemicals.viscosity.mu_data_VN2
Out [4]:
CAS
\(\begin{array}{llll}\text { Formula } & \ldots & \text { Tmin } & \text { Tmax } \\ & \ldots & & \end{array}\)
(continues on next page)

(continued from previous page)

[345 rows x 7 columns]
In [8]: chemicals.viscosity.mu_data_VDI_PPDS_7
Out [8]:
Chemical Formula
CAS


\section*{[271 rows x 7 columns]}

In [9]: chemicals.viscosity.mu_data_VDI_PPDS_8
Out [9]:
\begin{tabular}{|c|c|c|c|c|}
\hline & Chemical & A & D & E \\
\hline \multicolumn{5}{|l|}{CAS} \\
\hline 50-00-0 & Formaldehyde & -8.285000e-07 & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline 56-23-5 & Carbon tetrachloride & -7.132000e-07 & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline 56-81-5 & Glycerol & -1.460000e-08 & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline 60-29-7 & Diethyl ether & -8.933000e-07 & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline 62-53-3 & Aniline & -9.488000e-07 & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline & & & & \\
\hline 10097-32-2 & Bromine & \(1.948300 \mathrm{e}-06\) & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline 10102-43-9 & Nitric oxide & -9.105000e-07 & \(4.240000 \mathrm{e}-14\) & -1.020000e-17 \\
\hline 10102-44-0 & Nitrogen dioxide & -2.285050e-05 & \(1.713400 \mathrm{e}-13\) & -4.920000e-17 \\
\hline 10544-72-6 & Dinitrogentetroxide & -8.683000e-07 & \(0.000000 \mathrm{e}+00\) & \(0.000000 \mathrm{e}+00\) \\
\hline 132259-10-0 & Air & -1.702000e-07 & \(4.960000 \mathrm{e}-14\) & -1.388000e-17 \\
\hline
\end{tabular}
(continues on next page)

\subsection*{1.36 Density/Volume (chemicals.volume)}

This module contains various volume/density estimation routines, dataframes of fit coefficients, and mixing rules.
For reporting bugs, adding feature requests, or submitting pull requests, please use the GitHub issue tracker.
- Pure Low Pressure Liquid Correlations
- Pure High Pressure Liquid Correlations
- Liquid Mixing Rules
- Gas Correlations
- Pure Solid Correlations
- Pure Component Liquid Fit Correlations
- Pure Component Solid Fit Correlations
- Fit Coefficients

\subsection*{1.36.1 Pure Low Pressure Liquid Correlations}
chemicals.volume.Rackett ( \(T, T c, P c, Z c\) )
Calculates saturation liquid volume, using Rackett CSP method and critical properties.
The molar volume of a liquid is given by:
\[
V_{s}=\frac{R T_{c}}{P_{c}} Z_{c}^{\left[1+\left(1-T / T_{c}\right)^{2 / 7}\right]}
\]

Units are all currently in \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) - this can be changed to \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\)

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
Zc [float] Critical compressibility of fluid, [-]

\section*{Returns}

Vs [float] Saturation liquid volume, \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Notes}

According to Reid et. al, underpredicts volume for compounds with \(\mathrm{Zc}<0.22\)

\section*{References}
[1]

\section*{Examples}

Propane, example from the API Handbook
>>> from chemicals.utils import Vm_to_rho
>>> Vm_to_rho(Rackett(272.03889, 369.83, 4248000.0, 0.2763), 44.09562)
531.3221411755724

\section*{chemicals.volume. \(\operatorname{COSTALD}(T, T c, V c\), omega \()\)}

Calculate saturation liquid density using the COSTALD CSP method.
A popular and accurate estimation method. If possible, fit parameters are used; alternatively critical properties work well.
The density of a liquid is given by:
\[
\begin{gathered}
V_{s}=V^{*} V^{(0)}\left[1-\omega_{S R K} V^{(\delta)}\right] \\
V^{(0)}=1-1.52816\left(1-T_{r}\right)^{1 / 3}+1.43907\left(1-T_{r}\right)^{2 / 3}-0.81446\left(1-T_{r}\right)+0.190454\left(1-T_{r}\right)^{4 / 3} \\
V^{(\delta)}=\frac{-0.296123+0.386914 T_{r}-0.0427258 T_{r}^{2}-0.0480645 T_{r}^{3}}{T_{r}-1.00001}
\end{gathered}
\]

Units are that of critical or fit constant volume.

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]. This parameter is alternatively a fit parameter
omega [float] (ideally SRK) Acentric factor for fluid, [-] This parameter is alternatively a fit parameter.

\section*{Returns}

Vs [float] Saturation liquid volume

\section*{Notes}

196 constants are fit to this function in [1]. Range: \(0.25<\operatorname{Tr}<0.95\), often said to be to 1.0
This function has been checked with the API handbook example problem.

\section*{References}
[1]

\section*{Examples}

Propane, from an example in the API Handbook:
>>> from chemicals.utils import Vm_to_rho
>>> Vm_to_rho(COSTALD(272.03889, 369.83333, 0.20008161E-3, 0.1532), 44.097)
530.3009967969844
chemicals.volume.Yen_Woods_saturation \((T, T c, V c, Z c)\)
Calculates saturation liquid volume, using the Yen and Woods [1] CSP method and a chemical's critical properties.
The molar volume of a liquid is given by:
\[
\begin{gathered}
V c / V s=1+A\left(1-T_{r}\right)^{1 / 3}+B\left(1-T_{r}\right)^{2 / 3}+D\left(1-T_{r}\right)^{4 / 3} \\
D=0.93-B \\
A=17.4425-214.578 Z_{c}+989.625 Z_{c}^{2}-1522.06 Z_{c}^{3} \\
B=-3.28257+13.6377 Z_{c}+107.4844 Z_{c}^{2}-384.211 Z_{c}^{3} \text { if } Z c \leq 0.26 \\
B=60.2091-402.063 Z_{c}+501.0 Z_{c}^{2}+641.0 Z_{c}^{3} \text { if } Z c \geq 0.26
\end{gathered}
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
Zc [float] Critical compressibility of fluid, [-]

\section*{Returns}

Vs [float] Saturation liquid volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Notes}

Original equation was in terms of density, but it is converted here.
No example has been found, nor are there points in the article. However, it is believed correct. For compressed liquids with the Yen-Woods method, see the YenWoods_compressed function.

\section*{References}
[1]

\section*{Examples}
>>> Yen_Woods_saturation(300, 647.14, 55.45E-6, 0.245)
\(1.769533076529574 \mathrm{e}-05\)

\section*{chemicals.volume.Yamada_Gunn ( \(T, T c, P c\), omega)}

Calculates saturation liquid volume, using Yamada and Gunn CSP method and a chemical's critical properties and acentric factor.

The molar volume of a liquid is given by:
\[
V_{s}=\frac{R T_{c}}{P_{c}}(0.29056-0.08775 \omega)^{\left[1+\left(1-T / T_{c}\right)^{2 / 7}\right]}
\]

Units are in \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\).

\section*{Parameters}

T [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

Vs [float] saturation liquid volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Notes}

This equation is an improvement on the Rackett equation. This is often presented as the Rackett equation. The acentric factor is used here, instead of the critical compressibility A variant using a reference fluid also exists

\section*{References}
[1], [2]

\section*{Examples}
```

>>> Yamada_Gunn(300, 647.14, 22048320.0, 0.245)

```
\(2.188284384699659 \mathrm{e}-05\)
chemicals.volume.Townsend_Hales ( \(T, T c, V c\), omega)
Calculates saturation liquid density, using the Townsend and Hales CSP method as modified from the original Riedel equation. Uses chemical critical volume and temperature, as well as acentric factor
The density of a liquid is given by:
\[
V s=V_{c} /\left(1+0.85\left(1-T_{r}\right)+(1.692+0.986 \omega)\left(1-T_{r}\right)^{1 / 3}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]

Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ] omega [float] Acentric factor for fluid, [-]

\section*{Returns}

Vs [float] Saturation liquid volume, \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Notes}

The requirement for critical volume and acentric factor requires all data.

\section*{References}
[1]

\section*{Examples}
>>> Townsend_Hales(300, 647.14, 55.95E-6, 0.3449)
\(1.8007361992619923 \mathrm{e}-05\)
chemicals.volume.Bhirud_normal ( \(T, T c, P c\), omega)
Calculates saturation liquid density using the Bhirud [1] CSP method. Uses Critical temperature and pressure and acentric factor.

The density of a liquid is given by:
\[
\begin{gathered}
\ln \frac{P_{c}}{\rho R T}=\ln U^{(0)}+\omega \ln U^{(1)} \\
\ln U^{(0)}=1.39644-24.076 T_{r}+102.615 T_{r}^{2}-255.719 T_{r}^{3}+355.805 T_{r}^{4}-256.671 T_{r}^{5}+75.1088 T_{r}^{6} \\
\ln U^{(1)}=13.4412-135.7437 T_{r}+533.380 T_{r}^{2}-1091.453 T_{r}^{3}+1231.43 T_{r}^{4}-728.227 T_{r}^{5}+176.737 T_{r}^{6}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [ Pa ]
omega [float] Acentric factor for fluid, [-]

\section*{Returns}

Vm [float] Saturated liquid molar volume, \(\left[\mathrm{mol} / \mathrm{m}^{\wedge} 3\right.\) ]

\section*{Notes}

Claimed inadequate by others.
An interpolation table for \(\ln \mathrm{U}\) values are used from \(\mathrm{Tr}=0.98-1.000\). Has terrible behavior at low reduced temperatures.

\section*{References}
[1]

\section*{Examples}

Pentane
>>> Bhirud_normal(280.0, 469.7, 33.7E5, 0.252)
0.00011249657842514176
chemicals.volume.Campbell_Thodos (T, Tb, Tc, \(P C, M W\), dipole=0.0, has_hydroxyl=False) Calculate saturation liquid density using the Campbell-Thodos [1] CSP method.
An old and uncommon estimation method.
\[
\begin{gathered}
V_{s}=\frac{R T_{c}}{P_{c}} Z_{R A}{ }^{\left[1+\left(1-T_{r}\right)^{2 / 7}\right]} \\
Z_{R A}=\alpha+\beta\left(1-T_{r}\right) \\
\alpha=0.3883-0.0179 s \\
s=T_{b r} \frac{\ln P_{c}}{\left(1-T_{b r}\right)} \\
\beta=0.00318 s-0.0211+0.625 \Lambda^{1.35} \\
\Lambda=\frac{P_{c}^{1 / 3}}{M W^{1 / 2} T_{c}^{5 / 6}}
\end{gathered}
\]

For polar compounds:
\[
\begin{gathered}
\theta=P_{c} \mu^{2} / T_{c}^{2} \\
\alpha=0.3883-0.0179 s-130540 \theta^{2.41} \\
\beta=0.00318 s-0.0211+0.625 \Lambda^{1.35}+9.74 \times 10^{6} \theta^{3.38}
\end{gathered}
\]

Polar Combounds with hydroxyl groups (water, alcohols)
\[
\begin{aligned}
& \alpha=\left[0.690 T_{b r}-0.3342+\frac{5.79 \times 10^{-10}}{T_{b r}^{32.75}}\right] P_{c}^{0.145} \\
& \beta=0.00318 s-0.0211+0.625 \Lambda^{1.35}+5.90 \Theta^{0.835}
\end{aligned}
\]

\section*{Parameters}

T [float] Temperature of fluid [K]
Tb [float] Boiling temperature of the fluid [K]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
MW [float] Molecular weight of the fluid [ \(\mathrm{g} / \mathrm{mol}\) ]
dipole [float, optional] Dipole moment of the fluid [debye]
has_hydroxyl [bool, optional] Swith to use the hydroxyl variant for polar fluids

\section*{Returns}

Vs [float] Saturation liquid volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Notes}

If a dipole is provided, the polar chemical method is used. The paper is an excellent read. Pc is internally converted to atm.

\section*{References}
[1]

\section*{Examples}

Ammonia, from [1].
>>> Campbell_Thodos(T=405.45, Tb=239.82, Tc=405.45, Pc=111.7*101325, MW=17.03, 七
\(\rightarrow\) dipole=1.47)
\(7.347366126245 \mathrm{e}-05\)
chemicals.volume. SNMO ( \(T, T c, V c\), omega, delta_SRK=None)
Calculates saturated liquid density using the Mchaweh, Moshfeghian model [1]. Designed for simple calculations.
\[
\begin{gathered}
V_{s}=V_{c} /\left(1+1.169 \tau^{1 / 3}+1.818 \tau^{2 / 3}-2.658 \tau+2.161 \tau^{4 / 3}\right. \\
\tau=1-\frac{\left(T / T_{c}\right)}{\alpha_{S R K}} \\
\alpha_{S R K}=\left[1+m\left(1-\sqrt{T / T_{C}}\right]^{2}\right. \\
m=0.480+1.574 \omega-0.176 \omega^{2}
\end{gathered}
\]

If the fit parameter delta_SRK is provided, the following is used:
\[
V_{s}=V_{C} /\left(1+1.169 \tau^{1 / 3}+1.818 \tau^{2 / 3}-2.658 \tau+2.161 \tau^{4 / 3}\right) /\left[1+\delta_{S R K}\left(\alpha_{S R K}-1\right)^{1 / 3}\right]
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
Vc [float] Critical volume of fluid [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]
omega [float] Acentric factor for fluid, [-]
delta_SRK [float, optional] Fitting parameter [-]

\section*{Returns}

Vs [float] Saturation liquid volume, \(\left[\mathrm{m}^{\wedge} 3 / \mathrm{mol}\right]\)

\section*{Notes}

73 fit parameters have been gathered from the article.

\section*{References}
[1]

\section*{Examples}

Argon, without the fit parameter and with it. Tabulated result in Perry's is \(3.4613 \mathrm{e}-05\). The fit increases the error on this occasion.
```

>>> SNM0(121, 150.8, 7.49e-05, -0.004)
3.440225640273e-05
>> SNMO(121, 150.8, 7.49e-05, -0.004, -0.03259620)
3.493288100008e-05

```

\subsection*{1.36.2 Pure High Pressure Liquid Correlations}

\section*{chemicals.volume.COSTALD_compressed ( \(T, P, P s a t, T c, P c\), omega, \(V s)\)}

Calculates compressed-liquid volume, using the COSTALD [1] CSP method and a chemical's critical properties.
The molar volume of a liquid is given by:
\[
\begin{gathered}
V=V_{s}\left(1-C \ln \frac{B+P}{B+P^{s a t}}\right) \\
\frac{B}{P_{c}}=-1+a \tau^{1 / 3}+b \tau^{2 / 3}+d \tau+e \tau^{4 / 3} \\
e=\exp \left(f+g \omega_{S R K}+h \omega_{S R K}^{2}\right) \\
C=j+k \omega_{S R K}
\end{gathered}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
\(\mathbf{P}\) [float] Pressure of fluid [Pa]
Psat [float] Saturation pressure of the fluid [Pa]
Tc [float] Critical temperature of fluid [K]
Pc [float] Critical pressure of fluid [Pa]
omega [float] (ideally SRK) Acentric factor for fluid, [-] This parameter is alternatively a fit parameter.
Vs [float] Saturation liquid volume, [m^3/mol]

\section*{Returns}

V_dense [float] High-pressure liquid volume, [m^3/mol]

\section*{Notes}

Original equation was in terms of density, but it is converted here.
The example is from DIPPR, and exactly correct. This is DIPPR Procedure 4C: Method for Estimating the Density of Pure Organic Liquids under Pressure.

\section*{References}
[1]

\section*{Examples}
>>> COSTALD_compressed(303., 9.8E7, 85857.9, 466.7, 3640000.0, 0.281, 0.000105047)
9.287482879788505e-05

\subsection*{1.36.3 Liquid Mixing Rules}

\section*{chemicals.volume.Amgat ( \(x s, V m s\) )}

Calculate mixture liquid density using the Amgat mixing rule. Highly inacurate, but easy to use. Assumes idea liquids with no excess volume. Average molecular weight should be used with it to obtain density.
\[
V_{m i x}=\sum_{i} x_{i} V_{i}
\]
or in terms of density:
\[
\rho_{m i x}=\sum \frac{x_{i}}{\rho_{i}}
\]

\section*{Parameters}
xs [array] Mole fractions of each component, []
Vms [array] Molar volumes of each fluids at conditions [m^3/mol]

\section*{Returns}

Vm [float] Mixture liquid volume [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Notes}

Units are that of the given volumes. It has been suggested to use this equation with weight fractions, but the results have been less accurate.

\section*{Examples}
```

>>> Amgat([0.5, 0.5], [4.057e-05, 5.861e-05])
4.9590000000000005e-05

```
chemicals.volume.Rackett_mixture ( \(T, x s, M W s, T c s, P c s, Z r s)\)
Calculate mixture liquid density using the Rackett-derived mixing rule as shown in [2].
\[
V_{m}=\sum_{i} \frac{x_{i} T_{c i}}{M W_{i} P_{c i}} Z_{R, m}^{\left(1+\left(1-T_{r}\right)^{2 / 7}\right)} R \sum_{i} x_{i} M W_{i}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of liquid [K]
xs: list Mole fractions of each component, []
MWs [list] Molecular weights of each component [ \(\mathrm{g} / \mathrm{mol}\) ]
Tes [list] Critical temperatures of each component [K]
Pcs [list] Critical pressures of each component [Pa]
Zrs [list] Rackett parameters of each component []

\section*{Returns}

Vm [float] Mixture liquid volume [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Notes}

Model for pure compounds in [1] forms the basis for this model, shown in [2]. Molecular weights are used as weighing by such has been found to provide higher accuracy in [2]. The model can also be used without molecular weights, but results are somewhat different.

As with the Rackett model, critical compressibilities may be used if Rackett parameters have not been regressed.
Critical mixture temperature, and compressibility are all obtained with simple mixing rules.

\section*{References}
[1], [2]

\section*{Examples}

Calculation in [2] for methanol and water mixture. Result matches example.
```

>>> Rackett_mixture(T=298., xs=[0.4576, 0.5424], MWs=[32.04, 18.01], Tcs=[512.58,, 七
4647.29], Pcs=[8.096E6, 2.209E7], Zrs=[0.2332, 0.2374])
2.6252894930056885e-05

```
chemicals.volume.COSTALD_mixture ( \(x s, T, T c s, V c s\), omegas)
Calculate mixture liquid density using the COSTALD CSP method.
A popular and accurate estimation method. If possible, fit parameters are used; alternatively critical properties work well.

The mixing rules giving parameters for the pure component COSTALD equation are:
\[
\begin{gathered}
T_{c m}=\frac{\sum_{i} \sum_{j} x_{i} x_{j}\left(V_{i j} T_{c i j}\right)}{V_{m}} \\
V_{m}=0.25\left[\sum x_{i} V_{i}+3\left(\sum x_{i} V_{i}^{2 / 3}\right)\left(\sum_{i} x_{i} V_{i}^{1 / 3}\right)\right]
\end{gathered}
\]
\[
\begin{aligned}
V_{i j} T_{c i j} & =\left(V_{i} T_{c i} V_{j} T_{c j}\right)^{0.5} \\
\omega & =\sum_{i} z_{i} \omega_{i}
\end{aligned}
\]

\section*{Parameters}
xs: list Mole fractions of each component
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tes [list] Critical temperature of fluids [K]
Ves [list] Critical volumes of fluids [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]. This parameter is alternatively a fit parameter
omegas [list] (ideally SRK) Acentric factor of all fluids, [-] This parameter is alternatively a fit parameter.

\section*{Returns}

Vs [float] Saturation liquid mixture volume

\section*{Notes}

Range: \(0.25<\mathrm{Tr}<0.95\), often said to be to 1.0 No example has been found. Units are that of critical or fit constant volume.

\section*{References}
[1]

\section*{Examples}
```

>>> COSTALD_mixture([0.4576, 0.5424], 298., [512.58, 647.29], [0.000117, 5.6e-05],,

```
\(\rightarrow[0.559,0.344])\)
\(2.7065887732713534 \mathrm{e}-05\)

\subsection*{1.36.4 Gas Correlations}

Gas volumes are predicted with one of:
1) An equation of state
2) A virial coefficient model
3) The ideal gas law

Equations of state do much more than predict volume however. An implementation of many of them can be found in thermo.

Virial functions are implemented in chemicals.virial.
chemicals.volume.ideal_gas \((T, P)\)
Calculates ideal gas molar volume. The molar volume of an ideal gas is given by:
\[
V=\frac{R T}{P}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
\(\mathbf{P}\) [float] Pressure of fluid [Pa]

\section*{Returns}
\(\mathbf{V}\) [float] Gas volume, [m^3/mol]

\section*{Examples}
>>> ideal_gas(298.15, 101325.)
0.024465403697038125

\subsection*{1.36.5 Pure Solid Correlations}

Solid density does not depend on pressure significantly, and unless operating in the geochemical or astronomical domain is normally neglected.
chemicals.volume. Goodman ( \(T, T t, V m l\) )
Calculates solid density at T using the simple relationship by a member of the DIPPR.
The molar volume of a solid is given by:
\[
\frac{1}{V_{m}}=\left(1.28-0.16 \frac{T}{T_{t}}\right) \frac{1}{V m_{L}\left(T_{t}\right)}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tt [float] Triple temperature of fluid [K]
Vml [float] Liquid molar volume of the organic liquid at the triple point, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Returns}

Vms [float] Solid molar volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) ]

\section*{Notes}

Works to the next solid transition temperature or to approximately 0.3Tt.

\section*{References}
[1]

\section*{Examples}

Decane at 200 K :
```

>>> Goodman(200, 243.225, 0.00023585)
0.0002053665090860923

```

\subsection*{1.36.6 Pure Component Liquid Fit Correlations}

\section*{chemicals.volume.Rackett_fit( \(T, T c, r h o c, ~ b, ~ n, ~ M W=N o n e) ~\)}

Calculates saturation liquid volume, using the Rackett equation form and a known or estimated critical temperature and density as well as fit parameters \(b\) and \(n\).

The density of a liquid is given by:
\[
\rho_{\text {sat }}=\rho_{c} b^{-\left(1-\frac{T}{T_{c}}\right)^{n}}
\]

The density is then converted to a specific volume by taking its inverse.
Note that the units of this equation in some sources are \(\mathrm{kg} / \mathrm{m}^{\wedge} 3, \mathrm{~g} / \mathrm{mL}\) in others, and \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) in others. If the units for the coefficients are in molar units, do NOT provide \(M W\) or an incorrect value will be returned. If the units are mass units and \(M W\) is not provided, the output will have the same units as rhoc.

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
rhoc [float] Critical density of fluid, often a fit parameter only [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
b [float] Fit parameter, [-]
n [float] Fit parameter, [-]
MW [float, optional] Molecular weight, \([\mathrm{g} / \mathrm{mol}]\)

\section*{Returns}

Vs [float] Saturation liquid volume, [ \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\) if MW given; \(\mathrm{m}^{\wedge} 3 / \mathrm{kg}\) otherwise]

\section*{References}
[1], [2]

\section*{Examples}

Input sample from NIST (naphthalene) ( \(\mathrm{m}^{\wedge} 3 / \mathrm{kg}\) ):
>> Rackett_fit(T=400.0, \(\mathrm{Tc}=748.402\), rhoc=314.629, \(\mathrm{b}=0.257033\), \(\mathrm{n}=0.280338\) )
0.00106174320755

Parameters in Yaws form (butane) (note the 1000 multiplier on rhoc, called \(A\) in Yaws) ( \(\mathrm{m}^{\wedge} 3 / \mathrm{kg}\) ):
```

>>> Rackett_fit(T=298.15, Tc=425.18, rhoc=0.2283*1000, b=0.2724, n=0.2863)
0.00174520519958

```

Same Yaws point, with MW provided:
```

>>> Rackett_fit(T=298.15, Tc=425.18, rhoc=0.2283*1000, b=0.2724, n=0.2863, MW=58.
๑123)
0.00010143656181

```
chemicals.volume.volume_VDI_PPDS ( \(T, T c\), \(r h o c, a, b, c, d, M W=N o n e)\)
Calculates saturation liquid volume, using the critical properties and fitted coefficients from [1]. This is also known as the PPDS equation 10 or PPDS10.
\[
\rho_{\text {mass }}=\rho_{c}+a \tau^{0.35}+b \tau^{2 / 3}+c \tau+d \tau^{4 / 3}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Te [float] Critical temperature of fluid [K]
rhoc [float] Critical density of fluid [ \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) ]
\(\mathbf{a , b , c , d}\) [float] Fitted coefficients [-]
MW [float, optional] Molecular weight of chemical [ \(\mathrm{g} / \mathrm{mol}\) ]

\section*{Returns}

Vs [float] Saturation liquid molar volume or density, [m^3/mol if MW given; \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) otherwise]

\section*{References}
[1]

\section*{Examples}

Calculate density of nitrogen in \(\mathrm{kg} / \mathrm{m} 3\) at 300 K :
>> volume_VDI_PPDS (300, 126.19, 313, 470.922, 493.251, -560.469, 389.611)
313.0

Calculate molar volume of nitrogen in \(\mathrm{m} 3 / \mathrm{mol}\) at 300 K :
```

>>> volume_VDI_PPDS(300, 126.19, 313, 470.922, 493.251, -560.469, 389.611, 28.01)
8.9488817891e-05

```
chemicals.volume.TDE_VDNS_rho ( \(T, T c, r h o c, a 1, a 2, a 3, a 4, M W=N o n e)\)
Calculates saturation liquid volume, using the critical properties and fitted coefficients in the TDE VDNW form from [1].
\[
\rho_{\text {mass }}=\rho_{c}+a \tau^{0.35}+b \tau+c \tau^{2}+d \tau^{3}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Tc [float] Critical temperature of fluid [K]
rhoc [float] Critical density of fluid \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right.\) ]
a1 [float] Regression parameter, [-]
\(\mathbf{a} 2\) [float] Regression parameter, [-]
a3 [float] Regression parameter, [-]
a4 [float] Regression parameter, [-]
MW [float, optional] Molecular weight of chemical [g/mol]

\section*{Returns}

Vs [float] Saturation liquid molar volume or density, [m^3/mol if MW given; \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) otherwise]

\section*{References}
[1]

\section*{Examples}
>>> TDE_VDNS_rho(T=400.0, Tc=772.999, rhoc=320.037, a1=795.092, a2=-169.132, a3=448. \(\rightarrow 929\), a4=-102.931)
947.4906064903
chemicals.volume.PPDS17 ( \(T, T c, a 0, a l, a 2, M W=\) None \()\)
Calculates saturation liquid volume, using the critical temperature and fitted coefficients in the PPDS17 form in [1].
\[
\rho_{\text {mass }}=\frac{1}{a_{0}\left(a_{1}+a_{2} \tau\right)^{\left(1+\tau^{2 / 7}\right)}}
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of fluid [K]
Te [float] Critical temperature of fluid [K]
a0 [float] Regression parameter, [-]
a1 [float] Regression parameter, [-]
\(\mathbf{a} 2\) [float] Regression parameter, [-]
MW [float, optional] Molecular weight of chemical [g/mol]

\section*{Returns}

Vs [float] Saturation liquid molar volume or density, [m^3/mol if MW given; \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) otherwise]

\section*{References}
[1]

\section*{Examples}

Coefficients for the liquid density of benzene from [1] at 300 K :
```

>>> PPDS17(300, 562.05, a0=0.0115508, a1=0.281004, a2=-0.00635447)

```
871.520087707

\subsection*{1.36.7 Pure Component Solid Fit Correlations}

\section*{chemicals.volume.CRC_inorganic ( \(T\), rho0, \(k, T m, M W=N o n e)\)}

Calculates liquid density of a molten element or salt at temperature above the melting point. Some coefficients are given nearly up to the boiling point.

The mass density of the inorganic liquid is given by:
\[
\rho=\rho_{0}-k\left(T-T_{m}\right)
\]

\section*{Parameters}
\(\mathbf{T}\) [float] Temperature of the liquid, \([\mathrm{K}]\)
rho0 [float] Mass density of the liquid at \(\mathrm{Tm},\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]\)
\(\mathbf{k}\) [float] Linear temperature dependence of the mass density, \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3 / \mathrm{K}\right]\)
Tm [float] The normal melting point, used in the correlation [K]
MW [float, optional] Molecular weight of chemical [g/mol]

\section*{Returns}
rho [float] Mass density of molten metal or salt, [m^3/mol if MW given; \(\mathrm{kg} / \mathrm{m}^{\wedge} 3\) otherwise]

\section*{Notes}
[1] has units of \(\mathrm{g} / \mathrm{mL}\). While the individual densities could have been converted to molar units, the temperature coefficient could only be converted by refitting to calculated data. To maintain compatibility with the form of the equations, this was not performed.

This linear form is useful only in small temperature ranges. Coefficients for one compound could be used to predict the temperature dependence of density of a similar compound.

\section*{References}
[1]

\section*{Examples}
```

>>> CRC_inorganic(300, 2370.0, 2.687, 239.08)

```
2206.30796

\subsection*{1.36.8 Fit Coefficients}

All of these coefficients are lazy-loaded, so they must be accessed as an attribute of this module.
chemicals.volume.rho_data_COSTALD
Coefficients for the COSTALD method from [3]; 192 fluids have coefficients published.
chemicals.volume.rho_data_SNMO
Coefficients for the SNMO method for 73 fluids from [2].
chemicals.volume.rho_data_Perry_8E_105_l
Coefficients for chemicals.dippr.EQ105 from [1] for 344 fluids. Note this is in terms of molar density; to obtain molar volume, invert the result!
chemicals.volume.rho_data_VDI_PPDS_2
Coefficients in [5] developed by the PPDS using chemicals.dippr.EQ116 but in terms of mass density \(\left[\mathrm{kg} / \mathrm{m}^{\wedge} 3\right]\); Valid up to the critical temperature, and extrapolates to very low temperatures well.
chemicals.volume.rho_data_CRC_inorg_l
Single-temperature coefficient linear model in terms of mass density for the density of inorganic liquids. Data is available for 177 fluids normally valid over a narrow range above the melting point, from [4]; described in CRC_inorganic.
chemicals.volume.rho_data_CRC_inorg_l_const Constant inorganic liquid molar volumes published in [4].
chemicals.volume.rho_data_CRC_inorg_s_const
Constant solid densities molar volumes published in [4].
chemicals.volume.rho_data_CRC_virial
Coefficients for a tempereture polynomial (T in Kelvin) for the second \(B\) virial coefficient published in [4]. The form of the equation is \(B=\left(a_{1}+t\left(a_{2}+t\left(a_{3}+t\left(a_{4}+a_{5} t\right)\right)\right)\right) \times 10^{-6}\) with \(t=\frac{298.15}{T}-1\) and then \(B\) will be in units of \(\mathrm{m}^{\wedge} 3 / \mathrm{mol}\).

The structure of each dataframe is shown below:
\begin{tabular}{|c|c|c|c|c|}
\hline \multicolumn{5}{|l|}{In [1]: import chemicals} \\
\hline \multicolumn{5}{|l|}{In [2]: chemicals.volume.rho_data_COSTALD} \\
\hline \multicolumn{5}{|l|}{Out[2]:} \\
\hline & Chemical & omega_SRK & Vchar & Z_RA \\
\hline \multicolumn{5}{|l|}{CAS} \\
\hline 60-29-7 & ethyl ether & 0.2800 & 0.000281 & 0.2632 \\
\hline 64-17-5 & ethyl alcohol & 0.6378 & 0.000175 & 0.2502 \\
\hline 67-56-1 & methyl alcohol & 0.5536 & 0.000120 & 0.2334 \\
\hline 67-63-0 & isopropyl alcohol & 0.6637 & 0.000231 & 0.2493 \\
\hline 67-64-1 & acetone & 0.3149 & 0.000208 & 0.2477 \\
\hline & & & & \\
\hline 14752-75-1 & heptadecylbenzene & 0.9404 & 0.001146 & NaN \\
\hline 30453-31-7 & ethyl n-propyl disulfide & 0.3876 & 0.000440 & 0.2662 \\
\hline 33672-51-4 & propyl isopropyl disulfide & 0.4059 & 0.000502 & 0.2680 \\
\hline 53966-36-2 & ethyl isopropyl disulfide & 0.3556 & 0.000439 & 0.2711 \\
\hline 61828-04-4 & tricosylbenzene & 1.1399 & 0.001995 & NaN \\
\hline \multicolumn{5}{|l|}{[192 rows x 4 columns]} \\
\hline \multicolumn{5}{|l|}{In [3]: chemicals.volume.rho_data_SNMO} \\
\hline \multicolumn{5}{|l|}{Out[3]:} \\
\hline & Chemical & delta_SRK & & \\
\hline \multicolumn{5}{|l|}{CAS} \\
\hline 56-23-5 & Tetrachlouromethane, R-10 & -0.013152 & & \\
\hline 60-29-7 & Ethylether & 0.001062 & & \\
\hline 64-19-7 & Acetic acid & -0.010347 & & \\
\hline 65-85-0 & Benzoic acid & 0.026866 & & \\
\hline 67-56-1 & Methanol & 0.007195 & & \\
\hline . \(\cdot\) & & & & \\
\hline 7727-37-9 & Nitrogen & -0.007946 & & \\
\hline 7782-39-0 & Deuterium & -0.053345 & & \\
\hline 7782-41-4 & Flourine & -0.030398 & & \\
\hline 7782-44-7 & Oxygen & -0.027049 & & \\
\hline
\end{tabular}
(continued from previous page)

[344 rows x 7 columns]

In [5]: chemicals.volume.rho_data_VDI_PPDS_2
Out[5]:
\begin{tabular}{lrrlrr} 
& Chemical & MW & \(\ldots\) & C & D \\
CAS & & \(\ldots\) & & \\
\(50-00-0\) & Formaldehyde & 30.03 & \(\ldots\) & 245.3425 & 43.9601 \\
\(56-23-5\) & Carbon tetrachloride & 153.82 & \(\ldots\) & 535.7568 & -28.0071 \\
\(56-81-5\) & Glycerol & 92.09 & \(\ldots\) & 1429.7634 & -527.7710 \\
\(60-29-7\) & Diethyl ether & 74.12 & \(\ldots\) & -489.2726 & 486.7458 \\
\(62-53-3\) & Aniline & 93.13 & \(\ldots\) & 242.0930 & 0.7157 \\
\(\ldots\) & \(\ldots\) & \(\ldots\). & \(\ldots\) & \(\ldots\) & \(\ldots\) \\
\(10097-32-2\) & Bromine & 159.82 & \(\ldots\) & 676.7593 & 15.3973 \\
\(10102-43-9\) & Nitric oxide & 30.01 & \(\ldots\) & 2252.1437 & -1031.3210 \\
\(10102-44-0\) & Nitrogen dioxide & 46.01 & \(\ldots\) & 2233.6217 & -968.0655 \\
\(10544-72-6\) & Dinitrogentetroxide & 92.01 & \(\ldots\) & 604.1720 & -135.9384 \\
\(132259-10-0\) & Air & 28.96 & \(\ldots\) & -841.3265 & 495.5129
\end{tabular}
[272 rows x 8 columns]
In [6]: chemicals.volume.rho_data_CRC_inorg_l
Out [6]:
\begin{tabular}{lrrrrrrr} 
& Chemical & MW & rho & k & Tm & Tmax \\
CAS & & & & & & \\
\(497-19-8\) & Sodium carbonate & 105.989 & 1972.0 & 0.448 & 1129.15 & 1277.15 \\
\(584-09-8\) & Rubidium carbonate & 230.945 & 2840.0 & 0.640 & 1110.15 & 1280.15 \\
\(7429-90-5\) & Aluminum & 26.982 & 2377.0 & 0.311 & 933.47 & 1190.15 \\
\(7429-91-6\) & Dysprosium & 162.500 & 8370.0 & 1.430 & 1685.15 & 1813.15 \\
\(7439-88-5\) & Iridium & 192.217 & 19000.0 & 0.000 & 2719.15 & 2739.15 \\
\(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) & \(\ldots\) \\
\(13572-98-0\) & Gadolinium(III) iodide & 537.960 & 4120.0 & 0.908 & 1203.15 & 1305.15 \\
\(13709-38-1\) & Lanthanum fluoride & 195.900 & 4589.0 & 0.682 & 1766.15 & 2450.15
\end{tabular}
(continues on next page)

\begin{tabular}{lrrrrrr} 
\\
\(7783-81-5\) & Uranium(VI) fluoride -1204.0 & -2690.0 & -2144.0 & 0.0 & 0.0 \\
\(7783-82-6\) & Tungsten(VI) fluoride & -719.0 & -1143.0 & 0.0 & 0.0 & 0.0 \\
\(7803-51-2\) & Phosphine & -146.0 & -733.0 & 1022.0 & -1220.0 & 0.0 \\
\(10024-97-2\) & Nitrous oxide & -130.0 & -307.0 & -248.0 & 0.0 & 0.0 \\
\(10102-43-9\) & Nitric oxide & -12.0 & -119.0 & 89.0 & -73.0 & 0.0
\end{tabular}

\subsection*{1.37 Developer's Guide and Roadmap}

The chemicals project has the following core ideas as its goals:
- Efficient
- Functions do only the work required.
- Caching various values, precomputing others.
- Using various macros and automated expressions to run code with Numba at its optimal speed.
- Not using Numpy/SciPy most of the time, allowing PyPy or Numba to speed code up when speed is important.
- Capable of vectorized computation
- Wrapped with numpy's np.vectorize.
- Wrapped with numba's ufunc machinery.
- Comprehensive
- Most correlations taught at the undergrad level included.
- Capable of handling units
- Pint interface
- All docstrings/code in base SI units

This is a hobby project primarily by Caleb Bell. Contributors are welcome! Chemicals properties is huge big field.

\subsection*{1.37.1 Scope and Future Features}

The library has a focus on pure-component properties. Lots of data files are included and there is ample room for more files. However, it is not feasible to add data on an individual chemical alone - a compilation of data which includes that chemicals must be found instead.

The following properties have been looked at a little but may have too much data fit on PyPi. If you are interested in implementing one of them it may take multiple data packages uploaded to PyPi alongside chemicals:
- IR, NMR, MS, and UV-Vis spectra. Files are typically \(4-40\) KB. A collection of \(\sim 2000\) UV files from NIST takes 6 MB space, so the space issue would not be ran into right away. Some databases like NIST and NMRShiftDB are open.

\subsection*{1.37.2 Contributing}

Chemicals has a lot of infrastructure that makes it attractive to add code to the project. Adding functionality to chemicals may also make your work more visible to more people.
Adding new functionality is possible without compromising load speed, RAM usage or maintainability. If you have a chemical property you are interested in adding, a utility function, or a new data source, please feel free to open a PR and we can make any changes needed. There is no template - just do your best.

In an ideal world, new contributions would come with unit tests, docstrings, an addition to the tutorial if relevant.

\subsection*{1.37.3 Running Tests}

From the root directory of the project you downloaded with git clone https://github.com/CalebBell/chemicals.git, run the following command:
```

python3 -m pytest .

```

This will run all of the tests. Additionally pytest can be used to run the doctests:
```

python3 -m pytest --doctest-modules .

```

The test suite can take some time to run; tests are marked with various markers to allow a fast subset of tests to run.
```

python3 -m pytest -m "not slow" .

```

This should only take a few seconds, and show red output if a test is broken. To keep the main test suite fast, pytest allows a flag which shows how long each test takes.
```

python3 -m pytest -m "not slow" --durations=100

```

If a test you added appears in this list, consider splitting it into a fast portion and a slow portion.

\subsection*{1.37.4 Docstrings}

The docstrings follow Pep8, most of the numpydoc standard, More information about numpydoc can be found here In addition to being documentation, the docstrings in chemicals serve the following purposes:
- Contain LaTeX math formulas for implemented formulas. This makes it easy for the reader and authors to follow code. This is especially important when the code can be optimized by hand significantly, and end up not looking like the math formulas.
- Contain doctests for every public method. These examples often make debugging really easy since they can just be copy-pasted into Jupyter or an IDE/debugger.
- Contain type information for each variable, which is automatically parsed by the unit handling framework around pint.
- Contain the units of each argument, which is used by the unit handling framework around pint.
- Contain docstrings for every argument - these are checked by the unit tests programatically to avoid forgetting to add a description, which the author did often before the checker was added.

No automated style tool is ran on the docstrings at present, but the following command was used once to format the docstrings with the tool docformatter
```

python3 -m docformatter --wrap-summaries=80 --wrap-descriptions=80 --in-place --
recursive .

```

This does not quite match numpydoc's recommended 75 character limit.

\subsection*{1.37.5 Doctest}

As anyone who has used doctest before knows, floating-point calculations have trivially different results across platforms. An example cause of this is that most compilers have different \(\sin / c o s\) implementations which are not identical. However, docstrings are checked bit-for-bit, so consistent output is important. Python is better than most languages at maintaining the same results between versions but it is still an issue.

The docstrings are not considered sufficiently consistent to be part of the automated CI infrastructure. All functionality tested by docstrings should also be tested as part of the unit tests.

CPython 3.764 bit on Linux compiled with gcc 9.2 is currently the platform used to generate the final/official results of docstring examples. Docstrings are should be added by contributors for new functionality, but don't worry about this floating point issue. The principal author will make any necessary changes before each release.

\subsection*{1.37.6 Type Hints}

The Python ecosystem is gradually adding support for type information, which may allow static analyzers to help find bugs in code even before it is ran. The author has not found these helpful in Python yet - the tools are too slow, missing features, and most libraries do not contain type information. However, type hints might still be useful for your program that uses chemicals!

For that reason chemicals includes a set of type hints as stub files (.pyi extension). These are not generated by hand they use the cool MonkeyType library. An included script make_test_stubs interfaces with this library, which runs the test suite and at the end generates the type hints including the types of every argument to every function seen in the test suite. This is another reason comprehensive test suite coverage is required.

Monkeytype on the chemicals test suite takes \(\sim 5\) minutes to run, and generates a \(\sim 1\) GB database file which is deleted at the end of the run. Some manipulation of the result by hand may be required in the future, or MonkeyType may be replaced by making the type hints by hand. It is planned to incorporate the type stubs into the main file at some point in the future when the tooling is better.
If you are contributing, the main developer can do this step for your contribution.

\subsection*{1.37.7 Supported Python Versions}

It is strongly recommended to use Chemicals with Python 3.6 or later.
Numpy's latest release supports Python 3.6 or later as of August 2020. Pint, the unit interface, supports Python 3.6 or later as of August 2020. If using the Numba interface of Chemicals, the latest version of Numba is required. New features added to Numba may be added to Chemicals quite quickly.

Chemicals may import in an earlier Python but that is not an indication you should use it in that case.

\subsection*{1.37.8 Packaging}

The most up to date chemicals can be obtained on GitHub, and new releases are pushed to PyPi whenever a new release is made.

\subsection*{1.37.9 Code Formatting}

Pep8 is loosely followed. Do your best to follow it if possible, otherwise don't worry about it. Please don't submit a PR for just style changes.

\subsection*{1.37.10 Documentation}

Sphinx is used with readthedocs. Readthedocs is configured to build whatever is on the release branch. From the root of the chemicals project, the documentation can be built with the following command, which will output html files into a "_build" folder:
```

sphinx-build -b html docs _build

```

\subsection*{1.37.11 Sample Notebooks}

The nbval pytest plugin can be used to check the results of running the notebooks against the stored notebooks.
On UNIX/Mac OS/WSL, the notebook results can be regenerated with the following shell command, from the directory with the notebooks:
```

for i in *.ipynb ; do python3 -m jupyter nbconvert --to notebook --inplace --execute "\$i
\hookrightarrow" ; done

```

\subsection*{1.37.12 Continuous Integration}

Github Actions is presently used. They test only code in the release branch. Some tests, like those that download data from the internet, are not ran by design on their platforms. The same goes for testing numba online - getting an up to date version of numba is challenging.

\subsection*{1.37.13 Load Speed}

On CPython, chemicals will load Numpy on load if it is available and SciPy and Pandas when they are needed. Numpy loads in \(\sim 150 \mathrm{~ms}\). chemicals alone loads in \(\sim 15 \mathrm{~ms}\). It is intended for this to increase only slowly.

\subsection*{1.37.14 RAM Usage}

Adding new data and methods is well worth the price of increasing RAM, but it is intended to keep RAM consumption small via lazy-loading all data sets.

\subsection*{1.37.15 Additional Material}

More information about the interfaces with PyPy and Numba can be found on the fluids site.

\subsection*{1.38 Computing Properties of Water and Steam in Python}

Water is a very special substance. It is abundant, cheap, hydrating, and great for many engineering applications. Whatever your modeling goal, there is a good change you will require properties of water at various conditions.

There is an international association, IAPWS, which publishes and coordinates some of the best research on the properties of water. There is a special equation of state just for water developed by them that very accurately computes the properties of water, called IAPWS-95. There is also a "shortcut" version called IAPWS-97 which is faster to solve but has reduced accuracy and various discontinuities.

There are quite a few implementations of IAPWS-95 and IAPWS-97 out there. Besides the many commercial implementations, the are the following excellent open source ones:
- iapws by Juan José Gómez Romera, GPL3 licensed, containing IAPWS-95 and IAPWS-97 among other standards. Implemented in Python.
- CoolProp by Ian Bell, MIT licensed and containing IAPWS-95 and IAPWS-97 along with their transport properties. Implemented in C++ with an excellent interface to Python among other languages.
- freesteam by John Pye, GPL3 licensed, containing most of IAPWS-97 and the transport properties. Implemented in C.

There are many more, but these are the best developed libraries that can be used from Python. Water is so common and present in so many calculations that for many applications it is important to make it as fast as possible. IAPWS-95 is conventionally slow; properties are requested at a specified temperature \(T\) and pressure \(P\), but the equation of state's input variables are temperature and density! A numerical solver must be used in this case to find the density which yields the specified pressure. This density-solution procedure is normally the slowest part, although computing some properties requires many derivatives that can be slow also.

A good conventional density solver will take \(\sim 10-30 \mathrm{~s}\) on a modern computer. Only the CPU clockspeed really matters for this calculation time. It was discovered that with the use of Common subexpression elimination, the calculation could be speed up quite a lot. Additionally, if the IAPWS-95 density solution is initialized by the IAPWS-97 explicit calculation (applicable most of the time but not always), a few more iterations can be saved.

The net result of these optimizations is a greatly improved density solve time - normally \(2.5-4 \mathrm{~s}\) when running with PyPy or Numba. The con to this approach is that the code is nearly unreadable, and it would not be possible to update the coefficients without rewriting the implementation. As IAPWS-95 is a static model which will be the best one available for many years to come, this is an acceptable trade off.

\section*{INSTALLATION}

Get the latest version of chemicals from https://pypi.python.org/pypi/chemicals/
If you have an installation of Python with pip, simple install it with:
\$ pip install chemicals
If you are using conda, you can install chemicals from conda-forge channel:
\$ conda install -c conda-forge chemicals
To get the git version, run:
\$ git clone git://github.com/CalebBell/chemicals.git

\section*{LATEST SOURCE CODE}

The latest development version of chemicals's sources can be obtained at https://github.com/CalebBell/chemicals

\section*{BUG REPORTS}

To report bugs, please use the chemicals's Bug Tracker at: https://github.com/CalebBell/chemicals/issues

\section*{LICENSE INFORMATION}

See LICENSE. txt for information on the terms \& conditions for usage of this software, and a DISCLAIMER OF ALL WARRANTIES.

Although not required by the chemicals license, if it is convenient for you, please cite chemicals if used in your work. Please also consider contributing any changes you make back, and benefit the community.

To cite chemicals in publications use:
Caleb Bell, Yoel Rene Cortes-Pena, and Contributors (2016-2023). Chemicals: Chemical \(\quad\) \(\rightarrow\) properties component of Chemical Engineering Design Library (ChEDL)
https://github.com/CalebBell/chemicals.

\section*{INDICES AND TABLES}
- genindex
- modindex
- search

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chemicals.acentric, }
chemicals.air, 11
chemicals.combustion, 28
chemicals.critical,45
chemicals.dipole, }6
chemicals.dippr,64
chemicals.elements,77
chemicals.environment, 86
chemicals.exceptions,90
chemicals.flash_basic, }9
chemicals.heat_capacity,100
chemicals.iapws, }13
chemicals.identifiers,183
chemicals.interface, 191
chemicals.lennard_jones, 211
chemicals.miscdata, 224
chemicals.molecular_geometry, 225
chemicals.permittivity,228
chemicals.phase_change, 230
chemicals.rachford_rice, 246
chemicals.reaction, 262
chemicals.refractivity,274
chemicals.safety, 280
chemicals.solubility, }29
chemicals.temperature, 304
chemicals.thermal_conductivity, 307
chemicals.triple, 335
chemicals.utils, 338
chemicals.vapor_pressure, 370
chemicals.vectorized, }39
chemicals.virial, 399
chemicals.viscosity,442
chemicals.volume,471

```

\section*{A}
air_fuel_ratio_solver() (in module chemicals.combustion), 37
AKI() (in module chemicals.combustion), 40
Aleem() (in module chemicals.interface), 196
Alibakhshi () (in module chemicals.phase_change), 243
Ambrose_Walton() (in module chemicals.vapor_pressure), 386
Amgat () (in module chemicals.volume), 479
Antoine() (in module chemicals.vapor_pressure), 371
Antoine_AB_coeffs_from_point() (in module chemicals.vapor_pressure), 393
Antoine_coeffs_from_point() (in module chemicals.vapor_pressure), 392
Antoine_fitting_jacobian() (in module chemicals.vapor_pressure), 384
API10A32() (in module chemicals.interface), 203
API_to_rho() (in module chemicals.utils), 338
API_to_SG() (in module chemicals.utils), 338
atom_fractions() (in module chemicals.elements), 84
atom_matrix() (in module chemicals.elements), 86
atoms_to_Hill() (in module chemicals.elements), 81

\section*{B}

B_from_Z() (in module chemicals.virial), 400
B_to_Z() (in module chemicals.virial), 399
Bahadori_gas() (in module chemicals.thermal_conductivity), 322
Bahadori_liquid() (in module chemicals.thermal_conductivity), 311
balance_stoichiometry() (in module chemicals.reaction), 272
Bhirud_normal () (in module chemicals.volume), 475
boiling_critical_relation() (in module chemicals.vapor_pressure), 387
brix_to_RI() (in module chemicals.refractivity), 276
Brock_Bird() (in module chemicals.interface), 191
Brokaw() (in module chemicals.viscosity), 449
BVirial_Abbott() (in module chemicals.virial), 414
BVirial_Abbott_fast() (in module chemicals.virial), 421

BVirial_Abbott_mat() (in module chemicals.virial), 434
BVirial_Abbott_vec() (in module chemicals.virial), 433
BVirial_Meng() (in module chemicals.virial), 424
BVirial_Meng_mat () (in module chemicals.virial), 436
BVirial_Meng_vec() (in module chemicals.virial), 435
BVirial_mixture() (in module chemicals.virial), 402
BVirial_Oconnell_Prausnitz() (in module chemicals.virial), 423
BVirial_Oconnell_Prausnitz_mat() (in module chemicals.virial), 437
BVirial_Oconnell_Prausnitz_vec() (in module chemicals.virial), 437
BVirial_Pitzer_Curl() (in module chemicals.virial), 413
BVirial_Pitzer_Curl_fast() (in module chemicals.virial), 420
BVirial_Pitzer_Curl_mat() (in module chemicals.virial), 433
BVirial_Pitzer_Curl_vec() (in module chemicals.virial), 432
BVirial_Tsonopoulos() (in module chemicals.virial), 416
BVirial_Tsonopoulos_extended() (in module chemicals.virial), 417
BVirial_Tsonopoulos_extended_fast() (in module chemicals.virial), 422
BVirial_Tsonopoulos_extended_mat() (in module chemicals.virial), 439
BVirial_Tsonopoulos_extended_vec() (in module chemicals.virial), 438
BVirial_Tsonopoulos_fast() (in module chemicals.virial), 421
BVirial_Tsonopoulos_mat() (in module chemicals.virial), 435
BVirial_Tsonopoulos_vec() (in module chemicals.virial), 434
BVirial_Xiang() (in module chemicals.virial), 424
BVirial_Xiang_mat() (in module chemicals.virial), 431
BVirial_Xiang_vec() (in module chemicals.virial),

431
C
calculate() (chemicals.heat_capacity.ShomateRange method), 105
calculate() (chemicals.heat_capacity.ZabranskyQuasip method), 120
calculate() (chemicals.heat_capacity.ZabranskySpline method), 119
calculate_integral() cals.heat_capacity.ShomateRange method), 105
calculate_integral() (chemicals.heat_capacity.ZabranskyQuasipolynomial method), 121
calculate_integral() (chemicals.heat_capacity.ZabranskySpline method), 119
calculate_integral_over_T()
cals.heat_capacity.ShomateRange 105
calculate_integral_over_T() cals.heat_capacity.ZabranskyQuasipolynomial method), 121
calculate_integral_over_T() (chemicals.heat_capacity.ZabranskySpline method), 120
Campbell_Thodos() (in module chemicals.volume), 476
Carcinogen() (in module chemicals.safety), 284
Carcinogen_all_methods (in module chemicals.safety), 285
Carcinogen_methods() (in module chemicals.safety), 285
CAS_from_any() (in module chemicals.identifiers), 183
CAS_to_int() (in module chemicals.identifiers), 187
Ceiling() (in module chemicals.safety), 283
Ceiling_all_methods (in module chemicals.safety), 283
Ceiling_methods() (in module chemicals.safety), 283
charge_from_formula() (in module chemicals.elements), 80
check_CAS() (in module chemicals.identifiers), 186
ChemicalMetadata (class in chemicals.identifiers), 188
ChemicalMetadataDB (class in chemicals.identifiers), 189
chemicals.acentric module, 7
chemicals.air module, 11
chemicals.combustion module, 28
chemicals.critical module, 45
chemicals.dipole
module, 63
chemicals.dippr
module, 64
chemicals.elements
module, 77
 module, 86
chemicals.exceptions module, 90
chemicals.flash_basic
module, 92
chemicals.heat_capacity
module, 100
chemicals.iapws
module, 133
chemicals.identifiers module, 183
chemicals.interface module, 191
chemicals.lennard_jones module, 211
chemicals.miscdata module, 224
chemicals.molecular_geometry
module, 225
chemicals.permittivity
module, 228
chemicals.phase_change module, 230
chemicals.rachford_rice module, 246
chemicals.reaction module, 262
chemicals.refractivity module, 274
chemicals.safety module, 280
chemicals.solubility module, 297
chemicals.temperature module, 304
chemicals.thermal_conductivity module, 307
chemicals.triple module, 335
chemicals.utils
module, 338
chemicals.vapor_pressure module, 370
chemicals.vectorized module, 398
chemicals.virial
module, 399
chemicals.viscosity
module, 442
chemicals.volume
module, 471
Chemsep_16() (in module chemicals.thermal_conductivity), 333
Chen() (in module chemicals.phase_change), 235
Chueh_Prausnitz_Tc() (in module chemicals.critical), 59
Chueh_Prausnitz_Vc() (in module chemicals.critical), 61
Chung() (in module chemicals.thermal_conductivity), 319
Chung_dense() (in module chemicals.thermal_conductivity), 325
Clapeyron() (in module chemicals.phase_change), 241
combustion_data() (in module chemicals.combustion), 32
combustion_products_mixture() (in module chemicals.combustion), 29
combustion_spec_solver() (in module chemicals.combustion), 36
combustion_stoichiometry() (in module chemicals.combustion), 28
CombustionData (class in chemicals.combustion), 33
CommonMixtureMetadata (class in chemicals.identifiers), 189
COSTALD() (in module chemicals.volume), 472
COSTALD_compressed() (in module chemicals.volume), 478
COSTALD_mixture() (in module chemicals.volume), 480
Cp_data_Poling (in module chemicals.heat_capacity), 130
Cp_dict_characteristic_temperatures_adjusted_(in module chemicals.heat_capacity), 130
Cp_dict_characteristic_temperatures_psi4_2022ad (in module chemicals.heat_capacity), 130
Cp_dict_PerryI (in module chemicals.heat_capacity), 130
Cp_minus_Cv() (in module chemicals.utils), 339
Cpg_statistical_mechanics() (in module chemicals.heat_capacity), 113
Cpg_statistical_mechanics_integral() (in module chemicals.heat_capacity), 114
Cpg_statistical_mechanics_integral_over_T() (in module chemicals.heat_capacity), 114
CRC_inorganic() (in module chemicals.volume), 486
CRC_standard_data (in module chemicals.heat_capacity), 130
critical_surface() (in module chemicals.critical), 52
critical_surface_all_methods (in module chemicals.critical), 53
critical_surface_methods() (in module chemicals.critical), 53
Crowl_Louvar_LFL() (in module chemicals.safety), 289

Crowl_Louvar_UFL() (in module chemicals.safety), 293
cryogenics (in module chemicals.identifiers), 190
CVirial_Liu_Xiang() (in module chemicals.virial), 427
CVirial_Liu_Xiang_mat() (in module chemicals.virial), 440
CVirial_Liu_Xiang_vec() (in module chemicals.virial), 439
CVirial_mixture_Orentlicher_Prausnitz() (in module chemicals.virial), 404
CVirial_Orbey_Vera() (in module chemicals.virial), 426
CVirial_Orbey_Vera_mat() (in module chemicals.virial), 441
CVirial_Orbey_Vera_vec() (in module chemicals.virial), 440
d2Antoine_dT2() (in module chemicals.vapor_pressure), 377
d2BVirial_mixture_dzizjs() (in module chemicals.virial), 403
d2CVirial_mixture_dT2_Orentlicher_Prausnitz() (in module chemicals.virial), 405
d2CVirial_mixture_Orentlicher_Prausnitz_dTdzs() (in module chemicals.virial), 410
d2CVirial_mixture_Orentlicher_Prausnitz_dzizjs() (in module chemicals.virial), 408
d2Henry_constants_dT2() (in module chemicals.solubility), 301
d2ns_to_dn2_partials() (in module chemicals.utils), 344
\$2TRZORAREOine_extended_dT2() (in module chemicals.vapor_pressure), 381
d2V_dzizjs_virial() (in module chemicals.virial), 412
d2Wagner_dT2() (in module chemicals.vapor_pressure), 378
d2Wagner_original_dT2() (in module chemicals.vapor_pressure), 380
d2xs_to_d2xsn1() (in module chemicals.utils), 345
d2xs_to_dxdn_partials() (in module chemicals.utils), 346
d2Yaws_Psat_dT2() (in module chemicals.vapor_pressure), 382
d3BVirial_mixture_dzizjzks() (in module chemicals.virial), 404
d3CVirial_mixture_dT3_Orentlicher_Prausnitz() (in module chemicals.virial), 406
d3CVirial_mixture_Orentlicher_Prausnitz_dzizjzks() (in module chemicals.virial), 409
Dadgostar_Shaw() (in module chemicals.heat_capacity), 124

Dadgostar_Shaw_integral() (in module chemicals.heat_capacity), 124
Dadgostar_Shaw_integral_over_T() (in module chemicals.heat_capacity), 125
Dadgostar_Shaw_terms() (in module chemicals.heat_capacity), 126
dAntoine_dT() (in module chemicals.vapor_pressure), 377
dBVirial_mixture_dzs() (in module chemicals.virial), 403
dCVirial_mixture_dT_Orentlicher_Prausnitz() (in module chemicals.virial), 405
dCVirial_mixture_Orentlicher_Prausnitz_dzs() (in module chemicals.virial), 407
dHenry_constants_dT() (in module chemicals.solubility), 300
Diguilio_Teja() (in module chemicals.interface), 201
dipole_moment() (in module chemicals.dipole), 63
dipole_moment_all_methods (in module chemicals.dipole), 64
dipole_moment_methods() (in module chemicals.dipole), 64
DIPPR101_ABC_coeffs_from_point() (in module chemicals.vapor_pressure), 394
DIPPR9B() (in module chemicals.thermal_conductivity), 318
DIPPR9G() (in module chemicals.thermal_conductivity), 313
DIPPR9H() (in module chemicals.thermal_conductivity), 315
DIPPR9I() (in module chemicals.thermal_conductivity), 315
dippr_compounds() (in module chemicals.identifiers), 190
dmu_Yaws_dT() (in module chemicals.viscosity), 464
dns_to_dn_partials() (in module chemicals.utils), 347
dPPDS9_dT() (in module chemicals.viscosity), 460
dPsat_IAPWS_dT() (in module chemicals.vapor_pressure), 391
dTRC_Antoine_extended_dT() (in module chemicals.vapor_pressure), 380
dV_dzs_virial() (in module chemicals.virial), 411
dWagner_dT() (in module chemicals.vapor_pressure), 378
dWagner_original_dT() (in module chemicals.vapor_pressure), 379
dxs_to_dn_partials() (in module chemicals.utils), 347
dxs_to_dns() (in module chemicals.utils), 348
dxs_to_dxsn1() (in module chemicals.utils), 349
dYaws_Psat_dT() (in module chemicals.vapor_pressure), 382

\section*{\(E\)}

Edalat() (in module chemicals.vapor_pressure), 388
Element (class in chemicals.elements), 78
Eli_Hanley() (in module chemicals.thermal_conductivity), 320
Eli_Hanley_dense() (in module chemicals.thermal_conductivity), 324
entropy_formation() (in module chemicals.reaction), 270
epsilon_Bird_Stewart_Lightfoot_boiling() (in module chemicals.lennard_jones), 214
epsilon_Bird_Stewart_Lightfoot_critical() (in module chemicals.lennard_jones), 213
epsilon_Bird_Stewart_Lightfoot_melting() (in module chemicals.lennard_jones), 214
epsilon_Flynn() (in module chemicals.lennard_jones), 213
epsilon_Stiel_Thodos() (in module chemicals.lennard_jones), 215
epsilon_Tee_Gotoh_Steward_1() (in module chemicals.lennard_jones), 215
epsilon_Tee_Gotoh_Steward_2() (in module chemicals.lennard_jones), 216
EQ100 () (in module chemicals.dippr), 65
EQ101() (in module chemicals.dippr), 66
EQ101_fitting_jacobian() (in module chemicals.dippr), 75
EQ102() (in module chemicals.dippr), 67
EQ102_fitting_jacobian() (in module chemicals.dippr), 76
EQ104() (in module chemicals.dippr), 68
EQ105() (in module chemicals.dippr), 69
EQ105_fitting_jacobian() (in module chemicals.dippr), 76
EQ106() (in module chemicals.dippr), 70
EQ106_fitting_jacobian() (in module chemicals.dippr), 76
EQ107() (in module chemicals.dippr), 71
EQ107_fitting_jacobian() (in module chemicals.dippr), 76
EQ114() (in module chemicals.dippr), 72
EQ115() (in module chemicals.dippr), 73
EQ116() (in module chemicals.dippr), 73
EQ127() (in module chemicals.dippr), 74
Eucken() (in module chemicals.thermal_conductivity), 317
Eucken_modified() (in module chemicals.thermal_conductivity), 317

F
Filippov() (in module chemicals.thermal_conductivity), 316
fire_mixing() (in module chemicals.safety), 294
flash_ideal() (in module chemicals.flash_basic), 92
flash_inner_loop() (in module chemicals.rachford_rice), 247
flash_inner_loop_all_methods (in module chemicals.rachford_rice), 248
flash_inner_loop_methods() (in module chemicals.rachford_rice), 248
flash_Tb_Tc_Pc() (in module chemicals.flash_basic), 95
flash_wilson() (in module chemicals.flash_basic), 94
fuel_air_spec_solver() (in module chemicals.combustion), 34

\section*{G}
get_pubchem_db() (in module chemicals.identifiers), 190
Gharagheizi_gas() (in module chemicals.thermal_conductivity), 321
Gharagheizi_liquid() (in module chemicals.thermal_conductivity), 309
Gibbs_formation() (in module chemicals.reaction), 269
Goodman() (in module chemicals.volume), 482
Grieves_Thodos() (in module chemicals.critical), 60
Grigoras() (in module chemicals.critical), 55
GWP() (in module chemicals.environment), 87
GWP_all_methods (in module chemicals.environment), 88
GWP_methods() (in module chemicals.environment), 88

\section*{H}

Hakim_Steinberg_Stiel() (in module chemicals.interface), 194
Hekayati_Raeissi() (in module chemicals.critical), 56
Henry_constants() (in module chemicals.solubility), 299
Henry_converter() (in module chemicals.solubility), 298
Henry_pressure() (in module chemicals.solubility), 297
Henry_pressure_mixture() (in module chemicals.solubility), 297
Herning_Zipperer() (in module chemicals.viscosity), 448
Hf_basis_converter() (in module chemicals.reaction), 271
Hfg() (in module chemicals.reaction), 265
Hfg_all_methods (in module chemicals.reaction), 266
Hfg_methods() (in module chemicals.reaction), 266
Hfl () (in module chemicals.reaction), 264
Hfl_all_methods (in module chemicals.reaction), 264
Hfl_methods() (in module chemicals.reaction), 264
Hfs() (in module chemicals.reaction), 263
Hfs_all_methods (in module chemicals.reaction), 263
Hfs_methods() (in module chemicals.reaction), 263

Hfus() (in module chemicals.phase_change), 233
Hfus_all_methods (in module chemicals.phase_change), 234
Hfus_methods() (in module chemicals.phase_change), 234
HHV_modified_Dulong() (in module chemicals.combustion), 31
HHV_stoichiometry() (in module chemicals.combustion), 30

I
iapws04_dHenry_air_dT() (in module chemicals.air), 27
iapws04_Henry_air() (in module chemicals.air), 27
iapws11_Psub() (in module chemicals.iapws), 143
iapws92_dPsat_dT() (in module chemicals.iapws), 142
iapws92_Psat() (in module chemicals.iapws), 141
iapws92_rhog_sat() (in module chemicals.iapws), 146
iapws92_rhol_sat() (in module chemicals.iapws), 146
iapws95_AQ() (in module chemicals.iapws), 174
iapws95_AQ_tau_derivatives() (in module chemicals.iapws), 176
iapws95_Ar() (in module chemicals.iapws), 176
iapws95_d2AQ_dtau2() (in module chemicals.iapws), 175
iapws95_d2Ar_ddelta2() (in module chemicals.iapws), 178
iapws95_d2Ar_ddeltadtau() (in module chemicals.iapws), 181
iapws95_d2Ar_dtau2() (in module chemicals.iapws), 180
iapws95_d3AQ_dtau3() (in module chemicals.iapws), 175
iapws95_d3Ar_ddelta2dtau() (in module chemicals.iapws), 182
iapws95_d3Ar_ddelta3() (in module chemicals.iapws), 179
iapws95_d3Ar_ddeltadtau2() (in module chemicals.iapws), 181
iapws95_d4Ar_ddelta2dtau2() (in module chemicals.iapws), 183
iapws95_dAQ_dtau() (in module chemicals.iapws), 174
iapws95_dAr_ddelta() (in module chemicals.iapws), 177
iapws95_dAr_dtau() (in module chemicals.iapws), 179
iapws95_dPsat_dT() (in module chemicals.iapws), 141
iapws95_drhol_sat_dT() (in module chemicals.iapws), 145
iapws95_MW (in module chemicals.iapws), 147
iapws95_P() (in module chemicals.iapws), 134
iapws95_Pc (in module chemicals.iapws), 147
iapws95_properties() (in module chemicals.iapws), 139
iapws95_Psat() (in module chemicals.iapws), 140
iapws95_R (in module chemicals.iapws), 147
iapws95_rho() (in module chemicals.iapws), 133
iapws95_rhoc (in module chemicals.iapws), 147
iapws95_rhog_sat() (in module chemicals.iapws), 145
iapws95_rhol_sat() (in module chemicals.iapws), 144
iapws95_saturation() (in module chemicals.iapws), 143
iapws95_T() (in module chemicals.iapws), 135
iapws95_Tc (in module chemicals.iapws), 147
iapws95_Tsat() (in module chemicals.iapws), 142
iapws95_Tt (in module chemicals.iapws), 147
iapws97_A_region3() (in module chemicals.iapws), 155
iapws97_boundary_3ab() (in module chemicals.iapws), 160
iapws97_boundary_3cd() (in module chemicals.iapws), 158
iapws97_boundary_3ef() (in module chemicals.iapws), 157
iapws97_boundary_3gh() (in module chemicals.iapws), 158
iapws97_boundary_3ij() (in module chemicals.iapws), 158
iapws97_boundary_3jk() (in module chemicals.iapws), 159
iapws97_boundary_3mn() (in module chemicals.iapws), 159
iapws97_boundary_3op() (in module chemicals.iapws), 161
iapws97_boundary_3qu() (in module chemicals.iapws), 159
iapws97_boundary_3rx() (in module chemicals.iapws), 160
iapws97_boundary_3uv() (in module chemicals.iapws), 157
iapws97_boundary_3wx () (in module chemicals.iapws), 160
iapws97_d2A_ddelta2_region3() (in module chemicals.iapws), 155
iapws97_d2A_ddeltadtau_region3() (in module chemicals.iapws), 157
iapws97_d2A_dtau2_region3() (in module chemicals.iapws), 156
iapws97_d2G0_dtau2_region2() (in module chemicals.iapws), 151
iapws97_d2G0_dtau2_region5() (in module chemicals.iapws), 171
iapws97_d2G_dpi2_region1() (in module chemicals.iapws), 148
iapws97_d2G_dpidtau_region1() (in module chemicals.iapws), 150
iapws97_d2G_dtau2_region1() (in module chemicals.iapws), 149
iapws97_d2Gr_dpi2_region2() (in module chemi-
cals.iapws), 153
iapws97_d2Gr_dpi2_region5() (in module chemicals.iapws), 172
iapws97_d2Gr_dpidtau_region2() (in module chemicals.iapws), 154
iapws97_d2Gr_dpidtau_region5() (in module chemicals.iapws), 173
iapws97_d2Gr_dtau2_region2() (in module chemicals.iapws), 154
iapws97_d2Gr_dtau2_region5() (in module chemicals.iapws), 173
iapws97_dA_ddelta_region3() (in module chemicals.iapws), 155
iapws97_dA_dtau_region3() (in module chemicals.iapws), 156
iapws97_dG0_dtau_region2() (in module chemicals.iapws), 151
iapws97_dG0_dtau_region5() (in module chemicals.iapws), 170
iapws97_dG_dpi_region1() (in module chemicals.iapws), 148
iapws97_dG_dtau_region1() (in module chemicals.iapws), 149
iapws97_dGr_dpi_region2() (in module chemicals.iapws), 152
iapws97_dGr_dpi_region5() (in module chemicals.iapws), 172
iapws97_dGr_dtau_region2() (in module chemicals.iapws), 153
iapws97_dGr_dtau_region5() (in module chemicals.iapws), 173
iapws97_G0_region2() (in module chemicals.iapws), 150
iapws97_G0_region5() (in module chemicals.iapws), 170
iapws97_G_region1() (in module chemicals.iapws), 148
iapws97_Gr_region2() (in module chemicals.iapws), 152
iapws97_Gr_region5() (in module chemicals.iapws), 171
iapws97_P() (in module chemicals.iapws), 136
iapws97_R (in module chemicals.iapws), 147
iapws97_region3_a() (in module chemicals.iapws), 161
iapws97_region3_b() (in module chemicals.iapws), 161
iapws97_region3_c() (in module chemicals.iapws), 162
iapws97_region3_d() (in module chemicals.iapws), 162
iapws97_region3_e() (in module chemicals.iapws), 162
iapws97_region3_f() (in module chemicals.iapws),

163
iapws97_region3_g() (in module chemicals.iapws), 163
iapws97_region3_h() (in module chemicals.iapws), 163
iapws97_region3_i() (in module chemicals.iapws), 164
iapws97_region3_j() (in module chemicals.iapws), 164
iapws97_region3_k() (in module chemicals.iapws), 164
iapws97_region3_1() (in module chemicals.iapws), 165
iapws97_region3_m() (in module chemicals.iapws), 165
iapws97_region3_n() (in module chemicals.iapws), 165
iapws97_region3_o() (in module chemicals.iapws), 166
iapws97_region3_p() (in module chemicals.iapws), 166
iapws97_region3_q() (in module chemicals.iapws), 166
iapws97_region3_r() (in module chemicals.iapws), 167
iapws97_region3_s() (in module chemicals.iapws), 167
iapws97_region3_t() (in module chemicals.iapws), 167
iapws97_region3_u() (in module chemicals.iapws), 168
iapws97_region3_v() (in module chemicals.iapws), 168
iapws97_region3_w() (in module chemicals.iapws), 168
iapws97_region3_x() (in module chemicals.iapws), 169
iapws97_region3_y() (in module chemicals.iapws), 169
iapws97_region3_z() (in module chemicals.iapws), 169
iapws97_rho() (in module chemicals.iapws), 136
iapws97_T() (in module chemicals.iapws), 137
ideal_gas() (in module chemicals.volume), 481
IDs_to_CASs() (in module chemicals.identifiers), 186
IDT_to_DCN() (in module chemicals.combustion), 41
ignition_delay() (in module chemicals.combustion), 44
ignition_delay_all_methods (in module chemicals.combustion), 44
ignition_delay_methods() (in module chemicals.combustion), 44
Ihmels() (in module chemicals.critical), 54
index_hydrogen_deficiency() (in module chemi-
cals.elements), 83
inerts (in module chemicals.identifiers), 190
int_to_CAS() (in module chemicals.identifiers), 187
isentropic_exponent() (in module chemicals.utils), 349
isentropic_exponent_PT() (in module chemicals.utils), 350
isentropic_exponent_PV() (in module chemicals.utils), 350
isentropic_exponent_TV() (in module chemicals.utils), 351
isobaric_expansion() (in module chemicals.utils), 352
isothermal_compressibility() (in module chemicals.utils), 352
ISTExpansion() (in module chemicals.interface), 208
ITS90_68_difference() (in module chemicals.temperature), 305

Jasper () (in module chemicals.interface), 206
Joule_Thomson() (in module chemicals.utils), 340
K
k_air_lemmon() (in module chemicals.thermal_conductivity), 330
k _data_Perrys_8E_2_314 (in module chemicals.thermal_conductivity), 334
k _data_Perrys_8E_2_315 (in module chemicals.thermal_conductivity), 334
k_data_VDI_PPDS_10 (in module chemicals.thermal_conductivity), 334
k_data_VDI_PPDS_9 (in module chemicals.thermal_conductivity), 334
k_IAPWS() (in module chemicals.thermal_conductivity), 328
K_value() (in module chemicals.flash_basic), 96
\(\mathrm{kl} \_M e r s m a n n \_K i n d()\) (in module chemicals.thermal_conductivity), 312

\section*{\(L\)}

Lakshmi_Prasad() (in module chemicals.thermal_conductivity), 308
Lastovka_Shaw() (in module chemicals.heat_capacity), 108
Lastovka_Shaw_integral() (in module chemicals.heat_capacity), 110
Lastovka_Shaw_integral_over_T() (in module chemicals.heat_capacity), 110
Lastovka_Shaw_T_for_Hm() (in module chemicals.heat_capacity), 111
Lastovka_Shaw_T_for_Sm() (in module chemicals.heat_capacity), 112

Lastovka_Shaw_term_A() (in module chemicals.heat_capacity), 112
Lastovka_solid() (in module chemicals.heat_capacity), 127
Lastovka_solid_integral() (in module chemicals.heat_capacity), 128
Lastovka_solid_integral_over_T() (in module chemicals.heat_capacity), 128
Lee_Kesler() (in module chemicals.vapor_pressure), 385
Lee_Kesler_virial_CSP_Vcijs() (in module chemicals.virial), 430
lemmon2000_air_A0() (in module chemicals.air), 15
lemmon2000_air_Ar() (in module chemicals.air), 17
lemmon2000_air_d2AO_dtau2() (in module chemicals.air), 16
lemmon2000_air_d2Ar_ddelta2() (in module chemicals.air), 20
lemmon2000_air_d2Ar_ddeltadtau() (in module chemicals.air), 21
lemmon2000_air_d2Ar_dtau2() (in module chemicals.air), 18
lemmon2000_air_d3A0_dtau3() (in module chemicals.air), 16
lemmon2000_air_d3Ar_ddelta2dtau() (in module chemicals.air), 22
lemmon2000_air_d3Ar_ddelta3() (in module chemicals.air), 20
lemmon2000_air_d3Ar_ddeltadtau2() (in module chemicals.air), 22
lemmon2000_air_d3Ar_dtau3() (in module chemicals.air), 18
lemmon2000_air_d4A0_dtau4() (in module chemicals.air), 17
lemmon2000_air_d4Ar_ddelta2dtau2() (in module chemicals.air), 23
lemmon2000_air_d4Ar_ddelta3dtau() (in module chemicals.air), 24
lemmon2000_air_d4Ar_ddelta4() (in module chemicals.air), 21
lemmon2000_air_d4Ar_ddeltadtau3() (in module chemicals.air), 23
lemmon2000_air_d4Ar_dtau4() (in module chemicals.air), 19
lemmon2000_air_dAO_dtau() (in module chemicals.air), 16
lemmon2000_air_dAr_ddelta() (in module chemicals.air), 19
lemmon2000_air_dAr_dtau() (in module chemicals.air), 17
lemmon2000_air_MW (in module chemicals.air), 15
lemmon2000_air_P_bubble() (in module chemicals.air), 13
lemmon2000_air_P_dew() (in module chemicals.air),
lemmon2000_air_P_max (in module chemicals.air), 15
lemmon2000_air_P_reducing (in module chemicals.air), 15
lemmon2000_air_R (in module chemicals.air), 15
lemmon2000_air_rho_bubble() (in module chemicals.air), 14
lemmon2000_air_rho_dew() (in module chemicals.air), 14
lemmon2000_air_rho_reducing (in module chemicals.air), 15
lemmon2000_air_T_max (in module chemicals.air), 15
lemmon2000_air_T_reducing (in module chemicals.air), 15
lemmon2000_P() (in module chemicals.air), 12
lemmon2000_rho() (in module chemicals.air), 11
lemmon2000_T() (in module chemicals.air), 12
Letsou_Stiel() (in module chemicals.viscosity), 442
LFL() (in module chemicals.safety), 287
LFL_all_methods (in module chemicals.safety), 289
LFL_ISO_10156_2017() (in module chemicals.safety), 290
LFL_methods() (in module chemicals.safety), 288
LHV_from_HHV() (in module chemicals.combustion), 31
Li () (in module chemicals.critical), 58
Li_Johns_Ahmadi_solution() (in module chemicals.rachford_rice), 251
Lindsay_Bromley() (in module chemicals.thermal_conductivity), 326
linear() (in module chemicals.molecular_geometry), 226
linear_all_methods (in module chemicals.molecular_geometry), 227
linear_methods() (in module chemicals.molecular_geometry), 226
Liu() (in module chemicals.phase_change), 236
LK_omega() (in module chemicals.acentric), 10
\(\log \mathrm{P}()\) (in module chemicals.environment), 89
\(\log\) _all_methods (in module chemicals.environment), 90
logP_methods() (in module chemicals.environment), 90 lookup_VDI_tabular_data() (in module chemicals.miscdata), 224
Lorentz_Bray_Clarke() (in module chemicals.viscosity), 458
Lucas() (in module chemicals.viscosity), 444
Lucas_gas() (in module chemicals.viscosity), 446

\section*{M}
mass_fractions() (in module chemicals.elements), 84 Meissner() (in module chemicals.critical), 54
Meng_Duan_2005_virial_CSP_kijs() (in module chemicals.virial), 430
Meng_virial_a() (in module chemicals.virial), 425

Mersmann_Kind_predictor() (in module chemicals.critical), 49
Mersmann_Kind_sigma() (in module chemicals.interface), 197
Meybodi_Daryasafar_Karimi() (in module chemicals.interface), 204
mgm3_to_ppmv() (in module chemicals.safety), 295
Miqueu() (in module chemicals.interface), 195
Missenard() (in module chemicals.thermal_conductivity), 314
mix_component_flows() (in module chemicals.utils), 353
mix_component_partial_flows() (in module chemicals.utils), 354
mix_multiple_component_flows() (in module chemicals.utils), 355
mixing_logarithmic() (in module chemicals.utils), 355
mixing_power() (in module chemicals.utils), 356
mixing_simple() (in module chemicals.utils), 357
mixture_atomic_composition() (in module chemicals.elements), 85
mixture_atomic_composition_ordered() (in module chemicals.elements), 85
MK () (in module chemicals.phase_change), 239
modified_Wilson_Tc() (in module chemicals.critical), 60
modified_Wilson_Vc() (in module chemicals.critical), 62
module
chemicals.acentric, 7
chemicals.air, 11
chemicals.combustion, 28
chemicals.critical, 45
chemicals.dipole, 63
chemicals.dippr, 64
chemicals.elements, 77
chemicals.environment, 86
chemicals.exceptions, 90
chemicals.flash_basic, 92
chemicals.heat_capacity, 100
chemicals.iapws, 133
chemicals.identifiers, 183
chemicals.interface, 191
chemicals.lennard_jones, 211
chemicals.miscdata, 224
chemicals.molecular_geometry, 225
chemicals.permittivity, 228
chemicals.phase_change, 230
chemicals.rachford_rice, 246
chemicals.reaction, 262
chemicals.refractivity, 274
chemicals.safety, 280
chemicals.solubility, 297
chemicals.temperature, 304
chemicals.thermal_conductivity, 307
chemicals.triple, 335
chemicals.utils, 338
chemicals.vapor_pressure, 370
chemicals.vectorized, 398
chemicals.virial, 399
chemicals.viscosity, 442
chemicals.volume, 471
molar_refractivity_from_RI() (in module chemicals.refractivity), 278
molar_velocity_to_velocity() (in module chemicals.utils), 357
molecular_diameter() (in module chemicals.lennard_jones), 216
molecular_diameter_all_methods (in module chemicals.lennard_jones), 218
molecular_diameter_methods() (in module chemicals.lennard_jones), 217
molecular_weight() (in module chemicals.elements), 82
MON() (in module chemicals.combustion), 43
MON_all_methods (in module chemicals.combustion), 43
MON_methods() (in module chemicals.combustion), 43
mu_air_lemmon() (in module chemicals.viscosity), 455
mu_data_Dutt_Prasad (in module chemicals.viscosity), 467
mu_data_Perrys_8E_2_312 (in module chemicals.viscosity), 467
mu_data_Perrys_8E_2_313 (in module chemicals.viscosity), 467
mu_data_VDI_PPDS_7 (in module chemicals.viscosity), 467
mu_data_VDI_PPDS_8 (in module chemicals.viscosity), 468
mu_data_VN2 (in module chemicals.viscosity), 467
mu_data_VN2E (in module chemicals.viscosity), 467
mu_data_VN3 (in module chemicals.viscosity), 467
mu_IAPWS() (in module chemicals.viscosity), 453
mu_TDE() (in module chemicals.viscosity), 464
mu_Yaws() (in module chemicals.viscosity), 463
mu_Yaws_fitting_jacobian() (in module chemicals.viscosity), 464
MW () (in module chemicals.identifiers), 184
N
nested_formula_parser() (in module chemicals.elements), 80
NFPA_30_classification() (in module chemicals.safety), 296
Nicola() (in module chemicals.thermal_conductivity), 311

Nicola_original() (in module cals.thermal_conductivity), 310
none_and_length_check() (in module cals.utils), 358
normalize() (in module chemicals.utils), 358
octane_sensitivity() (in module chemicals.combustion), 40
ODP() (in module chemicals.environment), 88
ODP_all_methods (in module chemicals.environment), 89
ODP_methods() (in module chemicals.environment), 89 omega() (in module chemicals.acentric), 7 omega_all_methods (in module chemicals.acentric), 8 omega_definition() (in module chemicals.acentric), 9 omega_methods() (in module chemicals.acentric), 8
OverspeficiedError (class in chemicals.exceptions), 91

\section*{P}

Parachor () (in module chemicals.utils), 340
Pc() (in module chemicals.critical), 47
Pc_all_methods (in module chemicals.critical), 48
Pc_methods () (in module chemicals.critical), 48
Perez_Boehman_MON_from_ignition_delay() (in module chemicals.combustion), 39
Perez_Boehman_RON_from_ignition_delay() (in module chemicals.combustion), 39
periodic_table (in module chemicals.elements), 77
PeriodicTable (class in chemicals.elements), 78
permittivity_CRC() (in module chemicals.permittivity), 229
permittivity_data_CRC (in module chemicals.permittivity), 229
permittivity_IAPWS() (in module chemicals.permittivity), 228
Perry_151() (in module chemicals.heat_capacity), 126
phase_change_data_Alibakhshi_Cs (in module chemicals.phase_change), 245
phase_change_data_Perrys2_150 (in module chemicals.phase_change), 245
phase_change_data_VDI_PPDS_4 (in module chemicals.phase_change), 245
phase_identification_parameter() (in module chemicals.utils), 359
phase_identification_parameter_phase() (in module chemicals.utils), 359
PhaseCountReducedError (class in chemicals.exceptions), 91
PhaseExistenceImpossible (class in chemicals.exceptions), 91
PiecewiseHeatCapacity (class in chemicals.heat_capacity), 129

Pitzer() (in module chemicals.phase_change), 238
Pitzer_sigma() (in module chemicals.interface), 192
polarizability_from_RI() (in module chemicals.refractivity), 277
Poling() (in module chemicals.heat_capacity), 105
Poling_integral() (in module chemicals.heat_capacity), 106
Poling_integral_over_T() (in module chemicals.heat_capacity), 107
PPDS12() (in module chemicals.phase_change), 244
PPDS14() (in module chemicals.interface), 207
PPDS15() (in module chemicals.heat_capacity), 121
PPDS17() (in module chemicals.volume), 485
PPDS2 () (in module chemicals.heat_capacity), 107
PPDS3() (in module chemicals.thermal_conductivity), 332
PPDS5() (in module chemicals.viscosity), 460
PPDS8() (in module chemicals.thermal_conductivity), 332
PPDS9 () (in module chemicals.viscosity), 459
ppmv_to_mgm3() (in module chemicals.safety), 294
PR_water_K_value() (in module chemicals.flash_basic), 99
property_mass_to_molar() (in module chemicals.utils), 360
property_molar_to_mass() (in module chemicals.utils), 361
Przedziecki_Sridhar () (in module chemicals.viscosity), 443
Psat_data_Alcock_elements (in module chemicals.vapor_pressure), 395
Psat_data_AntoineExtended (in module chemicals.vapor_pressure), 395
Psat_data_AntoinePoling (in module chemicals.vapor_pressure), 395
Psat_data_Perrys2_8 (in module chemicals.vapor_pressure), 395
Psat_data_VDI_PPDS_3 (in module chemicals.vapor_pressure), 395
Psat_data_WagnerMcGarry (in module chemicals.vapor_pressure), 395
Psat_data_WagnerPoling (in module chemicals.vapor_pressure), 395
Psat_IAPWS() (in module chemicals.vapor_pressure), 390
Psub_Clapeyron() (in module chemicals.vapor_pressure), 389
Pt() (in module chemicals.triple), 337
Pt_all_methods (in module chemicals.triple), 337
Pt_methods() (in module chemicals.triple), 337

\section*{R}

Rachford_Rice_flash_error() (in module chemicals.rachford_rice), 260

Rachford_Rice_polynomial() (in module chemicals.rachford_rice), 259
Rachford_Rice_solution() (in module chemicals.rachford_rice), 248
Rachford_Rice_solution2() (in module chemicals.rachford_rice), 256
Rachford_Rice_solution_binary_dd() (in module chemicals.rachford_rice), 254
Rachford_Rice_solution_Leibovici_Neoschil() (in module chemicals.rachford_rice), 251
Rachford_Rice_solution_Leibovici_Neoschil_dd() (in module chemicals.rachford_rice), 255
Rachford_Rice_solution_LN2() (in module chemicals.rachford_rice), 249
Rachford_Rice_solution_mpmath() (in module chemicals.rachford_rice), 254
Rachford_Rice_solution_polynomial() (in module chemicals.rachford_rice), 252
Rachford_Rice_solutionN() (in module chemicals.rachford_rice), 258
Rackett() (in module chemicals.volume), 471
Rackett_fit() (in module chemicals.volume), 483
Rackett_mixture() (in module chemicals.volume), 479
radius_of_gyration() (in module chemicals.utils), 361
REFPROP_sigma() (in module chemicals.interface), 204
remove_zeros() (in module chemicals.utils), 363
RG() (in module chemicals.molecular_geometry), 225
RG_all_methods (in module chemicals.molecular_geometry), 226
RG_methods() (in module chemicals.molecular_geometry), 225
rho_data_COSTALD (in module chemicals.volume), 486
rho_data_CRC_inorg_l (in module chemicals.volume), 487
rho_data_CRC_inorg_l_const (in module chemicals.volume), 487
rho_data_CRC_inorg_s_const (in module chemicals.volume), 487
rho_data_CRC_virial (in module chemicals.volume), 487
rho_data_Perry_8E_105_1 (in module chemicals.volume), 486
rho_data_SNMO (in module chemicals.volume), 486
rho_data_VDI_PPDS_2 (in module chemicals.volume), 487
rho_to_API() (in module chemicals.utils), 363
rho_to_Vm() (in module chemicals.utils), 364
RI () (in module chemicals.refractivity), 274
RI_all_methods (in module chemicals.refractivity), 275
RI_from_molar_refractivity() (in module chemicals.refractivity), 278
RI_IAPWS() (in module chemicals.refractivity), 275
RI_methods() (in module chemicals.refractivity), 275

RI_to_brix() (in module chemicals.refractivity), 277
Riedel() (in module chemicals.phase_change), 234
RON() (in module chemicals.combustion), 42
RON_all_methods (in module chemicals.combustion), 42
RON_methods() (in module chemicals.combustion), 42
Rowlinson_Bondi() (in module chemicals.heat_capacity), 123
Rowlinson_Poling() (in module chemicals.heat_capacity), 123

\section*{S}

SOg () (in module chemicals.reaction), 268
SOg_all_methods (in module chemicals.reaction), 269
SOg_methods() (in module chemicals.reaction), 269
S01() (in module chemicals.reaction), 267
S01_all_methods (in module chemicals.reaction), 268
S01_methods() (in module chemicals.reaction), 268
SOs() (in module chemicals.reaction), 266
SOs_all_methods (in module chemicals.reaction), 267
S0s_methods() (in module chemicals.reaction), 267
Sanjari() (in module chemicals.vapor_pressure), 387
Sastri_Rao() (in module chemicals.interface), 193
Sato_Riedel () (in module chemicals.thermal_conductivity), 308
search_chemical() (in module chemicals.identifiers), 185
serialize_formula() (in module chemicals.elements), 81
SG() (in module chemicals.utils), 341
SG_to_API() (in module chemicals.utils), 342
Sheffy_Johnson() (in module chemicals.thermal_conductivity), 307
Shomate() (in module chemicals.heat_capacity), 102
Shomate_integral() (in module chemicals.heat_capacity), 103
Shomate_integral_over_T() (in module chemicals.heat_capacity), 104
ShomateRange (class in chemicals.heat_capacity), 104
sigma_Bird_Stewart_Lightfoot_boiling() (in module chemicals.lennard_jones), 219
sigma_Bird_Stewart_Lightfoot_critical_1() (in module chemicals.lennard_jones), 219
sigma_Bird_Stewart_Lightfoot_critical_2() (in module chemicals.lennard_jones), 218
sigma_Bird_Stewart_Lightfoot_melting() (in module chemicals.lennard_jones), 220
sigma_data_Jasper_Lange (in module chemicals.interface), 209
sigma_data_Mulero_Cachadina (in module chemicals.interface), 209
sigma_data_Somayajulu (in module chemicals.interface), 209
sigma_data_Somayajulu2 (in module chemi- Suzuki_LFL() (in module chemicals.safety), 289
cals.interface), 209 Suzuki_UFL() (in module chemicals.safety), 292
sigma_data_VDI_PPDS_11 (in module chemi-
sigma_Stiel_Thodos() (in module chemicals.lennard_jones), 220
sigma_Tee_Gotoh_Steward_1() (in module chemicals.lennard_jones), 221
sigma_Tee_Gotoh_Steward_2() (in module chemicals.lennard_jones), 222
similarity_variable() (in module chemicals.elements), 82
simple_formula_parser() (in module chemicals.elements), 79
Skin() (in module chemicals.safety), 283
Skin_all_methods (in module chemicals.safety), 284
Skin_methods() (in module chemicals.safety), 284
SMK () (in module chemicals.phase_change), 238
SNMO () (in module chemicals.volume), 477
solubility_eutectic() (in module chemicals.solubility), 302
solubility_parameter() (in module chemicals.solubility), 303
solve_flow_composition_mix() (in module chemicals.utils), 364
Somayajulu() (in module chemicals.interface), 205
sorted_CAS_key() (in module chemicals.identifiers), 188
speed_of_sound() (in module chemicals.utils), 365
STEL() (in module chemicals.safety), 281
STEL_all_methods (in module chemicals.safety), 281
STEL_methods() (in module chemicals.safety), 281
Stiel_polar_factor() (in module chemicals.acentric), 9
Stiel_Thodos() (in module chemicals.viscosity), 446
Stiel_Thodos_dense() (in module chemicals.thermal_conductivity), 323
Stockmayer() (in module chemicals.lennard_jones), 211
Stockmayer_all_methods (in module chemicals.lennard_jones), 213 (in module chemi-
Stockmayer_methods() (in module chemicals.lennard_jones), 212
stoichiometric_matrix() (in module chemicals.reaction), 272

T
T_autoignition() (in module chemicals.safety), 286
T_autoignition_all_methods (in module chemicals.safety), 287
T_autoignition_methods() (in module chemicals.safety), 287
T_converter() (in module chemicals.temperature), 305
T_flash() (in module chemicals.safety), 285
T_flash_all_methods (in module chemicals.safety),
T_flash_methods() (in module chemicals.safety), 286
Suzuki_LFL() (in module chemicals.safety), 289

T_star() (in module chemicals.lennard_jones), 223
Tarakad_Danner_virial_CSP_kijs() (in module chemicals.virial), 428
Tarakad_Danner_virial_CSP_omegaijs() (in module chemicals.virial), 429
Tarakad_Danner_virial_CSP_Pcijs() (in module chemicals.virial), 429
Tarakad_Danner_virial_CSP_Tcijs() (in module chemicals.virial), 428
Tb() (in module chemicals.phase_change), 230
Tb_all_methods (in module chemicals.phase_change), 231
Tb_methods() (in module chemicals.phase_change), 231
Tb_Tc_relationship() (in module chemicals.critical), 57
Tc () (in module chemicals.critical), 45
Tc_all_method_types (in module chemicals.critical), 46
Tc_all_methods (in module chemicals.critical), 46
Tc_methods() (in module chemicals.critical), 46
TDE_CSExpansion() (in module chemicals.heat_capacity), 122
TDE_PVExpansion() (in module chemicals.vapor_pressure), 376
TDE_RIXExpansion() (in module chemicals.refractivity), 279
TDE_VDNS_rho() (in module chemicals.volume), 484
TEOS10_BAW_derivatives() (in module chemicals.air), 24
TEOS10_CAAW_derivatives() (in module chemicals.air), 25
TEOS10_CAWW_derivatives() (in module chemicals.air), 26
third_property() (in module chemicals.critical), 53
Tm () (in module chemicals.phase_change), 232
Tm_all_methods (in module chemicals.phase_change), 233
Tm_depression_eutectic() (in module chemicals.solubility), 303
Tm_methods() (in module chemicals.phase_change), 232
to_num() (in module chemicals.utils), 366
Townsend_Hales() (in module chemicals.volume), 474
TRC_Antoine_extended() (in module chemicals.vapor_pressure), 374
TRC_Antoine_extended_fitting_jacobian() (in module chemicals.vapor_pressure), 384
TRC_gas_data (in module chemicals.heat_capacity), 130
TRCCp() (in module chemicals.heat_capacity), 100
TRCCp_integral() (in module chemicals.heat_capacity), 101
TRCCp_integral_over_T() (in module chemicals.heat_capacity), 102
TrivialSolutionError (class in chemicals.exceptions), 91
Tsat_IAPWS() (in module chemicals.vapor_pressure), 391
Tt () (in module chemicals.triple), 336
Tt_all_methods (in module chemicals.triple), 336
Tt _methods() (in module chemicals.triple), 336
TWA() (in module chemicals.safety), 282
TWA_all_methods (in module chemicals.safety), 282
TWA_methods() (in module chemicals.safety), 282
Twu_1985() (in module chemicals.viscosity), 457

\section*{U}

UFL() (in module chemicals.safety), 291
UFL_all_methods (in module chemicals.safety), 292
UFL_methods() (in module chemicals.safety), 292
UnderspecifiedError (class in chemicals.exceptions), 90

\section*{V}
v_molar_to_v() (in module chemicals.utils), 366
v_to_v_molar() (in module chemicals.utils), 366
vapor_mass_quality() (in module chemicals.utils), 367
Vc() (in module chemicals.critical), 48
Vc_all_methods (in module chemicals.critical), 49
Vc_methods() (in module chemicals.critical), 49
Velasco() (in module chemicals.phase_change), 240
velocity_to_molar_velocity() (in module chemicals.utils), 367
Vetere() (in module chemicals.phase_change), 237
Vfs_to_zs() (in module chemicals.utils), 342
vibration_frequency_cm_to_characteristic_temperature() (in module chemicals.heat_capacity), \(115 \quad \mathrm{Z}\) () (in module chemicals.utils), 344
viscosity_converter() (in module chemi- Z_from_virial_density_form() (in module chemicals.viscosity), 465
viscosity_gas_Gharagheizi() (in module chemicals.viscosity), 447
viscosity_index() (in module chemicals.viscosity), 466
Viswanath_Natarajan_2() (in module chemicals.viscosity), 461

Viswanath_Natarajan_2_exponential() (in module chemicals.viscosity), 462
Viswanath_Natarajan_3() (in module chemicals.viscosity), 462
Vm_to_rho() (in module chemicals.utils), 343
volume_VDI_PPDS() (in module chemicals.volume), 483

\section*{W}

Wagner() (in module chemicals.vapor_pressure), 372
Wagner_fitting_jacobian() (in module chemicals.vapor_pressure), 383
Wagner_original() (in module chemicals.vapor_pressure), 373
Wagner_original_fitting_jacobian() (in module chemicals.vapor_pressure), 383
Wassiljewa_Herning_Zipperer() (in module chemicals.thermal_conductivity), 327
Watson() (in module chemicals.phase_change), 242
Watson_K() (in module chemicals.utils), 343
Watson_n() (in module chemicals.phase_change), 242
Watson_sigma() (in module chemicals.interface), 207
Weinaug_Katz() (in module chemicals.interface), 200
Wilke() (in module chemicals.viscosity), 450
Wilke_large() (in module chemicals.viscosity), 453
Wilke_prefactored() (in module chemicals.viscosity), 452
Wilke_prefactors() (in module chemicals.viscosity), 451
Wilson_K_value() (in module chemicals.flash_basic), 98
Winterfeld_Scriven_Davis() (in module chemicals.interface), 199
ws_to_zs() (in module chemicals.utils), 368
Y
Yamada_Gunn() (in module chemicals.volume), 474
Yaws_Psat() (in module chemicals.vapor_pressure), 375
Yaws_Psat_fitting_jacobian() (in module chemicals.vapor_pressure), 384
Yen_Woods_saturation() (in module chemicals.volume), 473
Yoon_Thodos() (in module chemicals.viscosity), 445 cals.virial), 401
Z_from_virial_pressure_form() (in module chemicals.virial), 401
Zabransky_cubic() (in module chemicals.heat_capacity), 117
Zabransky_cubic_integral() (in module chemicals.heat_capacity), 118

Zabransky_cubic_integral_over_T() (in module chemicals.heat_capacity), 118
zabransky_dicts (in module chemicals.heat_capacity), 130
Zabransky_quasi_polynomial() (in module chemicals.heat_capacity), 115
Zabransky_quasi_polynomial_integral() (in module chemicals.heat_capacity), 116
Zabransky_quasi_polynomial_integral_over_T() (in module chemicals.heat_capacity), 116
ZabranskyQuasipolynomial (class in chemicals.heat_capacity), 120
ZabranskySpline (class in chemicals.heat_capacity), 119
Zc () (in module chemicals.critical), 51
Zc_all_methods (in module chemicals.critical), 52
Zc_methods() (in module chemicals.critical), 52
zs_to_Vfs() (in module chemicals.utils), 368
zs_to_ws() (in module chemicals.utils), 369
Zuo_Stenby () (in module chemicals.interface), 193```

